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**16. ABSTRACT**

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More than 3000 noise and environmental measurements were made at sixteen level road sites in California. Included were automobiles and medium and heavy trucks traveling at constant speeds between 25 and 65 mph. Microphones were located at distances of 25, 50 and 100 feet, and at heights of 5 and 10 feet.

Analyses of data show that California automobile noise is 0.8 to 1.0 dBA higher than national levels. In contrast, medium and heavy trucks are 0.5 to 3 dBA lower than the national levels. The study also indicated that the three vehicle groups adequately represented the California vehicle population and geographical differences may be ignored. Effects of opposite winds of less than 12 mph, and terrain cover introduced errors of no more than 1 dBA at the 50-foot reference distance.

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CALIFORNIA VEHICLE NOISE  
EMISSION LEVELS

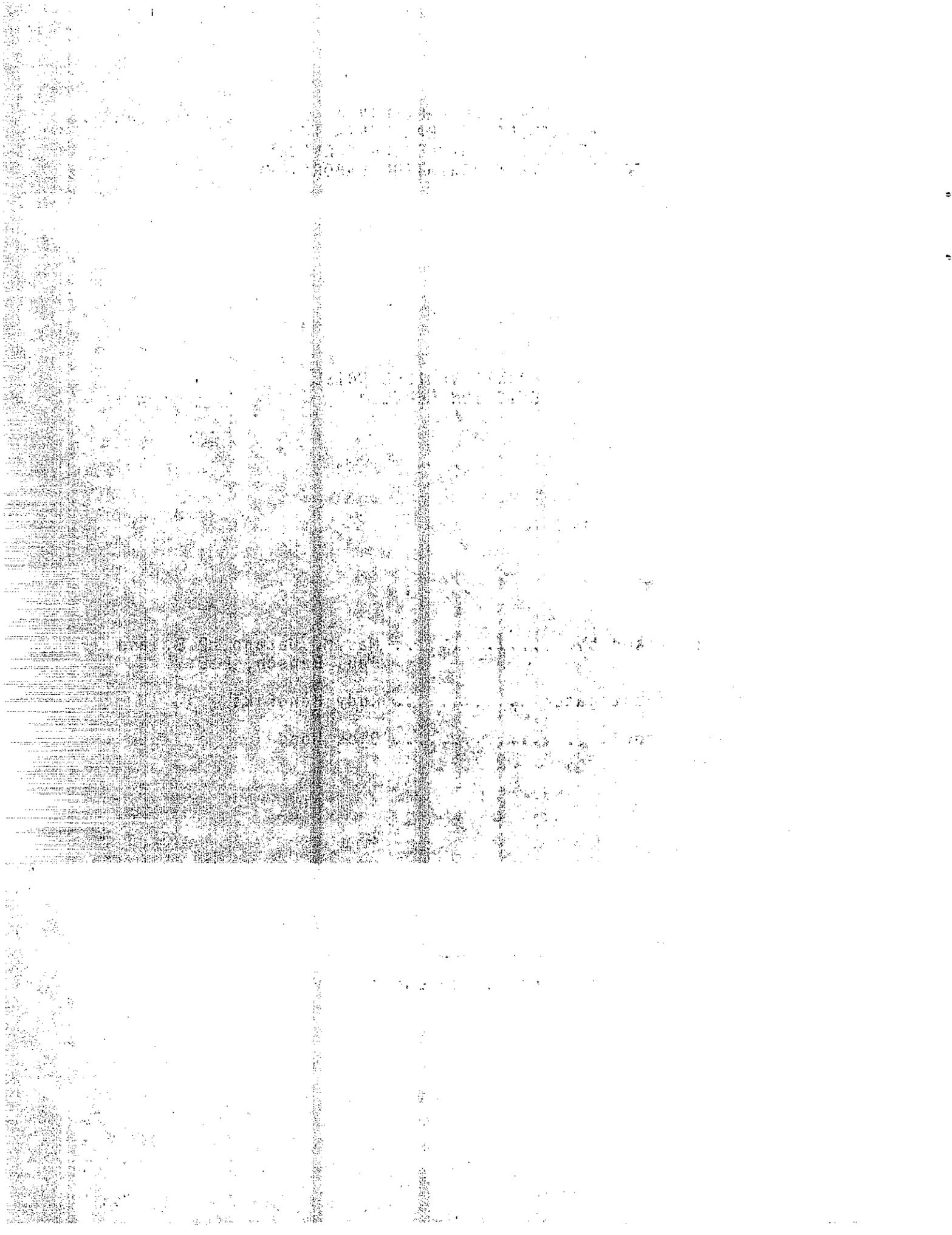
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Co-Investigator ..... Dick Wood



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Chief, Office of Transportation Laboratory



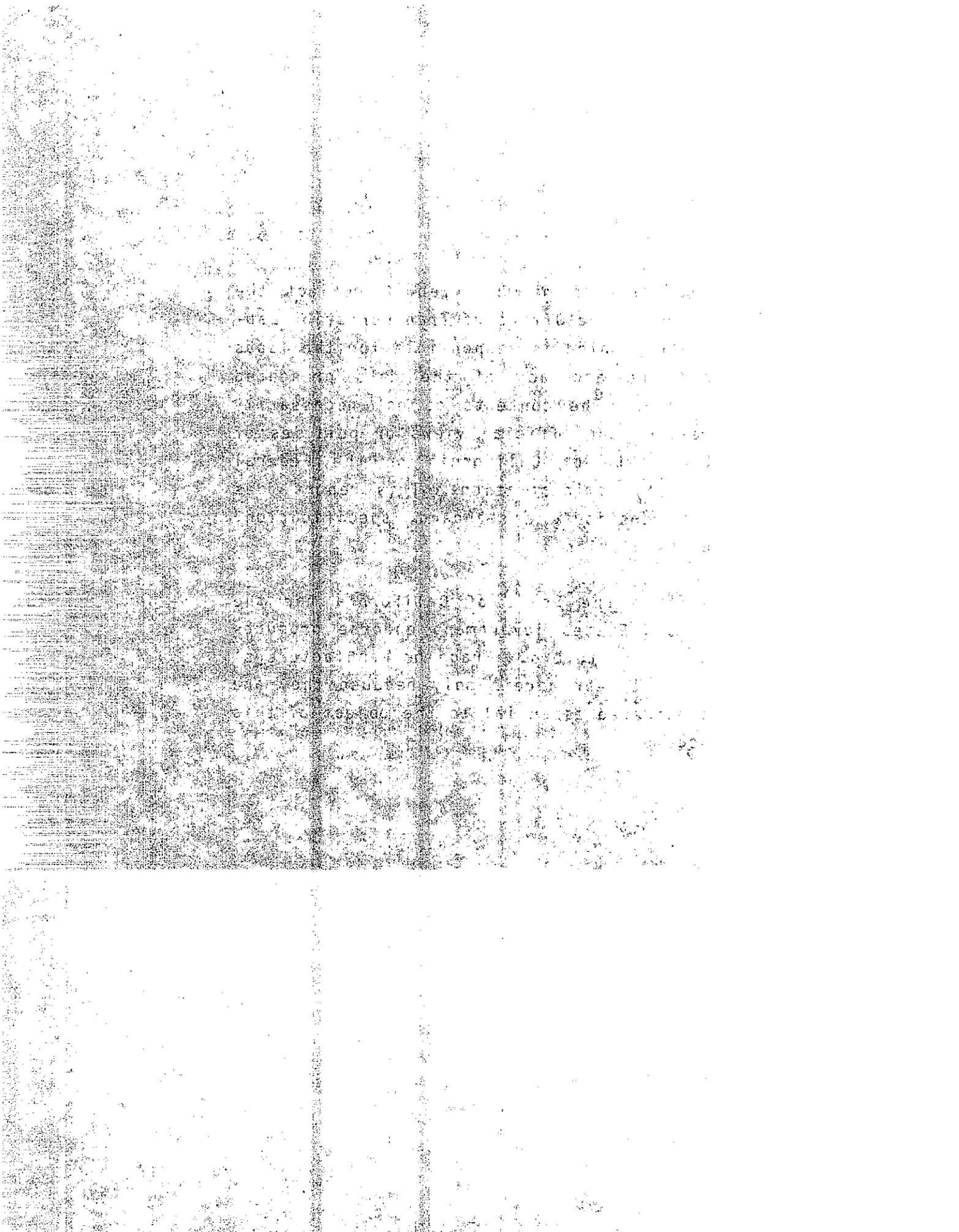
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Population	150,000,000	155,000,000	160,000,000	165,000,000	170,000,000	175,000,000	180,000,000	185,000,000	190,000,000	195,000,000	200,000,000	205,000,000	210,000,000	215,000,000	220,000,000	225,000,000	230,000,000	235,000,000	240,000,000	245,000,000	250,000,000	255,000,000	260,000,000	265,000,000	270,000,000	275,000,000	280,000,000	285,000,000	290,000,000	295,000,000	300,000,000	305,000,000	310,000,000	315,000,000	320,000,000	325,000,000	330,000,000	335,000,000	340,000,000	345,000,000	350,000,000	355,000,000	360,000,000	365,000,000	370,000,000	375,000,000	380,000,000	385,000,000	390,000,000	395,000,000	400,000,000	405,000,000	410,000,000	415,000,000	420,000,000	425,000,000	430,000,000	435,000,000	440,000,000	445,000,000	450,000,000	455,000,000	460,000,000	465,000,000	470,000,000	475,000,000	480,000,000	485,000,000	490,000,000	495,000,000	500,000,000	505,000,000	510,000,000	515,000,000	520,000,000	525,000,000	530,000,000	535,000,000	540,000,000	545,000,000	550,000,000	555,000,000	560,000,000	565,000,000	570,000,000	575,000,000	580,000,000	585,000,000	590,000,000	595,000,000	600,000,000	605,000,000	610,000,000	615,000,000	620,000,000	625,000,000	630,000,000	635,000,000	640,000,000	645,000,000	650,000,000	655,000,000	660,000,000	665,000,000	670,000,000	675,000,000	680,000,000	685,000,000	690,000,000	695,000,000	700,000,000	705,000,000	710,000,000	715,000,000	720,000,000	725,000,000	730,000,000	735,000,000	740,000,000	745,000,000	750,000,000	755,000,000	760,000,000	765,000,000	770,000,000	775,000,000	780,000,000	785,000,000	790,000,000	795,000,000	800,000,000	805,000,000	810,000,000	815,000,000	820,000,000	825,000,000	830,000,000	835,000,000	840,000,000	845,000,000	850,000,000	855,000,000	860,000,000	865,000,000	870,000,000	875,000,000	880,000,000	885,000,000	890,000,000	895,000,000	900,000,000	905,000,000	910,000,000	915,000,000	920,000,000	925,000,000	930,000,000	935,000,000	940,000,000	945,000,000	950,000,000	955,000,000	960,000,000	965,000,000	970,000,000	975,000,000	980,000,000	985,000,000	990,000,000	995,000,000	1,000,000,000

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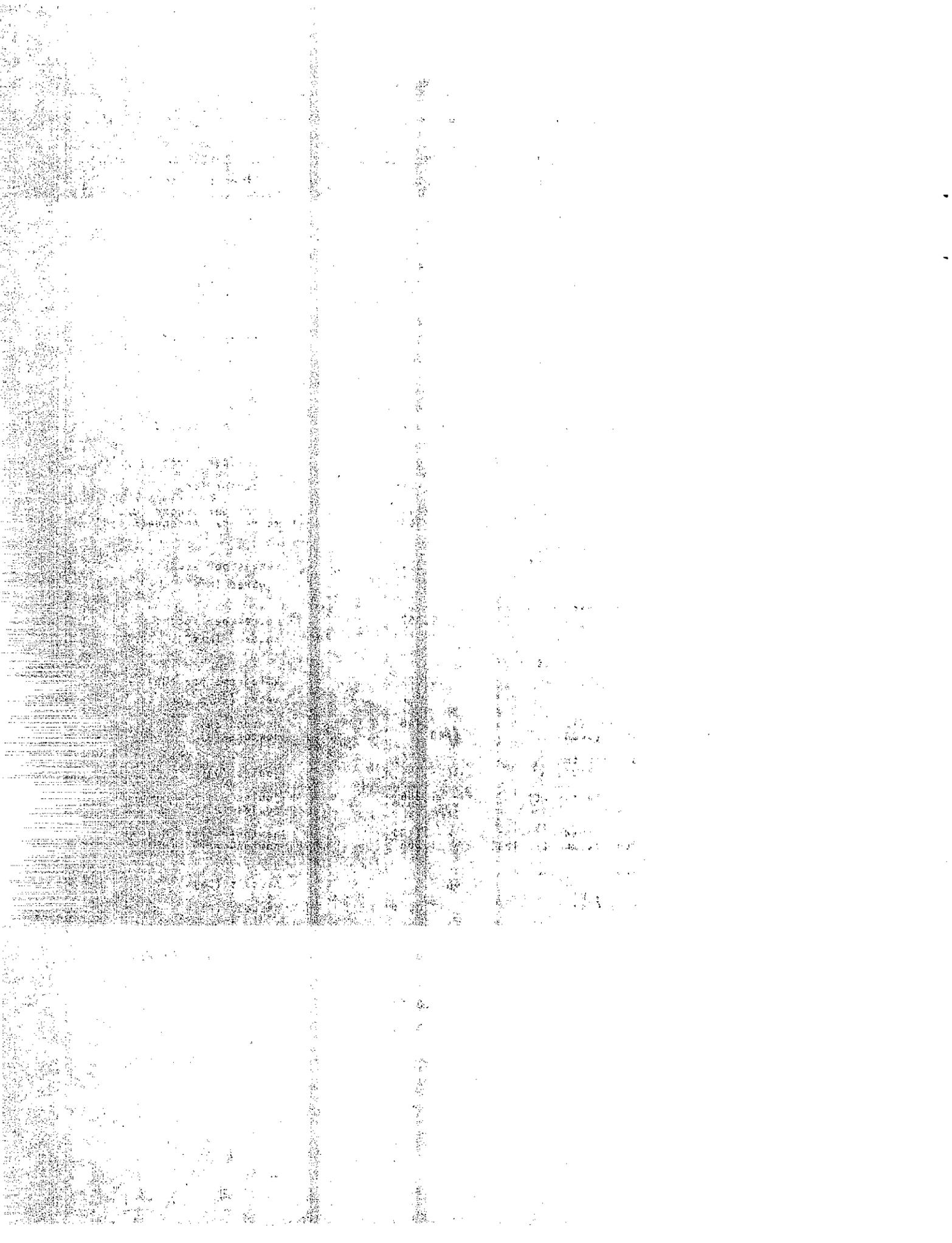
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English to Metric System (SI) of Measurement

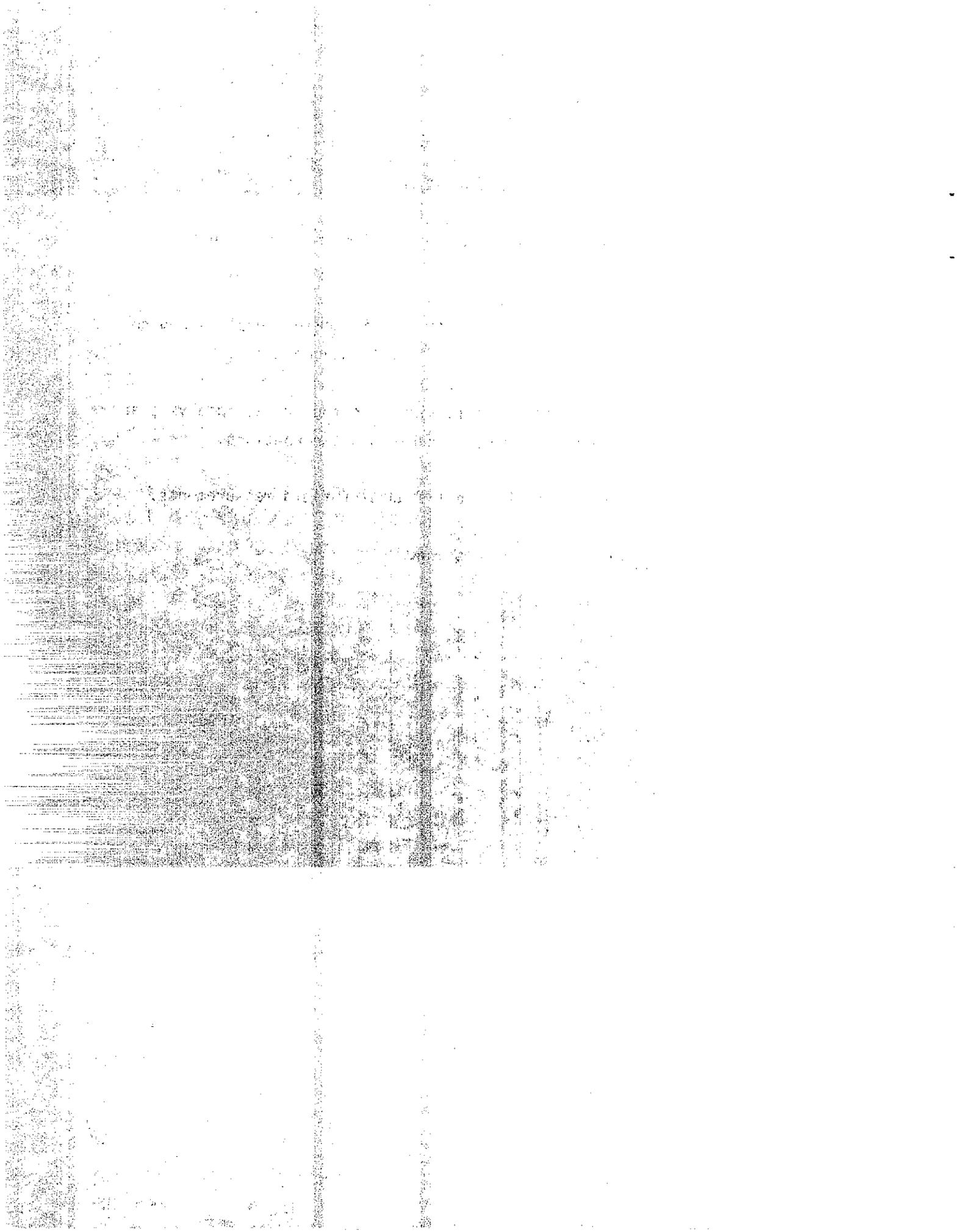
<u>Quantity</u>	<u>English unit</u>	<u>Multiply by</u>	<u>To get metric equivalent</u>
Length	inches (in) or (")	25.40 .02540	millimetres (mm) metres (m)
	feet (ft) or (')	.3048	metres (m)
	miles (mi)	1.609	kilometres (km)
Area	square inches (in <sup>2</sup> )	6.432 x 10 <sup>-4</sup>	square metres (m <sup>2</sup> )
	square feet (ft <sup>2</sup> )	.09290	square metres (m <sup>2</sup> )
	acres	.4047	hectares (ha)
Volume	gallons (gal)	3.785	litres (l)
	cubic feet (ft <sup>3</sup> )	.02832	cubic metres (m <sup>3</sup> )
	cubic yards (yd <sup>3</sup> )	.7646	cubic metres (m <sup>3</sup> )
Volume/Time (Flow)	cubic feet per second (ft <sup>3</sup> /s)	28.317	litres per second (l/s)
	gallons per minute (gal/min)	.06309	litres per second (l/s)
Mass	pounds (lb)	.4536	kilograms (kg)
Velocity	miles per hour (mph)	.4470	metres per second (m/s)
	feet per second (fps)	.3048	metres per second (m/s)
Acceleration	feet per second squared (ft/s <sup>2</sup> )	.3048	metres per second squared (m/s <sup>2</sup> )
	acceleration due to force of gravity (G)	9.807	metres per second squared (m/s <sup>2</sup> )
Weight Density	pounds per cubic (lb/ft <sup>3</sup> )	16.02	kilograms per cubic metre (kg/m <sup>3</sup> )
Force	pounds (lbs)	4.448	newtons (N)
	kips (1000 lbs)	4448	newtons (N)
Thermal Energy	British thermal unit (BTU)	1055	joules (J)
Mechanical Energy	foot-pounds (ft-lb)	1.356	joules (J)
	foot-kips (ft-k)	1356	joules (J)
Bending Moment or Torque	inch-pounds (ft-lbs)	.1130	newton-metres (Nm)
	foot-pounds (ft-lbs)	1.356	newton-metres (Nm)
Pressure	pounds per square inch (psi)	6895	pascals (Pa)
	pounds per square foot (psf)	47.88	pascals (Pa)
Stress Intensity	kips per square inch square root inch (ksi √in)	1.0988	mega pascals √metre (MPa √m)
	pounds per square inch square root inch (psi √in)	1.0988	kilo pascals √metre (KPa √m)
Plane Angle	degrees (°)	0.0175	radians (rad)
Temperature	degrees fahrenheit (F)	$\frac{tF - 32}{1.8} = tC$	degrees celsius (°C)



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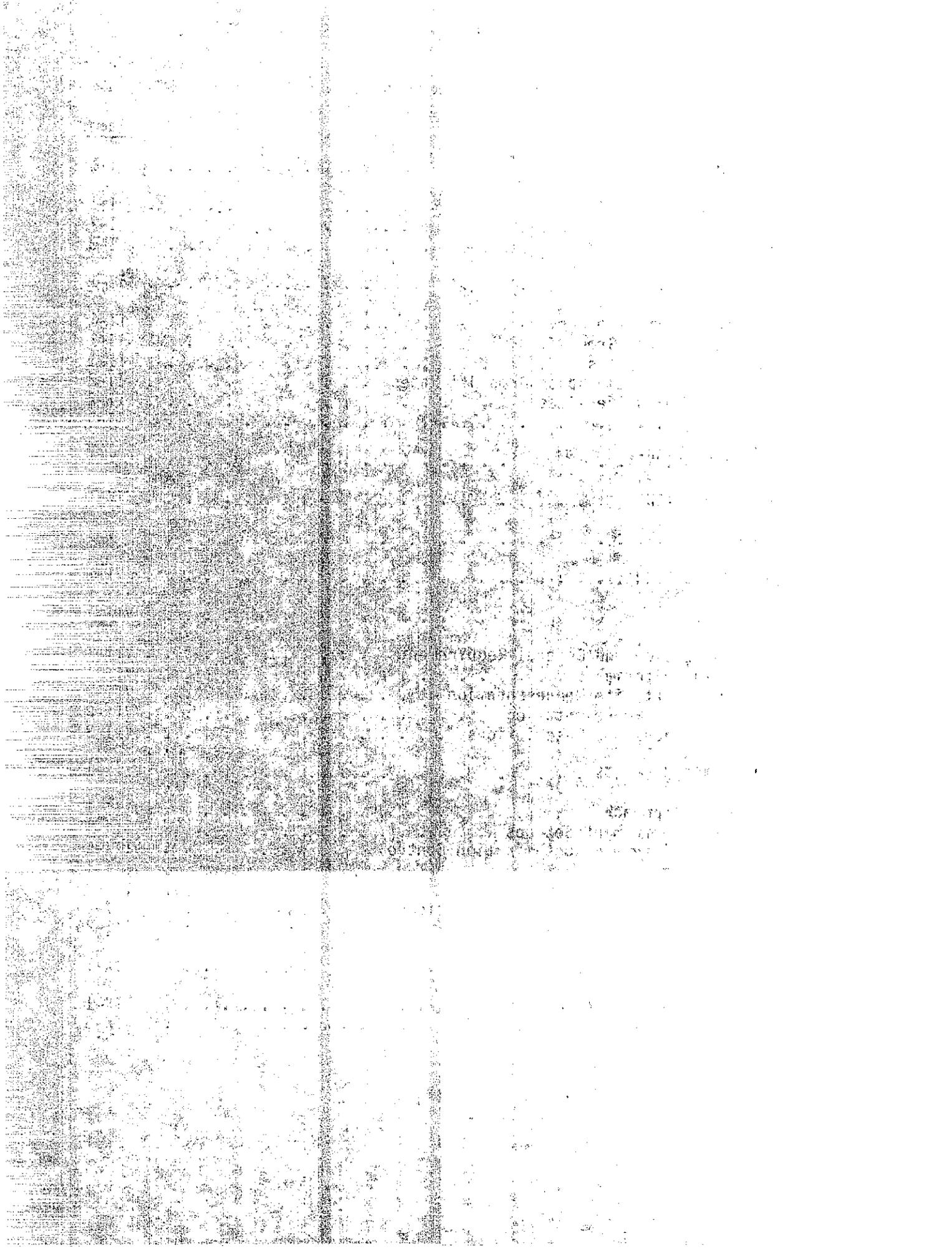
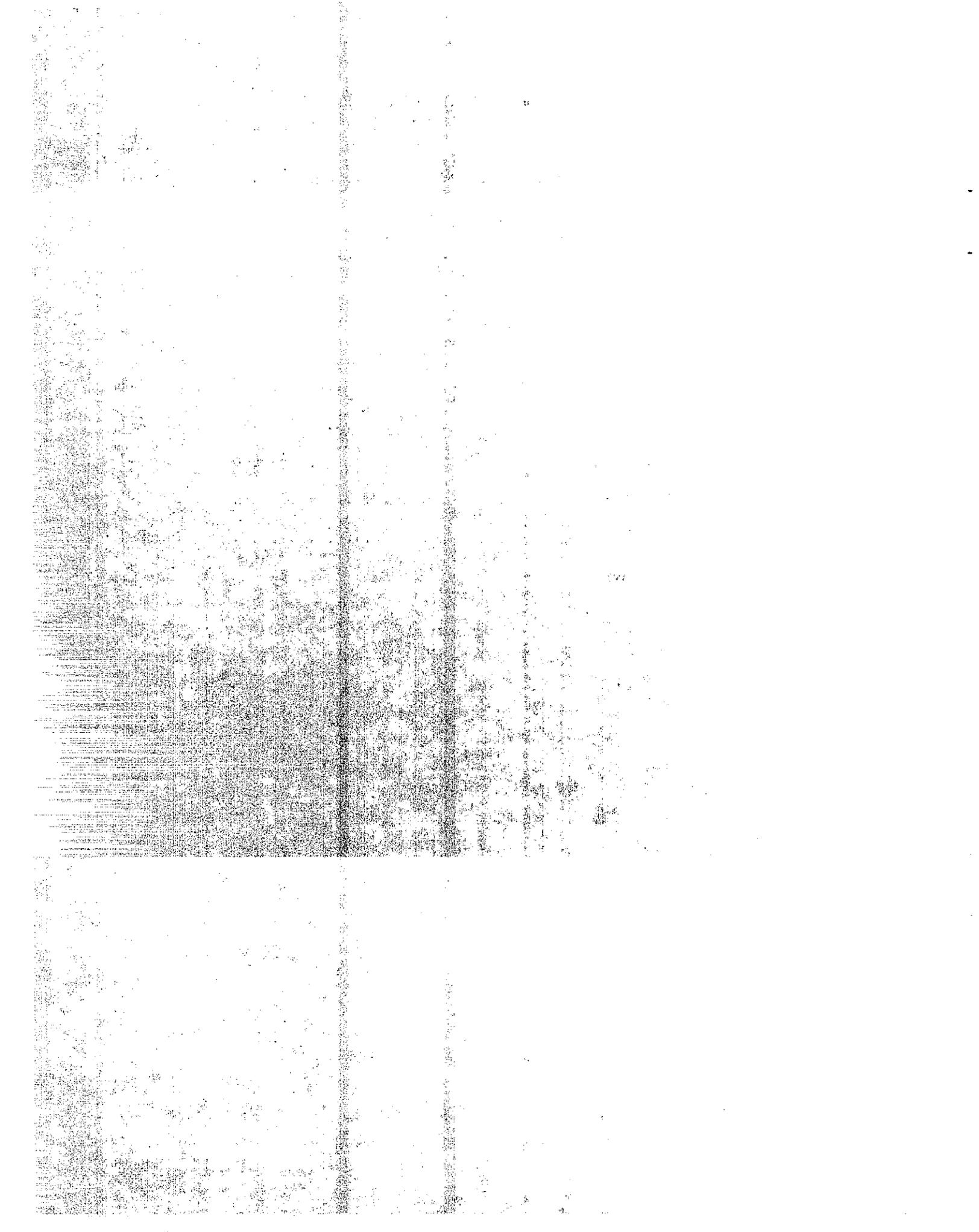


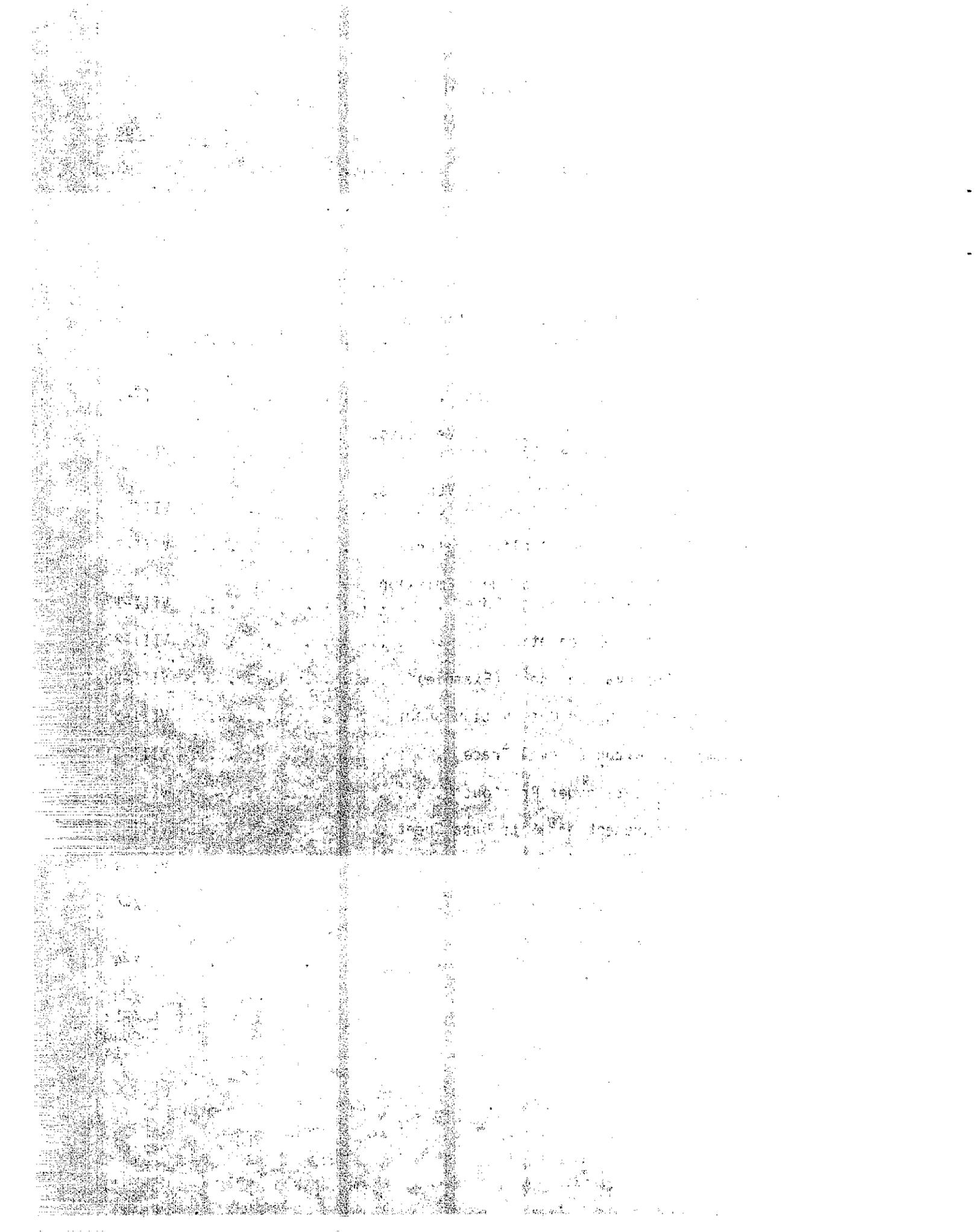
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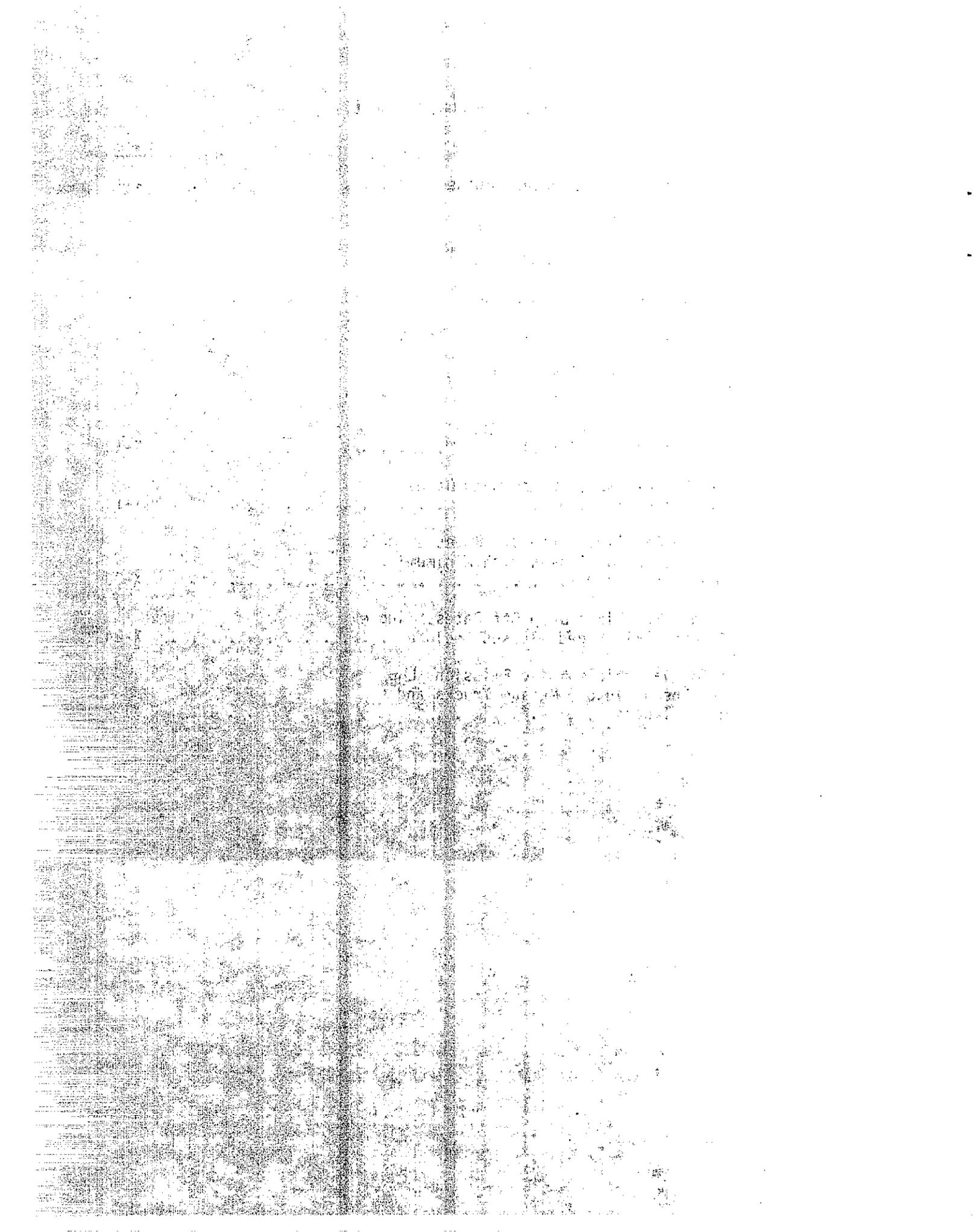
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## I. INTRODUCTION

This is a draft interim report presenting the results of the California Vehicle Noise Reference Energy Mean Emission Levels study for level roads. An extension to the research project has been approved to include noise emission levels for trucks when grades are involved.

The final report including noise emission curves for both level roads and grades is expected to be completed by July 1985.

### Background

The noise abatement procedures for Federal or Federal Aid highway projects are governed by the Federal Aid Highway Program Manual (FHPM) 7-7-3(1). This directive requires state highway agencies to determine and analyze expected traffic noise impacts and alternative noise abatement measures to mitigate these impacts.

As part of the traffic noise impact analysis under FHPM 7-7-3, prediction of future traffic noise is required. Any prediction method may be used to satisfy this requirement if it generally meets the following two conditions:

1. The method must be consistent with the FHWA Highway Traffic Noise Prediction Model, Report No. FHWA RD-77-108(2).

- 2 The prediction method must use either the National Reference Energy Mean Emission Levels as a function of speed(1,2) or reference energy mean emission levels determined by the methodology described in FHWA-DP-45 1R(3).

Since 1978, the California Department of Transportation (Caltrans) has used the National Reference Energy Mean Emission Levels as a function of speed for noise predictions for Federal or Federal Aid highway projects. These noise emission levels were based on FHWA-RD-77-19(4) (autos), and FHWA-RD-78-64(5) which presented statistical analyses on truck data gathered in the 1975 Four-State Noise Inventory(6). California was not among the four states in the study. It is also reasonable to assume that vehicle noise emission levels may have changed since 1975, due to new truck noise emissions regulations and the recent popularity of compact, energy efficient automobiles. For these reasons, Caltrans recognized the need for a California vehicle noise emission study.

A 1981 Caltrans barrier evaluation study(7) comparing before and after barrier measured noise levels with those predicted by FHWA-RD-77-108(2) methods concluded that the latter tended to predict average values of 3 to 4 dBA higher than those measured at eleven barrier sites throughout California. That study recommended further investigation to examine the validity of using the national emission levels in California. The recommendation was followed up, and this report presents the results.

### Objectives

The primary objective of this study was to develop California Vehicle Noise Reference Energy Mean Emission Levels for use in California highway noise studies complying with the FHPM 7-7-3 requirements. The methods and criteria used to accomplish the primary objective are consistent with FHWA-DP-451R(3) and FHWA-OEP/HEV-78-1(8).

There were some secondary objectives in this study:

°Verification of the inference from the four state study that vehicles in California can be categorized in three acoustic source groups to represent the State's entire vehicle population without introducing significant errors in noise predictions.

°Examining the effects of hard and soft site characteristics (as defined by FHWA RD-77-108(2)) on noise emission levels measured at a 50-foot reference distance.

°Studying near and far field (defined in FHWA RD-77-108(2)) single event drop-off rates as a function of distance and vehicle group.

°Examining geographical differences in vehicle emission levels for two regions in California, representing as Northern and Southern California.

°Examining the effects of wind on emission level measurements.

#### Work Plan

A total of sixteen sites were selected for this study, eight in Northern California and eight in the southern part of the state. Each vehicle group was about equally represented in the northern and southern portions of the state.

The number of vehicle passby events measured was 3045. Because of stringent contamination control and other rejection criteria, 2734 events were actually used to determine

emission levels. Of these, 46.2% were automobiles, 11.6% medium trucks and 42.2% heavy trucks (as defined in FHWA-RD-77-108(2)). Speed dependent reference energy mean emission levels were developed for each of the three vehicle groups for constant speeds from 25 mph to 65 mph on level roads. These emission curves are presented in Chapter XI of this report.

The secondary objectives were attained by measurements using up to 5 microphones at distances ranging from 25 to 100 feet from the centerline of vehicle travel and at heights of 5 feet and 10 feet.

All noise measurements were made on the A-weighted scale. No frequency spectra were measured, nor was any attempt made to verify vehicle noise centroid heights as reported in FHWA-RD-77-108(2).

## II. CONCLUSIONS

### California Emission Levels

Automobiles. The California reference energy mean emission levels are from 0.8 dBA at 31 mph to 1.0 dBA at 60 mph higher than the national reference mean energy emission levels.

Medium Trucks. The California levels are from 0.5 dBA at 31 mph to 2.9 dBA at 60 mph lower than FHWA (national) levels.

Heavy Trucks. The California levels are from 0.2 dBA higher at 31 mph to 2.8 dBA lower at 60 mph than FHWA levels.

Because of the importance of heavy truck volumes in noise predictions, the net effect of the above three findings is a lower predicted noise level of about 2 dBA for average traffic mixes.

### Acoustic Source Groups

California vehicles can be categorized in three acoustic source groups: autos, medium trucks and heavy trucks, using the same definitions as in FHWA RD-77-108(2).

### Hard vs. Soft Sites

The difference in noise levels between hard and soft site characteristics at 50 feet from the centerline of vehicle travel, averaged 2.0 dBA for autos, 1.9 dBA for medium trucks and 1.6 dBA for heavy trucks. Because of the many variations in site characteristics encountered in the sixteen measuring sites, the California emission levels provide a balance between hard

and soft site noise levels at 50 feet that guarantees accuracies of well within +1 dBA for all but the most extreme site conditions.

#### Near and Far Field Noise Drop-Off Rates

In both near (less than 50 feet) and far (50 feet or greater) fields, site characteristics had an effect on the single event drop off rates.

On hard sites, the near field drop off rates were reduced to an average of 5.2 dBA per doubling of distance (DD), probably due to point source degradation close to the vehicles.

In the far field, the average hard site single event drop off rates were 5.9 dBA/DD for the low microphones (5-foot high) and 5.2 dBA/DD for the high microphones (10-foot high). The latter deviation from the expected 6.0 dBA/DD point source drop off rate was probably due to greater exposure to reflections from the roadway.

On soft sites, the near field point source degradation effects on drop off rates was more than offset by excess ground attenuation. The drop off rates averaged 7.0 dBA/DD at a height of 5 feet.

In the far field, the average soft site drop off rate for single events was 7.9 dBA at 5-foot heights and 6.8 dBA at 10 feet, indicating that soft site characteristics still affect noise levels at 10 feet above the ground.

#### Geographical Differences

There appeared to be no differences between Northern and Southern California for autos and medium trucks. Heavy trucks

appeared to be louder in Northern California by up to 2 dBA. The California emission curve for heavy trucks, however, provides a balance guaranteeing accuracies within +1 dBA in most locations in California.

### Wind

For winds of 12 mph or less, direction had no apparent effect on measurements at 50 feet. For opposite cross wind (90° to roadway) directions with speeds between 6-12 mph there appeared to be a statistically significant difference at 100 feet of 3 dBA in noise levels generated by autos. This difference could have been caused by wind direction, site variation, or both. It was not possible to separate individual contributions by each. No differences were detected for medium and heavy trucks at 100 feet.



### III. RECOMMENDATIONS

This report makes the following recommendations:

°The California Vehicle Noise Reference Energy Mean Emission Levels should be used in California for highway noise predictions in new studies effective as soon as possible after FHWA approval.

°Computer programs should have an option for either National or California emission levels to allow completion of studies already in progress.

°California vehicle noise emission levels should be updated periodically to account for changes in vehicle fleets. These update efforts do not have to be as extensive as the efforts presented in this report.

°Further research is recommended in line source drop off rates as a function of distance, height, terrain, wind speed and wind direction. These variables have a significant effect on noise measurements and prediction results.

The document contains several paragraphs of text, which are extremely faint and difficult to read. The text appears to be a formal report or document, possibly related to a project or organization. The content is largely illegible due to the low contrast and high noise of the scan. Some faint words and phrases are visible, but they do not form a coherent or readable message.

#### IV. IMPLEMENTATION

Immediately following approval by the FHWA, the California Vehicle Noise Reference Energy Mean Emission Levels presented in Chapter XI of this report will be programmed into all Caltrans computer versions of the FHWA Highway Traffic Noise Prediction Model (FHWA-RD-77-108)). The National Reference Energy Mean Emission Levels will remain available to allow completion of noise studies already in progress.

A memorandum will be sent to all Caltrans districts advising concerned environmental and project development personnel of the changes.

This draft interim report will also be distributed to concerned environmental and project development personnel.

The final report consisting of this report and grade emission levels, will also be distributed after completion in 1985. Appropriate computer program changes will be made at that time.



## V. BENEFITS

At the outset of this study, benefits could not be estimated in terms of dollar savings. There were three possible outcomes for the California emission level results. First, the levels could have been the same as the national emission levels. In this case, the "benefit" would have been the reassurance that the levels used for noise predictions and barrier designs were accurate.

A second outcome could have been that the California emission levels were higher than the national levels. There would not have been any benefit to Caltrans or FHWA in this outcome, at least not directly translatable into dollars. Higher predicted noise levels would result in higher barriers and greater costs.

The third outcome, lower California emission levels, would obviously translate directly into dollar savings for Caltrans and FHWA resulting from reduced mitigation measures.

The benefit common to all three outcomes is the improved accuracy of the model, thereby assuring both increased confidence in the model results, and a higher level of service to the public.

As the conclusions indicated, the third outcome - that of lower California truck emission levels than national levels - occurred.

It is, therefore, not entirely fair to credit the benefit in barrier savings to the design of this study. The benefits, however, may be viewed as incidental to the search for increased accuracy in the model.

For average traffic mixes and speeds of 55 mph predicted noise levels should be approximately 2 dBA lower using the California emission levels. To translate this into dollar savings, several items need to be considered. Firstly, retrofit barriers for existing freeways will not be affected by the lower emission levels, due to the current Caltrans practice of calibrating the model with existing noise measurements.

Secondly, Caltrans Noise Barrier Design Information Bulletin No. 58(9) requires a barrier line-of-sight (LOS) break between an 11.5-foot truck stack and 5-foot receiver. The actual height of the LOS break depends on the roadway-barrier-receiver geometry. For average, at-grade highway conditions, the break height lies between 8 to 10 feet.

Finally, the accoustical barrier design also depends on traffic mix and geometry.

For future barriers along proposed new highway alignments where model calibration is not possible, barrier cost savings using California emission levels could result in savings of \$200,000 per mile for at-grade sections. The estimate is based on typical traffic mixes at 55 mph, at-grade section, barrier to equivalent noise source distance of 50 feet and barrier to receiver distance of 50 feet. A noise wall designed to be 13 feet high with national emission levels could be reduced to approximately 10 feet using California emission levels to achieve a certain predicted noise level behind the barrier. In some marginal cases it is possible that a barrier might be entirely eliminated.

Higher predictions of 2 dBA with national emission levels are consistent with average overpredictions of 3 to 4 dBA reported in a previous Caltrans study(8).

## VI. INSTRUMENTATION

All sound level meters (SLM) used in this study met the requirements of Type I Precision SLM per ANSI S1.4, 1983 (10). The SLM were connected to a datalogger specifically designed for the California Transportation Laboratory.

The datalogger has sixteen channels which may be selectively activated to receive up to sixteen DC output signals from SLM. The signals are then converted by the datalogger's microprocessor into continuous, time varying noise signals which are digitally displayed and updated at short time intervals depending on the "slow" or "fast" response settings. The datalogger has two mode settings: "standby" and "sampling". In the "sampling" mode the datalogger stores one sample per activated channel per second in the microprocessor. The stored values are used at the end of each sampling period to derive noise descriptors and statistical values. During sampling, an "omit sample" button may be depressed to exclude any noise contamination such as barking dogs, sirens or aircraft noise.

At the end of each noise measurement period, the datalogger prints out the channel number, date, site number, time sampling started, time sampling ended, number of samples lost (due to "editing" during measurement),  $L_{eq}$ ,  $L_{10}$ ,  $L_{50}$ , a histogram of noise levels vs. percent frequency, standard deviations, skewness, and kurtosis for each channel.

The datalogger also has the capability to measure maximum noise levels in either standby or sampling mode while a "peak" button is pressed. Upon release of the button, the maximum noise level received by each channel while the peak

button was depressed, is printed with the date, site number, time, and elapsed time of single event. The datalogger was used in this mode during this study.

A 50-foot reference microphone (mic 2) and SLM were also connected to a graphic level recorder (GLR). The GLR was used as a "valid peak" evaluation tool as will be discussed in the Field Measurements chapter.

Table VI-1 lists the instruments used in this study. Figure VI-1 shows the instrument setup.

Table VI-1

INSTRUMENTS USED IN THIS STUDY

Sound Level Meters

5 Bruel & Kjaer Type 2218 Precision SLM

Microphones

5 Bruel & Kjaer Type 4165 1/2" Microphones

Graphic Level Recorders

1 Bruel & Kjaer Type 2306 Portable GLR

Calibrators

1 Bruel & Kjaer Type 4230 1000 Hz, 94 dB Calibrator

Noise Data Acquisition System

1 ea. Datalogger Microcomputer made to specifications prepared by the Transportation Laboratory; the unit was manufactured by James Cox & Sons, Inc., Colfax, California, and Walt Winter of Engineering Logic, Sacramento, California.

Miscellaneous

1 ea. Range Master 715 (radar gun); Decatur Electronics, Inc. Wind Measuring Instrument; Belfort Instrument Company

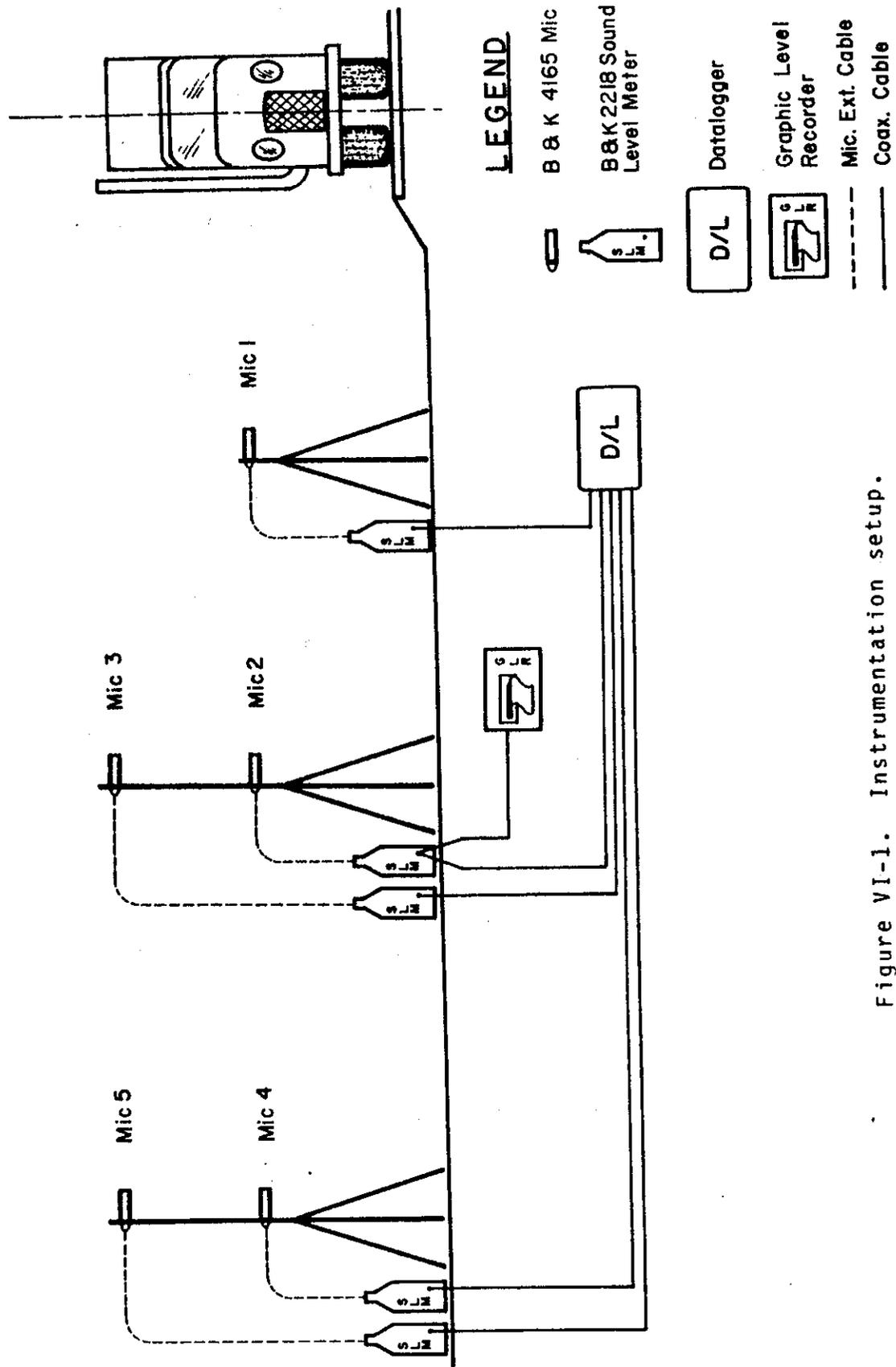


Figure VI-1. Instrumentation setup.

The SLM datalogger system was calibrated before and after each measuring period at each site by a field calibrator. The calibrator was periodically calibrated at the Caltrans Transportation Laboratory (TransLab) in Sacramento. TransLab has the facilities and instruments for performing sound equipment calibrations traceable to the National Bureau of Standards in Washington, D.C., via two Bruel and Kjaer 4160 one inch laboratory standard microphones. These microphones are sent alternately to NBS every six months to insure the availability of a recently calibrated standard microphone at the TransLab.

## VII. SITES

### Site Selection and General Requirements

All selected sites for this study were in conformance with emission level site criteria set forth by FHWA-OEP/HEV-78-1 (8) and FHWA-DP-45-1R(3). In addition to these physical criteria, the following general requirements were strived for during the selection process:

- °Adequate representation of hard and soft sites as defined by FHWA-RD-77-108(2).
- °Adequate geographical representation of vehicles.
- °Adequate speed representation.

These site criteria and requirements will be discussed in greater detail.

Physical Criteria. The following physical criteria were imposed on the sites:

1. The site shall be open without obstacles or large reflecting surfaces within 100 feet of either the vehicle path or microphone positions.
2. The ground surface at the microphones shall be no more than 2 feet above or below the roadway elevation or the plane of pavement (if the cross slope, crown or superelevation is significant).

3. The ground surface elevations along a line perpendicular to the roadway and passing through all microphones shall not vary more than 2 feet parallel to the plane of pavement.
4. The ground within the measurement area may be hard or soft as defined in FHWA-RD-77-108(2).
5. The roadway pavement shall be either concrete or asphalt concrete, dry, and in good condition.
6. The site shall not be near other significant noise sources such as heavily travelled frontage roads, ramps, construction, aircraft, etc.
7. The site shall not be near intersections, lane mergings or any other features that would cause traffic to slow down or speed up. Traffic has to pass at constant speed.
8. Other criteria are discussed in Chapter VIII, Field Measurement Methodology, under Typical Instrument Set Ups.

Hard and Soft Site Representation. Of the sixteen sites selected, five were considered hard sites (sites 2, 9, 11, 12, 14), and eleven soft (sites 1, 3, 5, 6, 7, 10, 15, 16, 17, 18, 19). The effects of hard vs. soft sites on noise levels measured at 50-foot reference distance will be discussed in Chapter X, Data Analysis and Results.

Geographical Representation. California is a large and diverse state with many different types of traffic. Truck traffic, for example, consists of various types: interstate, urban industrial, rural agricultural, etc. In order

to get representative samples of the state's traffic, a few samples were taken at many sites rather than the opposite.

In California, the FHWA Highway Traffic Noise Prediction Model is used mainly with higher speed traffic in urban and suburban regions. Geographical representation was therefore concentrated on these regions. Adequate high speed representation of automobiles and heavy trucks was obtained by sampling in the following areas:

1. Sacramento and vicinity.
2. San Francisco Bay area.
3. Los Angeles/Ventura area.
4. San Diego and vicinity.
5. San Bernardino/Riverside area.

Site selection was limited to the outskirts of the above urban regions to avoid congested traffic conditions.

Low speed traffic and all medium trucks were not necessarily represented geographically because of the relative difficulty in obtaining enough samples. Low constant speed traffic was generally difficult to find. Medium trucks were also relatively scarce.

#### Site Locations and Descriptions

Selected noise sites were numbered sequentially, in the order of measurement. A total of nineteen sites were originally selected. However, three sites - sites 4, 8 and 13 - were not used. Site 4 was a Caltrans test site at the California Highway Patrol Academy. Some limited passby noise measurements were made for another research project

at this site, using a medium truck and auto at various speeds. It was decided not to include the data in this study because the single medium truck and auto were not representative of the California vehicle population.

The sequential number at site 8 was assigned just before measurement. Because of adverse weather conditions, no measurements were made at site 8. Subsequent measurement attempts were also foiled by inclement weather.

Measurements were made at site 13 in the Mojave Desert. Later it was discovered that the roadway is on a 3% grade. This fact went unnoticed at first because the entire desert floor in the area is along an average 3% incline. Profile elevations taken after the noise measurements exposed the gradient.

Although sites 4, 8 and 13 were eliminated, the remaining sites were not renumbered to avoid confusion and maintain correlation with the original data. In addition to the sequential numbers, the sites were also given names.

General site locations are shown in Figure VII-1, followed by detailed location descriptions in Table VII-1 Cross sections, layouts and area maps are shown in Appendix A.

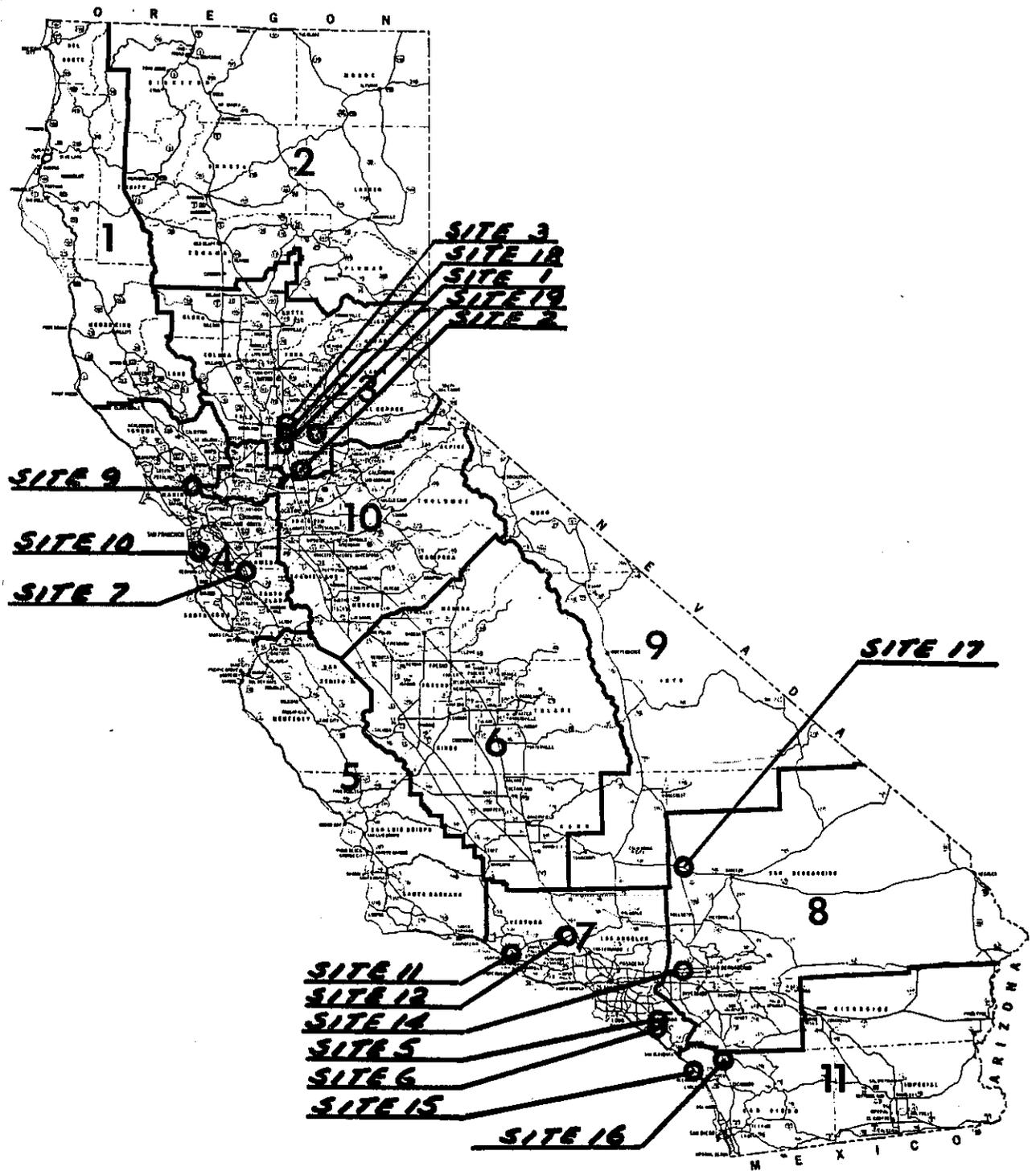


Figure VII-I Locations Of Noise Measurement Sites

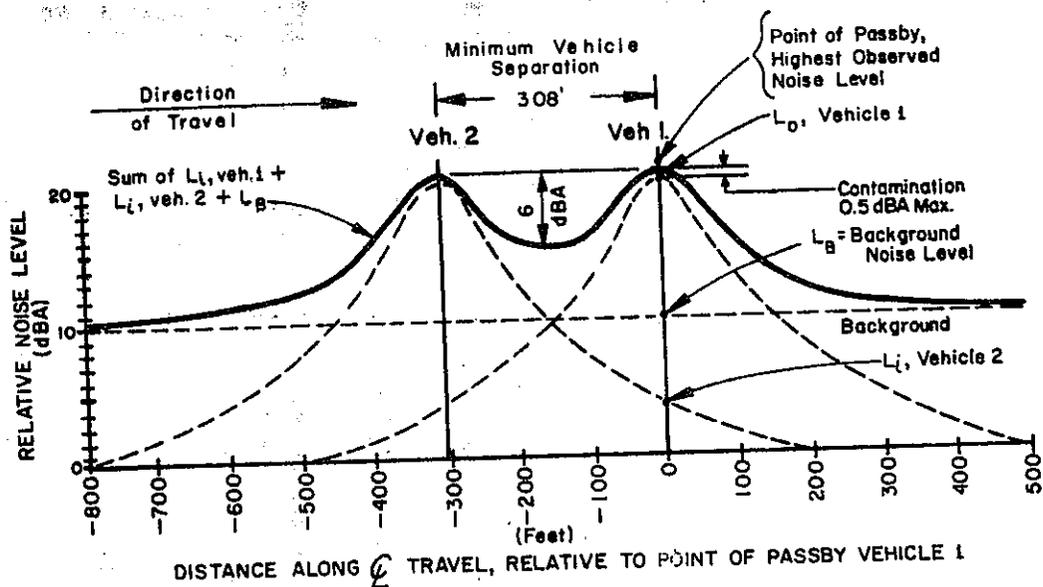


Figure VIII-5. Minimum separation between two vehicles, equal noise sources ( $L_0 = 20$  dBA Rel. Noise Level); background noise level ( $L_B = 10$  dBA R.N.L. ( $D_0 = 50'$ )).

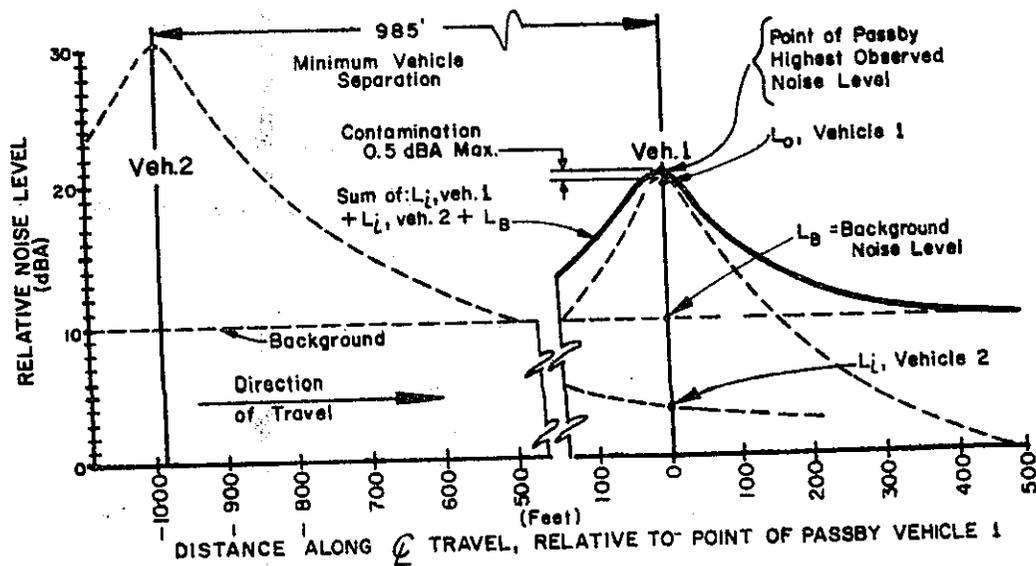


Figure VIII-6. Minimum separation between two vehicles, unequal sources ( $L_0$  veh. 1 = 20 dBA;  $L_0$  veh. 2 = 30 dBA, background noise level ( $L_B = 10$  dBA Relative Noise Level ( $D_0 = 50'$ )).

TABLE VII-1 SITE LOCATIONS (Con't.)

SITE I.D.		SITE LOCATION				Description	Date(s) Measured	Hard or Soft
No.	Name	Dist.	County	Route, Street	P.M.			
8*								
9	Weigh- Station	4	Son	37	2.51	Eastbound Rte 37, south side, 0.5 mi. east of Lakeville Rd., at old weigh-station, approx. 6 mi. east of Rte 101 and Novato.	1-11-83	Hard (Pavement)
10	Hills- borough	4	SM	280	15.1	Southbound I-280, 1 mi. north of Black Mountain and Hayne Rd. in Hillsborough	1-12-83	Soft
11	Kimball	7	Ven	126	2.8	Eastbound Rte 126, 200 ft+ east of Kimball Rd. overcrossing, City of Ventura.	2-8-83	Hard (Pavement)
12	Indian Dunes	7	LA	126	3.7	Eastbound Rte 126, south side, 2.1 mi. west of I-5, 0.4 mi. west of bridge No. 53-93 (Castaic Creek), 3.7 mi. east of Ventura Co. Line.	2-9-83	Hard (Dirt)
13*								
14	San Sevaine	8	Sbd	15	7.68	Southbound I-15, 5.3 mi. north of I-10, at bridge No. 54-9641-San Sevaine wash, 0.4 mi. south of Rte 30, in Etiwanda.	2-11-83	Hard (Pavement)
15	Oceanside	11	SD	5	59.4	Northbound I-5, at rest area, large space between I-5 and rest area, 6 mi. north of Rte 76 and Oceanside.	2-15-83	Soft

\* = Not Used (see text for reason)

TABLE VII-1 SITE LOCATIONS (Con't.)

SITE I.D.		SITE LOCATION				Date(s) Measured	Hard or Soft
No.	Name	Dist.	County	Route, Street	P.M.		
16	Half Fifteen	11	SD	15	R48.0	Southbound I-15, 1.5 mi. north of Rte 76 overcrossing, approx. 16 mi. north of Escondido.	2-16-83 Soft
17	Kramer Junction	8	Sbd	58	6.8	Eastbound Rte 58, south side 1.4 mi. of Rte 395, at entrance of dirt road; at old wood post: "State Hwy 466".	2-17-83 Soft
18	Richards	3	Sac	Richards Bl.	-	Westbound Richards Bl, north side, 0.05 mi. west of N. 3rd St. and 0.2 mi. east of I-5, in North Sacramento.	8-30-83 1-19-84 Soft
19	Sunrise	3	Sac	Sunrise Bl.	-	Northbound Sunrise Bl., 0.3 mi. north of White Rock Bl. east side, 1.0 mi. south of Rte 50, near Ranch Cordova.	2-1-84 Soft

## VIII. FIELD MEASUREMENTS

### General Approach

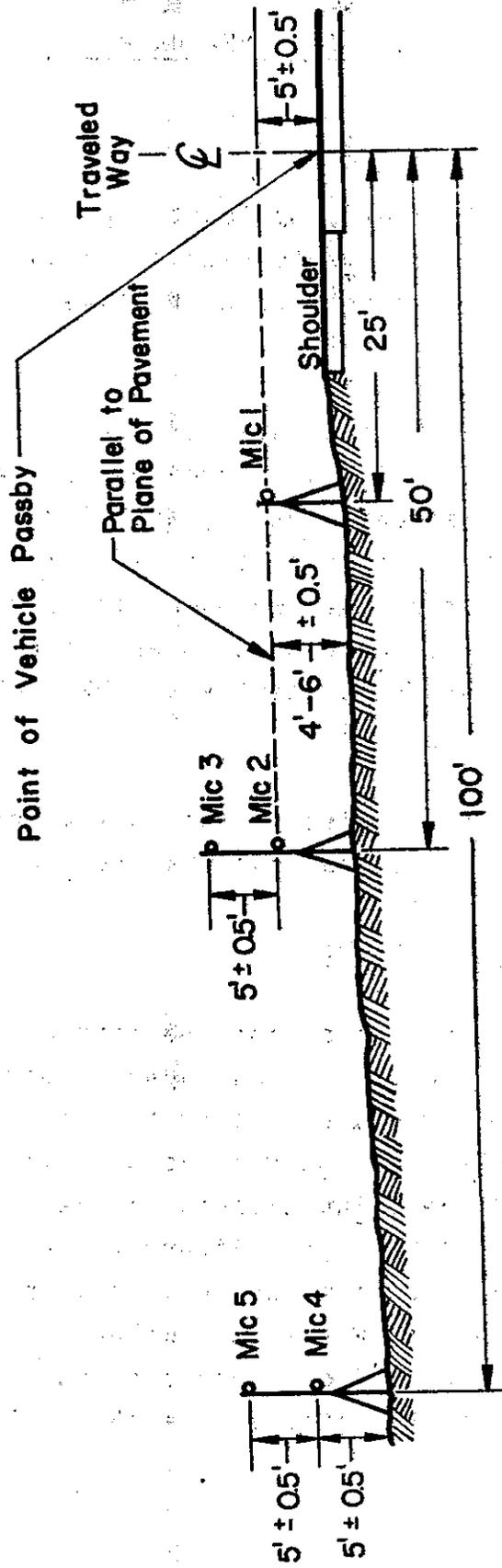
In the interest of safety, at least 2 persons were required to perform field measurements near the highways. Appendix B covers the general safety rules followed during measurements.

The field measurements consisted of three operations: 1) vehicle identification and speed measurements, 2) A-weighted noise measurements, and 3) meteorological measurements. The first operation was performed by a vehicle observer, the last two operations by an instrument operator. All measurement procedures and criteria reported in this chapter were consistent with FHWA-OEP/HEV-78-1(8) and FHWA-DP-45-1R(3).

The following sections discuss the instrument set-ups, measurement procedures and criteria used in this study.

### Typical Instrument Set-Ups

Where space and other conditions permitted the use of five mic's and SLM's, the typical microphone setup shown in Figure VIII-1, was used to measure highest noise levels of individual vehicles. These were assumed to occur when vehicles crossed the point closest to the mic's, called the "Point of (Vehicle) Passby". Figure VIII-1 also shows, typical site cross section and setup criteria, including a mic numbering convention used throughout the study, distances from the centerline of vehicle travel and mic height criteria. Mic height criteria were obviously linked to



\*Three mic. setup is identical, except for elimination of mic.'s 4 and 5

Figure VIII-1. Typical setup, five microphones\*.

cross section criteria discussed in the preceding chapter. Nine sites (Nos. 1, 2, 5, 7, 11, 12, 15, 16, 17) had the typical setup shown in Figure VIII-1. Of these, there was one exception, site 5. At this site, mics 4 and 5 were located 75 feet from the centerline of traveled way, instead of the typical 100 feet.

At each of the seven remaining sites, the terrain did not allow a setup of five mic's. At these locations a setup of three mic's was used. Except for the elimination of mic's 4 and 5, the mic location criteria and numbering convention for three mic setups were identical to those shown in Figure VIII-1. Sites 3, 6, 9, 10, 14, 18 and 19 had a three mic configuration.

Figure VIII-2 shows a typical site layout with mic clearances for 3 and 5 mic setups. Actual mic heights, distances, site cross sections, and layouts at each site are illustrated in Appendix B.

The typical setup of five mic's was designed to:

- °Include site and setup criteria set forth by FHWA-OEP/HEV-78-1(8).

- °Include the 50-foot reference distance for energy mean emission level determination(2,8).

- °Include a 100-foot distance to measure noise drop-off rate as a function of site type (hard site vs. soft site), and wind direction.

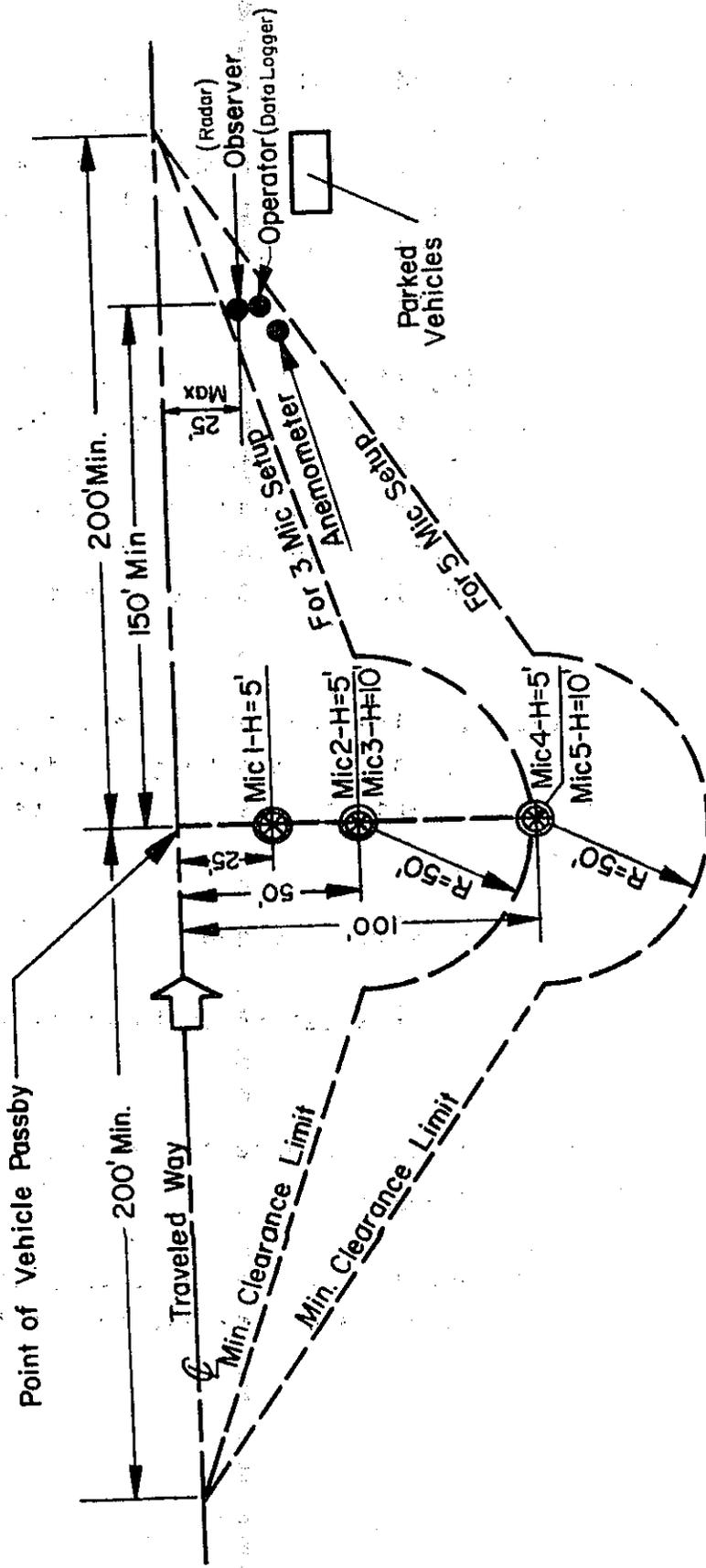


Figure VIII-2. Typical site layout and microphone locations.

°Include average mic heights of 5 and 10 feet at both the 50- and 100-foot distances, to investigate ground attenuation.

Except for the elimination of the 100-foot distance (mic 4 and 5), the above items also apply to the three mic setups.

### Event Quality and Contamination Control

In this report, an event is defined as the set of vehicle, noise, and environmental measurements of a vehicle passby. One of the most challenging problems in measuring vehicle noise emission levels was to insure that measurements were not significantly contaminated by background noise. For the purposes of this report, background noise is defined as the combined noise level of all on and off highway noise sources received by a microphone during a vehicle passby (event), excluding the vehicle passing by and in some instances, such as vehicle separation criteria (discussed in the next section), another designated vehicle. Contamination was especially difficult to avoid for autos because of their relatively high volumes and low noise emission levels compared to trucks.

The quality of the single passby events was maintained by using three noise contamination control strategies:

- 1) selecting vehicles that were adequately separated from other vehicles,
- 2) analyzing the GLR trace for compliance with "valid peak" criteria, and
- 3) audio-visual observation by the radar observer and instrument operator.

Strategies number 1 and 3 were enforced in the field at the time of the measurements. Determination of "valid peaks" was done later in the office. The three strategies will be discussed in detail in the following three sections.

Vehicle Separation Criteria. Figures VIII-3 through VIII-6 show a progressive development of the minimum vehicle separation criteria used during field measurements.

When a vehicle approaches the point of passby at a constant speed, the observed noise level at a microphone is related to the vehicle position as follows:

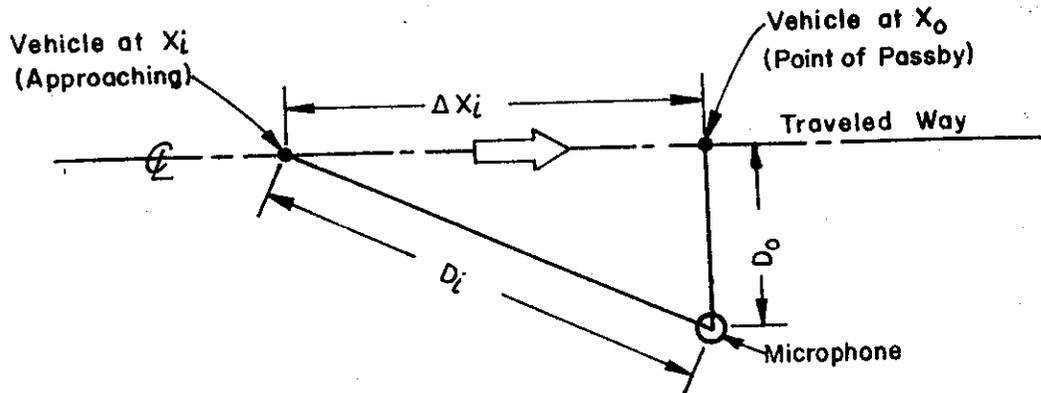
$$L_i = L_0 - 20 \log \frac{\sqrt{\Delta X_i^2 + D_0^2}}{D_0}. \quad (\text{Figure VIII-3})$$

where:  $L_i$  is the noise level at vehicle position  $X_i$ .  
 $L_0$  is the highest observed noise level at vehicle position  $X_0$ , the point of passby.  
 $\Delta X_i$  is the distance between position  $X_i$  and  $X_0$ .  
 $D_0$  is the distance from microphone to  $X_0$ .

This relationship is based on two assumptions: 1) the vehicle is a point source, and 2) there is no ground attenuation of the noise.

Figure VIII-4 is a plot of relative noise levels ( $L_0=20$  dBA) vs.  $\Delta X_i$  for the case of  $D_0=50$  feet. Note that this plot is representative of a point source traveling at a constant speed, with the microphone positioned 50 feet from the centerline of travel. This distance coincides with the reference distance of 15 meters for the National Reference Energy Mean Emission Levels per FHWA-RD-77-108(2).

The noise level vs. vehicle position plot in Figure VIII-4 was used in determining the minimum separation distances between two vehicles in two scenarios approximating conditions (Figures VIII-5 and VIII-6). The first scenario



When Vehicle is at  $X_0$ :

Highest observed noise level =  $L_0 =$   
Noise Emission Level

When Vehicle is at  $X_i$ :

Observed noise level,  $L_i = L_0 - 20 \text{ Log } \frac{D_i}{D_0} =$

$$L_i = L_0 - 20 \text{ Log } \frac{\sqrt{\Delta X_i^2 + D_0^2}}{D_0}$$

(Assuming point source)

Figure VIII-3. Vehicle noise level as a function of vehicle position.

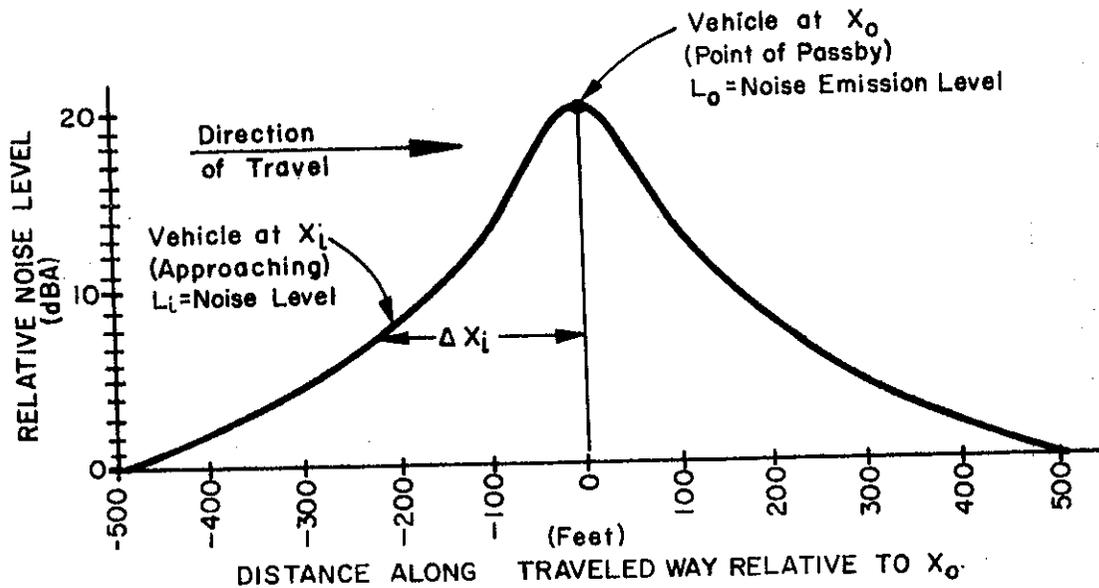


Figure VIII-4. Relative noise level vs. vehicle position (Microphone distance from  $\perp$  travel,  $D_0 = 50$  feet).



(Figure VIII-5), illustrates two vehicles with equal noise source strengths, and a "background" noise level ( $L_B$ ) of  $L_0 - 10$  dBA. The two vehicles are separated by a minimum distance so that the highest observed noise level includes no more than 0.5 dBA contamination when vehicle 1 crosses the point of passby. Because of the symmetrical relationship between the two noise sources, the same contamination is present when vehicle 2 crosses the point of passby. A GLR documenting the events would produce a trace similar to the solid line in Figure VIII-5 depicting the sum of  $L_i$  vehicle 1 +  $L_i$  vehicle 2 +  $L_B$ . This scenario approximates the passing of two autos without the presence of trucks, and may also be applied conservatively to the passing of two trucks. The minimum distance of 308 feet between the vehicles provides a criterion of separation when two vehicles of equal noise source are involved.

Because of uncertainties in actual background levels, and the fact that usually more than two vehicles were in the vicinity, the minimum distance criterion between the measured vehicle and any other vehicle of approximately equal source was set at 400 feet. A traffic cone placed 400' ahead of the point of passby aided the observer in estimating the minimum distance criterion in the field.

The second scenario, shown in Figure VIII-6 involves two vehicles of unequal source strength. In this scenario, the noise source of one vehicle is 10 dBA higher than that of the other vehicle. The background noise is assumed to be 10 dBA below the lower noise source. This scenario approximates that of measuring the noise emission level of an auto while a truck is approaching. In this case, the

minimum vehicle separation should be 985 feet, or approximately 1000 feet, to avoid contamination of more than 0.5 dBA.

The observer in the field had to estimate the 1000-foot distance when the second scenario applied. Usually this did not present a problem. Most auto measurements were taken when there were no trucks in sight. In the cases where trucks were present, the observer and instrument operators made independent judgements as to the measurement quality. Because of the probable presence of considerable ground attenuation and some atmospheric attenuation over a 1000-foot distance (not included in the criterion calculation), this criterion was probably conservative.

Finally, a short discussion about the reverse of scenario 2 (Figure VIII-6) should be included. In this scenario the louder vehicle is measured and the quieter vehicle is in the vicinity. If the difference between the sources is 10 dBA or greater, no separation should be necessary when two vehicles are involved. However, when the louder source is surrounded by several quieter sources, contamination may still occur. No criteria were set to cover this situation, but in general, trucks were not measured with more than two or three autos in the immediate vicinity. In most cases, trucks selected for measurement were adequately separated from autos so that few judgments were necessary.

The vehicle separation criteria used for the field measurements were all for the 50-foot microphone positions. Examination of Figures VIII-3 through VIII-6 indicate that these criteria will always satisfy the 25-foot, but not the 100-foot mic positions. However, mics 4 and 5 were not

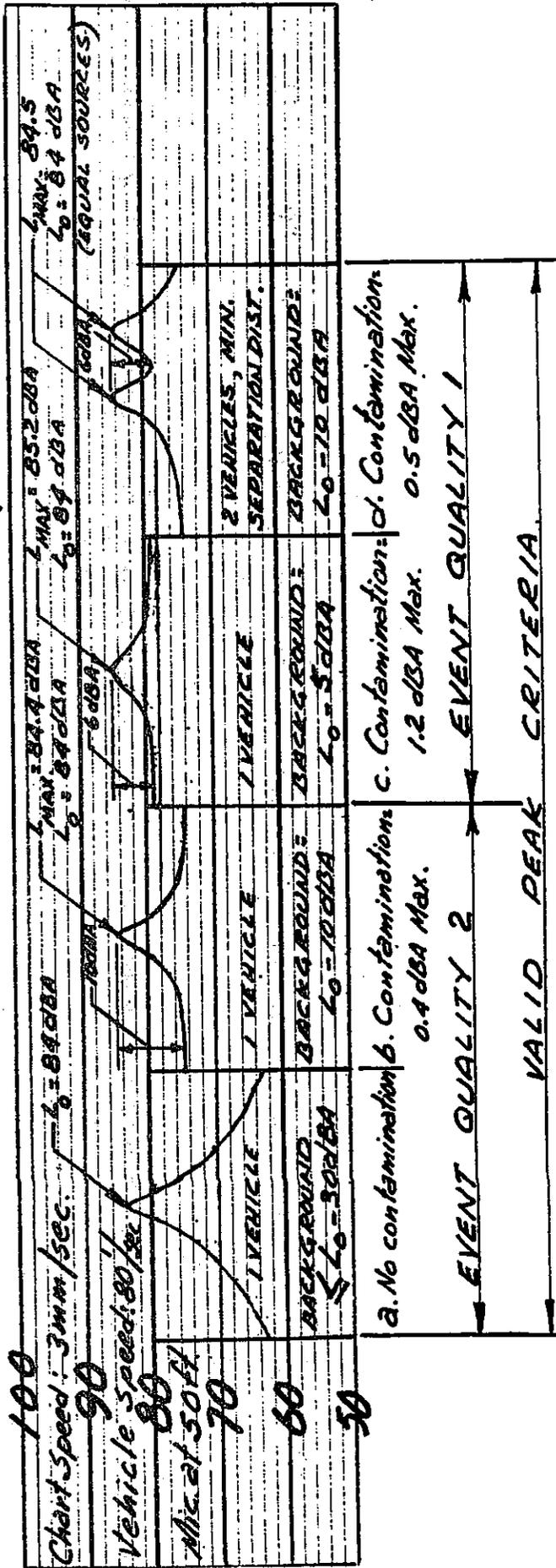
used for emission level measurements. The purpose of the 100-foot noise measurements was to determine the effects of terrain and wind. Other criteria were used to evaluate the quality of those measurements at the 100-foot distance as shall be discussed in the next section.

Valid Peak Criteria. Due to uncertainties in background noise levels (defined in the previous section) at the time of measurement, vehicle separation criteria by themselves were not sufficient insurance against contamination. Valid peak criteria were developed to help determine whether background noise contributed to the highest observed noise level of each event (vehicle passby). These criteria were based on a GLR trace of the event, recorded at 50 feet from the centerline of vehicle travel at a mic height of 5 feet (Ref mic 2 location).

In order to limit contamination to less than 0.5 dBA, the background noise levels should be at least 10 dBA lower than the highest observed value. This would have been a convenient criterion to use. A study by the New Jersey Department of Transportation(11), however, suggests that accepting only peaks of 10 dBA or greater would introduce a bias toward noisier vehicles. This is especially true when background noise is relatively high. The New Jersey study used a rise and fall criterion of 6 dBA to prevent this bias, at the risk of slightly contaminating the measurement.

Figure VIII-7 shows GLR traces of four passby scenarios and their associated valid peak criteria. Scenario "a" illustrates a single vehicle passby at 54.5 mph (80 feet/sec), with a background noise level of 30 dBA or more below its

Figure VIII-7 Valid Peak And Event Quality Criteria



- NOTES:
- $L_0$  = Vehicle Noise Emission Level
  - $L_{MAX}$  = Highest Observed Noise Level.
  - Contamination =  $L_{MAX} - L_0$
  - When  $L_{MAX} - BACKGROUND LEVEL < 6 dBA$ , event was rejected. (Event quality 0)

noise emission level,  $L_0$ , of 84 dBA. This trace is unaltered by any background noise. Scenario "b" depicts the same single event with a steady background noise level of  $L_0 - 10$  dBA. Note that the highest observed noise level,  $L_{max}$ , is 84.4 dBA and the measurement is contaminated by  $L_{max} - L_0 = 0.4$  dBA.

Scenarios "a" and "b" comprise "event quality 2". Quality 2 events represent the least contaminated events. They were used for all analyses, including those made for the 100 ft mic's. The criterion for quality 2 events is a peak that rises 10 dBA or more above the background noise level, measured by a SLM and GLR at a 50 ft distance and 5 ft mic height.

Scenario "c" shows contamination caused by a relatively steady background noise of  $L_0 - 5$  dBA. The contamination is 1.2 dBA above the background. Scenario "d" illustrates the trace of two vehicles of equal source strength, at the minimum separation distance discussed in the previous section. A steady background noise level of  $L_0 - 10$  dBA is assumed. As shown in Figure VIII-5, the peaks are separated by a 6 dBA valley, and contamination is 0.5 dBA. Scenarios "c" and "d" were grouped into "quality 1" events. These events were used only for emission levels analyses up to and including the 50-foot microphones. Quality 1 events were not used to analyze the noise levels measured at the 100-foot distance. The criterion for quality 1 events is a peak that rises 6-9 dBA above the background. Note that minimum vehicle separation criteria are under no circumstances in conflict with the quality 1 criterion.

Peaks that rose less than 6 dBA above background were coded event "quality 0" and later ignored in computer analyses.

Audio-Visual Observation. The preceding two methods of controlling noise measurement contamination - the vehicle separation and valid peak criteria - were objective criteria that required a minimum amount of judgment. Rigid compliance with the criteria appeared to be sufficient insurance against contamination in most cases. In some instances, however, it was necessary to apply subjective, on-the-spot judgment to determine the quality of an event. In these instances, judgments were made through audio-visual observations, i.e., using ears and eyes. Common examples included: sudden rises in background noise during measurements, due to aircraft, nearby construction, sporadic traffic on nearby frontage roads or ramps. When these rapid background noise increases coincided with vehicle passby measurements, they sometimes blended in with GLR traces, and showed valid peaks. Contamination would have gone undetected except for the alertness of the observers during measurements.

Other Event Criteria. In addition to the three contamination control strategies described in the previous sections, there were other factors governing rejection or acceptance of events. These included, but were not necessarily limited to: change of speed during passby, sudden change in environmental conditions (e.g., wind gusts), unusual vehicles, and measurement errors. Criteria for some of these factors will be discussed in the vehicle criteria, environmental criteria, and measurement procedure sections.

Number of Events Accepted and Rejected. When an approaching vehicle was judged to be a likely event, measurement began and a sequential number was assigned to the event. After the vehicle had passed, an evaluation was made using all previously described criteria. The data were recorded, whether the event was rejected or not. If rejected, the reason for rejection was coded on either the GLR trace, vehicle observation sheet, data logger printout or environmental data sheet. A rejection on one or more of these four data sources was treated as an event quality "0" and the event was ignored in later computer analyses. If the event was accepted it was given a quality 1, except in the valid peak evaluation, where it was assigned either a quality 1 or 2 as previously discussed. For convenience, combinations of qualities 0,1 and 2 and 0, 1 will be called event quality 0, (e.g., 2011 = 0), the combination 2111 will be referred to as quality 2, and the remaining combination 1111 will be called quality 1.

Of the total of 3045 vehicles measured at mic 2 (50 ft reference mic), on level roadways, the following statistics were derived by quality:

Quality 2 events	-	2426	or	79.7%	(Accepted)
Quality 1 events	-	308	or	10.1%	(Accepted)
Quality "0" events	-	311	or	10.2%	(Rejected)

Of the above 2734 accepted events, 88.7% were quality 2 and 11.3% quality 1.

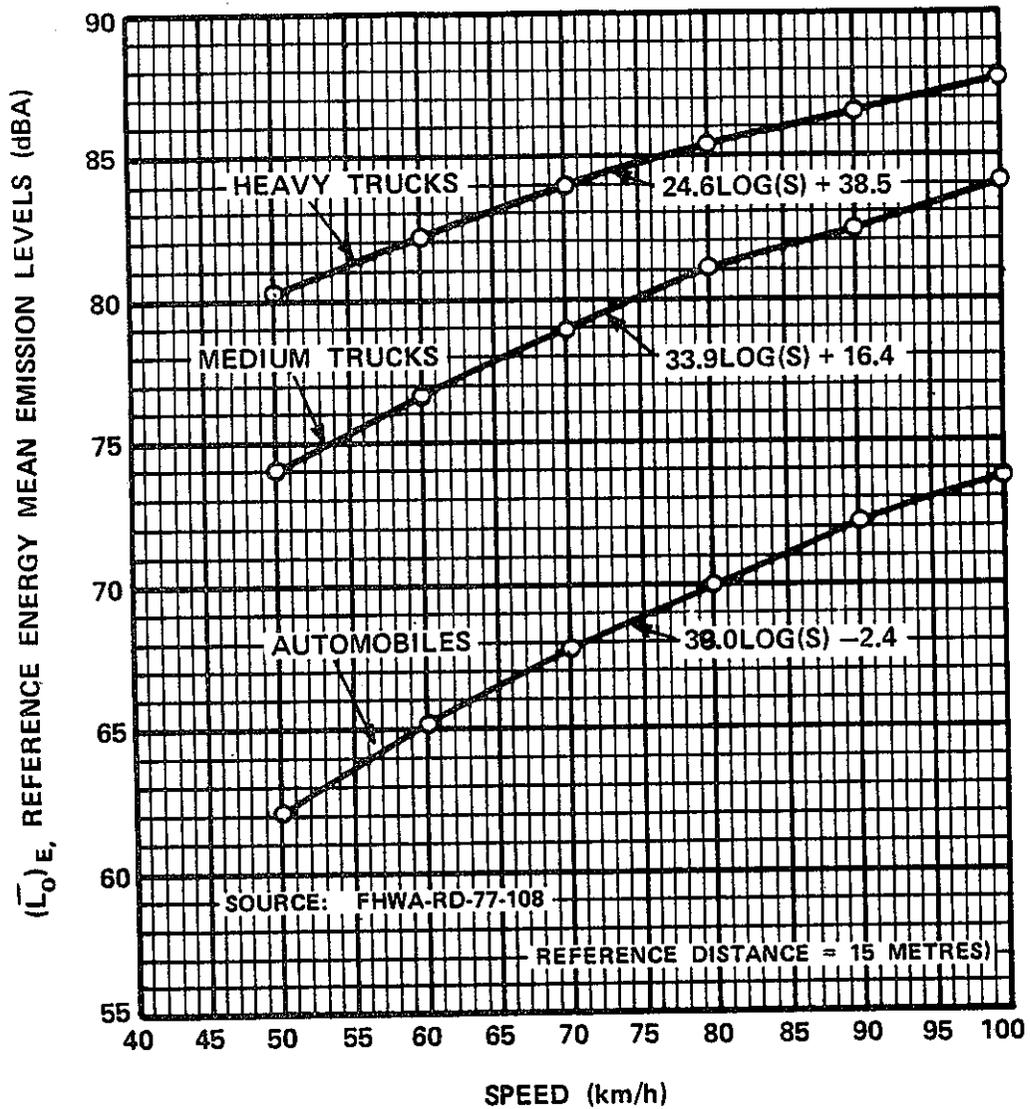
## Sample Size

For the purposes of determining the sample sizes required for each major vehicle group considered for emission level curves, the following criteria were set:

1. Total speed range from 25 mph to 65 mph.
2. Subdivision of the 40 mph range into equal sized intervals (speed classes) small enough to insure that any noise value along the curve inside the speed class is within +1 dBA from the mean noise value in that speed class.
3. 95% confidence interval for the mean of each speed class of 1 dBA.

The National Reference Energy Mean Emission Level curves (Figure VIII-8) per FHWA-RD-77-108(2) were examined to estimate the speed class size necessary to satisfy above criterion No. 2. Due to its steep slope, the lower end of the automobile curve was selected to represent the greatest change in noise levels with speed. From 50 km/hr to 56.5 km/hr the FHWA auto emission levels increase 2.0 dBA, or +1 dBA from the mean level at the 53.25 km/hr center point. A 6.5 km/hr (4 mph) interval would therefore satisfy criterion 2.

The following speed classes were designed to cover the entire range of desired speeds:



**LEGEND:**

1. AUTOMOBILES: ALL VEHICLES WITH TWO AXLES AND FOUR WHEELS.
2. MEDIUM TRUCKS: ALL VEHICLES WITH TWO AXLES AND SIX WHEELS.
3. HEAVY TRUCKS: ALL VEHICLES WITH THREE OR MORE AXLES.

**National Reference Energy Mean Emission Levels as a Function of Speed**

Figure VIII-8 (Extracted from FHPM 7-7-3)

Speed Class	Speed Range, mph	Speeds to Nearest 1 mph
0	<24.50	<25
1	24.50 - 28.49	25 - 28
2	28.50 - 32.49	29 - 32
3	32.50 - 36.49	33 - 36
4	36.50 - 40.49	37 - 40
5	40.50 - 44.49	41 - 44
6	44.50 - 48.49	45 - 48
7	48.50 - 52.49	49 - 52
8	52.50 - 56.49	53 - 56
9	56.50 - 60.49	57 - 60
10	60.50 - 64.49	61 - 64
	>64.49	>64

The minimum sample size for each vehicle group and each speed class was initially estimated from FHWA-OEP/HEV-78-1(8). According to the publication, minimum amount of samples using a 95% confidence interval of  $\pm 1$  dBA around the mean should be:

Autos - 28

Medium Trucks - 46

Heavy Trucks - 37

Another method for calculating a minimum number of samples for each vehicle group and speed class is:

$$n = \left[ \frac{Z_{\alpha/2}(\sigma)}{d} \right]^2 \quad (\text{Eq. 1})$$

where:  $n$  = minimum number of samples required.

$Z_{\alpha/2}$  = the amount of population standard deviations from the mean, associated with a  $(1.00-\alpha) \times 100\%$  confidence level.

$\alpha$  = significance level.

$d$  =  $(1.00-\alpha) \times 100\%$  confidence interval.

$\sigma$  = population standard deviation for a vehicle group and speed class

For  $d = 1$  dBA and  $\alpha = .05$  the formula reduces to:

$$n = (1.96\sigma)^2 \quad (\text{Eq. 2})$$

which may be used if  $\sigma$  is known.

After samples have been taken the minimum required number of samples may be calculated by:

$$n = \left[ \frac{(t_{\alpha/2; n-1})(S)}{d} \right]^2 \quad (\text{Eq. 3})$$

where:  $t_{\alpha/2; n-1}$  = the amount of sample standard deviations associated with (1.00- $\alpha$ ).100% confidence level and  $n-1$  degrees of freedom.  
 $S$  = the sample standard deviation.

Equation 3 was used in this study to determine whether enough samples were taken in each vehicle group and speed class. For a 95% confidence interval of  $\pm 1$  dBA the equation reduces to:

$$N = [(t_{.025; n-1})(S)]^2 \quad (\text{Eq. 4})$$

Table VIII-1 shows the number of events sampled (accepted events only) and the minimum required samples for each vehicle group and speed class. Note that for both autos and heavy trucks sufficient amounts of data were gathered above 32 mph in all speed classes, except for trucks above 64 mph. The mean noise levels for these speed classes are  $\pm 1$  dBA at 95% confidence levels. At 32 mph and below, however, insufficient amount of data were gathered, resulting in 95% confidence intervals of greater than  $\pm 1$  dBA.

TABLE VIII-1

NUMBER OF EVENTS SAMPLED AND MINIMUM REQUIRED\*  
BY VEHICLE GROUP AND SPEED CLASS

Speed Class	Speed Range (mph)	Autos		Medium Trucks		Heavy Trucks	
		Events Sampled	Minimum Required	Events Sampled	Minimum Required	Events Sampled	Minimum Required
0	<25	3	**	1	**	3	**
1	25-28	6	**	7	**	18	50
2	29-32	21	25	8	45	37	49
3	33-36	46	37	20	50	40	32
4	37-40	33	39	15	48	34	22
5	41-44	88	34	16	31	48	20
6	45-48	92	34	19	59	77	25
7	49-52	117	36	32	23	106	27
8	53-56	258	28	69	29	233	31
9	57-60	272	31	78	23	300	21
10	61-64	220	27	44	24	212	23
11	>64	107	35	8	8	46	85
All Speeds		1263		317		1154	

\*95% confidence interval of  $\pm 1$  dBA around mean of speed class.

\*\*Unable to determine accurately.

For medium trucks the minimum amount of samples required was reached only for all speed classes above 48 mph.

The above minimum sample size criteria affected the confidence intervals for each speed class. For curve fitting, different methods were employed for the calculation of regression line confidence "bands". These will be discussed in Chapter X, Data Analyses and Results.

#### Vehicle Types and Speed Criteria

The three vehicle groups discussed in FHWA-RD-77-108(2) are the automobiles, medium trucks and heavy trucks. They were defined as follows:

Automobiles - all vehicles having two axles and four wheels and designed primarily for transportation of nine or fewer passengers (automobiles), or transportation of cargo (light trucks). Generally, the gross vehicle weight is less than 4500 kg (9900 lb).

Medium trucks - all vehicles having two axles and six wheels and designed for transportation of cargo. Generally, the gross weight is greater than 4500 kg (9900 lb) but less than 12,000 kg (26,400 lb).

Heavy trucks - all vehicles having three or more axles and designed for the transportation of cargo. Generally, the gross weight is greater than 12,000 kg (26,400 lb).

These definitions were used throughout this study. However, for the purposes of confirming that vehicles can be placed in these three acoustic source groups, vehicles were identified in greater detail than the above groups. Automobiles were divided into compact and standard categories. This division was made subjectively in the field by the observer. Heavy trucks were categorized by number of axles. The subdivisions resulted in eight vehicle types which are defined in Table VIII-2.

All events were identified in the field and recorded with the passby speeds in miles per hour. The speeds were measured with a radar gun by the observer beginning at a point approximately 400 feet ahead of the point of passby, and ending just beyond the point of passby. The speed at the point of passby was recorded. If the speed changed more than 3 mph in the 400-foot distance, the vehicle was assumed to be accelerating or decelerating and the event rejected. A gradual 3 mph speed change in 400 feet at an average speed of 65 mph corresponds with an acceleration or deceleration of approximately 0.7 mph/sec ( $1.0 \text{ ft/sec}^2$ ). Abrupt changes in speed, such as a 3 mph change in the last 100 feet before the point of passby, were assessed subjectively on an individual basis.

The vehicle observer was positioned 25 feet from the centerline of travel way and 150 feet beyond the point of passby. This position was chosen to insure an accuracy within 1 mph of the radar gun reading. The radar gun uses the "Doppler effect" and is most accurate when vehicle travels in the same line with the observer. A feat that,

TABLE VIII-2

## VEHICLE TYPES

Vehicle Type	Designation	Definition/Description	FHWA-RD-77-108 Designation
0	Compact Auto	Four cylinders - otherwise same as FHWA automobiles.	Auto
1	Standard Auto	Six or eight cylinders - otherwise same as FHWA automobiles.	Auto
2	Medium Truck	Same as FHWA medium trucks includes 2-axled, 6-tire busses.	Medium Truck
3	3-Axle Truck	Three axles - otherwise same as FHWA heavy trucks.	Heavy Truck
4	4-Axle Truck	Four axles - otherwise same as FHWA heavy trucks.	Heavy Truck
5	5-Axle Truck	Five axles - otherwise same as FHWA heavy trucks.	Heavy Truck
6	>5-Axle Truck	More than five axles - otherwise same as FHWA heavy trucks.	Heavy Truck
7	Miscellaneous	Vehicles not covered under types 0-6. Example: motorcycles	-

obviously, cannot be achieved safely. When not in line with the vehicle's path, the true speed,  $S_t$ , can be calculated from the apparent speed,  $S_a$ , by

$$S_t = \frac{S_a}{\cos\theta},$$

where  $\theta$  is the angle between line of travel and line of sight between radar gun and the target vehicle. At 150 feet or more from the point of passby and no more than 25 feet from the centerline,  $\theta$  is small enough for  $S_t$  to approximate  $S_a$ .

### Environmental Measurements and Criteria

One of the objectives of this project was to attempt to isolate the effects of wind on vehicle noise emission measurements and noise measurements in general. FHWA-OEP/HEV-78-1(8) and FHWA-DP-45-1R(3) do not recommend taking noise measurements when wind speeds exceed 19 km/hr (12 mph). All measurement in this study were made at wind speeds below 10 knots (11.5 mph).

Wind speeds and direction were measured with a Belfort anemometer set on top of a 7-foot standard near the instrument operator and observer, at a distance of approximately 25 feet from the centerline of the nearest roadway. The measurements were taken between measured events and gaps in traffic to avoid turbulence from passing vehicles.

Wind speeds were measured to the nearest 1 knot, and then grouped in three wind speed classes. Table VIII-3 shows these classes.

Table VIII-3

Wind Speed Class	Range (knots)	Range (mph)	Speed Used (mph)
0	0-2.5	0.3	0
3	2.5-5.5	3-6	4.5
6	5.5-10	6-12	9

The midpoint speed was later used to compute crosswind components 90° to the roadway.

Wind directions were measured to the nearest 10° azimuth. For the purpose of this study, wind directions were oriented with 0° wind directions blowing perpendicular to the roadway from noise source to receivers (roadway to microphones). See Figure VIII-9 for complete azimuth orientation.

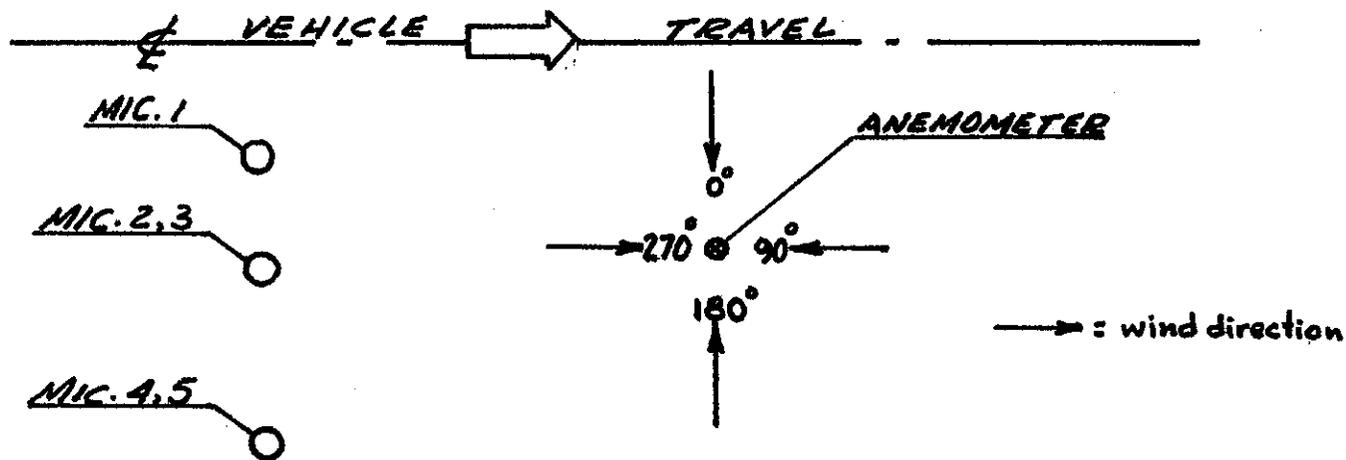


Figure VIII-9 Wind Direction Orientation

The crosswind components were calculated later by midpoint wind speed x cos (wind direction). Example: a wind speed class 3 at 250° direction would result in a cross wind component of 4.5 mph x cos (250°)=-1.5 mph. The minus sign means that the crosswind component is from receivers (mics) to source (roadway). The crosswind components thus calculated were subdivided into the following component intervals:

6 to 12 mph  
3 to 6 mph  
-3 to +3 mph  
-6 to -3 mph  
-12 to -6 mph

These intervals were later used to analyze the effects of wind on noise levels at the receivers.

Other important environmental criteria were 90% or greater relative humidity and wet pavement. No measurements were attempted under either condition.

If measurements had been made inadvertently during any of the described adverse environmental criteria, quality "0" would have been assigned to the events and the measurements would have been rejected. No rejections, however, were necessary for environmental reasons.

#### Measurement Procedures

After surveying the site and laying out the mic locations, the instruments were set up in accordance with the typical

setups discussed previously (Figures VI-1, VIII-1 and VIII-2). The SLM's were set on "A" weighted, and "fast" response. Fast response affects the DC output to which the datalogger was connected. The SLM's/datalogger and SLM/GLR system was then turned on and field calibrated. This procedure required 2 persons, one to place a calibrator on each mic and one to read the datalogger and adjust the GLR. SLM's were adjusted to the calibrator value read on the datalogger. The GLR, hooked up to the AC output of mic 2 SLM was then also adjusted to the value after the SLM adjustment. This procedure insured a system calibration including the datalogger and GLR rather than the SLM. Because of the separation between mics/SLM's and datalogger, radios were required for communication. Field calibration was performed after power was turned on and instruments warmed up. It was checked again before power was turned off. Once the system was turned on and calibrated, the power was usually not turned off until the end of the day. With few exceptions, the end-of-day calibration check was within 0.2-0.3 dBA of the values at the beginning of the day. The differences never exceeded 0.5 dBA.

After calibration, the instrument operator and vehicle observer took up positions approximately 150 feet beyond the point of passby and 25 feet from centerline, and began selecting potential events. Selection of a likely event was usually made as the vehicle approached the 400-foot marker (traffic cone) used for estimating the minimum vehicle separation distance. At the time the target vehicle passed the 400-foot marker, the instrument man activated the GLR connected to SLM and mic 2. At the same time, the vehicle observer began monitoring the target

vehicle speed with the radar gun. Approximately 200 feet from the point of passby the datalogger was activated by the instrument operator. When the target vehicle reached the passby point, the observer noted and recorded the vehicle's speed and identification. A short time after the vehicle had passed the instrument operator and observer positions, the datalogger and the GLR were deactivated. The observations were all marked with event numbers. Good communications needed to be maintained between the observer and the instrument operator to avoid event numbers getting out of phase between the datalogger printout, GLR chart and the vehicle observer sheet. Wind speeds and wind directions were observed by the instrument operator between events. Frequent observations guaranteed detection of wind shifts. If either wind speed or wind direction changed, the event number and the new wind data were recorded. Relative humidity measurements were taken only when there was uncertainty that the 90% criteria could be met, for example, in fog.

Figures VIII-10 through VIII-15 show examples of a vehicle observation sheet, GLR chart, datalogger printout and site/environmental data sheet.

CALIFORNIA VEHICLE NOISE EMISSION LEVELS - CALTRANS, TRANSLAB  
**VEHICLE OBSERVATION SHEET**

SITE NO: 16 (Husool) DATE: 2/16/82 NEW REPEAT   
 LOCATION: DIST. 11 CO. SD RTE. 15 P.M. 48.0  
 OBSERVER: KAY RECORDER: KAY No. of eye 76 O.C.

SHEET 3 OF 6  
 REMARKS:

EVENT NO.	AUTO'S		SPEED, MPH + REMARK CODE (see back of sheet)					OTHER OR UN-ID. H.T. (specify use code on back)
	COM	STD	2 AXLES 6 WHEELS	3 AXLES	4 AXLES	5 AXLES	> 5 AXLES	
101								
2								
3								
4								
5								
6								
7								
8								
9								
10								
11								
12								
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Figure VIII-10 Example Of Vehicle Observation Sheet  
 VIII-29

## CODES

### REMARK CODES

(Place behind speed in appropriate column, only if necessary).

C = Noise Contamination during measurement of event. (other traffic, aircraft, etc.)

S = Bad Speed (Accel./Decel., bad radar gun reading, interference, bad aim, etc.)

NV = Unusually Noisy Vehicle (clanging, vehicle hit bump, back fire, horn, etc.)

QV = Unusually Quiet Vehicle (coasting, in-between gears, etc.)

LC = Lane Change or Wrong Lane

W = Very Windy

WP = Wet pavement (due to sudden rain, sprinklers, etc.)

NG = No Good event due to any other reason. (Use typically for unusual cases, or if several of above items occur at same time)

### "OTHER" COLUMN CODES (Use only in "other vehicles" column)

B-3 = 3 AXLE BUS.  
(2 AXLE BUSES ARE M.T.'S)

MC = Motorcycle

MH = Large Motor Home  
(usually considered a M.T.)

HT = Unidentified Heavy Truck  
(Not sure of axle count)

SPECIFY OWN CODES BELOW: (For use in any column)

ADDITIONAL NOTES, COMMENTS, OR CLARIFICATIONS:

Figure VIII-11 Backside of Vehicle Observation Sheet

**CALIFORNIA VEHICLE NOISE EMISSION LEVELS - CALTRANS, TRANSLAB  
VEHICLE OBSERVATION SHEET**

SITE NO: 16 (1015001) DATE: 2/16/82 NEW REPEAT  SHEET 3 OF 6  
 LOCATION: DIST. 11 CO. SD RTE. 15 P.M. 48.0 REMARKS:  
SB I-15; 1.5 MI. NO. OF RTE 76 O.C.  
 OBSERVER: KAY RECORDER: KAY

EVENT NO.	SPEED, MPH + REMARK CODE (See back of sheet)							OTHER OR UN-ID. H.T. (Specify use code on back)
	AUTO'S 2 AXLE 4 WHEELS		MED. TRKS	HEAVY TRUCKS BY AXLES				
	COM	STD	2 AXLES 6 WHEELS	3 AXLES	4 AXLES	5 AXLES	> 5 AXLES	
101								
2		59						
3		61						
4						60		
5		63						
6						60		
7		65						
8		62						
9						59		
10		57						
111		66						
12		61						
13			57					
14		59						
15		71						
16						56		
17		70						
18		57						
19			56					
20						65		
121		65						
23		67						
23						53		
24		57						
25				57				
26			57					
27						57		
28		58						
29		67						
30						62		
31						57		
131			57					
32								
33		67						
34		57						
35			61					
36						57		
37						67		
38						57		
39		60						
40		68						
141		57						
42				57				
43		63						
44		57						
45								
46			57					
47						56		
48			59					
49		67						
150		60						

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 RWH

Figure VIII-10 Example Of Vehicle Observation Sheet  
 VIII-29

## CODES

### REMARK CODES

(Place behind speed in appropriate column, only if necessary).

- C: Noise Contamination during measurement of event. (Other traffic, aircraft, etc.)
- S: Bad Speed (Accel./Decel., bad radar/gun reading, interference, bad aim, etc.)
- NV: Unusually Noisy Vehicle (clanging, vehicle hit bump, back fire, horn, etc.)
- QV: Unusually Quiet Vehicle (coasting, inbetween gears, etc.)
- LC: Lane Change or Wrong Lane
- W: Very Windy
- WP: Wet pavement (due to sudden rain, sprinklers, etc.)
- NG: No Good event due to any other reason. (Use typically for unusual cases, or if several of above items occur at same time)

### "OTHER" COLUMN CODES

(Use only in "other vehicles" column)

- B-3: 3 AXLE BUS.  
(2 AXLE BUSES ARE M.T.'S)
- MC: Motorcycle
- MH: Large Motor Home  
(usually considered a M.T.)
- HT: Unidentified Heavy Truck  
(Not sure of axle count)

SPECIFY OWN CODES  
BELOW: (For use in any column)

**ADDITIONAL NOTES, COMMENTS, OR CLARIFICATIONS:**

Figure VIII-11 Backside of Vehicle Observation Sheet

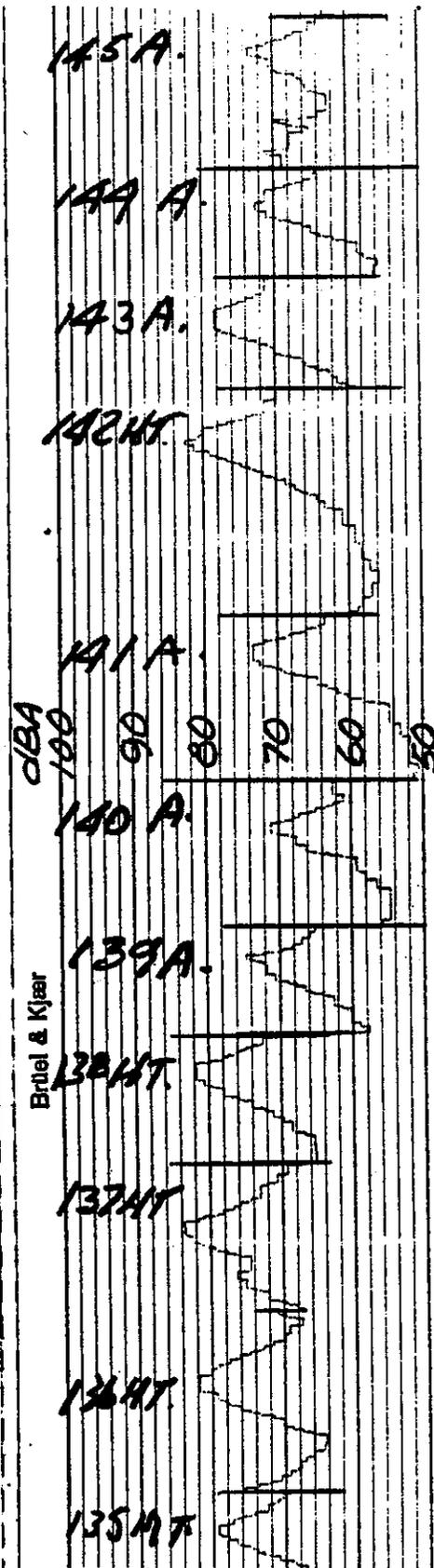


Figure VIII-12 Example  
Of Graphic Level Recorder  
Trace

```

++++ PEAK EVENT ++++
SITE      137
2/16/83   11:35:29
ELAPSED TIME  3.8 S
CH 1 = 91.01 DB
CH 2 = 84.19 DB
CH 3 = 84.56 DB
CH 4 = 75.81 DB
CH 5 = 78.23 DB

```

```

++++ PEAK EVENT ++++
SITE      138
2/16/83   11:36:08
ELAPSED TIME  4.2 S
CH 1 = 89.53 DB
CH 2 = 82.15 DB
CH 3 = 83.13 DB
CH 4 = 73.80 DB
CH 5 = 75.23 DB

```

```

++++ PEAK EVENT ++++
SITE      139
2/16/83   11:37:12
ELAPSED TIME  3.2 S
CH 1 = 80.27 DB
CH 2 = 74.21 DB
CH 3 = 75.23 DB
CH 4 = 65.90 DB
CH 5 = 68.55 DB

```

```

++++ PEAK EVENT ++++
SITE      140
2/16/83   11:38:45
ELAPSED TIME  4.8 S
CH 1 = 78.45 DB
CH 2 = 71.03 DB
CH 3 = 72.22 DB
CH 4 = 61.73 DB
CH 5 = 65.38 DB

```

```

++++ PEAK EVENT ++++
SITE      141
2/16/83   11:39:50
ELAPSED TIME  3.2 S
CH 1 = 81.23 DB
CH 2 = 73.53 DB
CH 3 = 74.89 DB
CH 4 = 65.76 DB
CH 5 = 68.21 DB

```

Figure VIII-13 Example  
Of Datalogger Print Out

CALIFORNIA VEHICLE NOISE EMISSION LEVELS - CALTRANS, TRANSLAB  
**NOISE MEASUREMENT & SITE DATA (BACK SIDE)**

SITE NO: J6 (11015001) DATE: 2/16/83 NEW REPEAT  SHEET / OF /  
 LOCATION: "HALF FIFTEEN" DIST. 11 CO. SD RTE. 15 AM. 48.0 REMARKS:  
S/B I-15 - 1.5 MI. NO. OF RTE 76 O.C. EXCELLENT SOFT SITE  
 OPERATOR: HENDRIK RECORDER: HENDRIK AUTOS - TRUCKS  
 GOOD SEPARATION

**NOISE MEASUREMENTS SUMMARY**

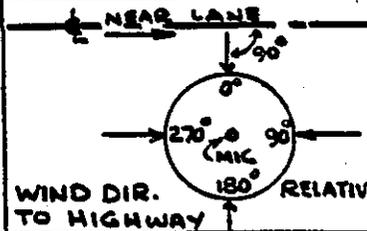
RUN NO.	TIME		Δt	Leq(Δt), dBA, SLM//DL					SINGLE EVENTS NO'S
	START	END		MIC. 1	MIC. 2	MIC. 3	MIC. 4	MIC. 5	
									1-276
NO LEO'S									

**ENVIRONMENTAL DATA SUMMARY**

RUN NO.	EVENT NO.	WIND DATA			DEGREES (see below)	SKY			TEMP.			HUMIDITY		
		SPEED (MPH)				CLR	PTLY CLDY	OVER CAST	COLD <50°	MILD 50-90°	HOT >90°	LO	MED	HI
	1	✓			90°	✓								
	23	✓			90°	✓								
	89	✓			320°	✓								
	108	✓			270°	✓								
	143	✓			90°	✓								
	149		✓		270°	✓								
	150			✓	270°	✓								
	GUMEN.													
	151		✓		90°	✓								
	176			✓	90°	✓								
	183			✓	90°	✓								
	195	✓			90°	✓								
	207			✓	140°	✓								
	212			✓	100°	✓								
	236			✓	90°	✓								
	276			✓	90°	✓								

**COMMENTS:**

VERY QUIET BACKGROUND.  
 FRONTAGE ROAD ON WEST  
 SIDE APPROX. 200' FROM I-15  
 W/VERY LITTLE TRAFFIC. DID  
 NOT ACCEPT EVENTS WHEN  
 VEHICLE(S) ON FR. RD.



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 9-82

Figure VIII-14 Noise Measurement  
 And Environmental Data Sheet Example

CALCULATION SPACE:  
(OR ADDITIONAL COMMENTS)

ROD	X	ELEV.
34	0°	→ 0.0
35	62° EP	→ -0.3
41	17° ES	→ -0.3
42	X 25° OS MIC1	→ -0.2
42	X 50° OS MIC23	→ -1.2
50	X 75° OS	→ -1.6
44	X 100° OS MIC45	→ -1.0

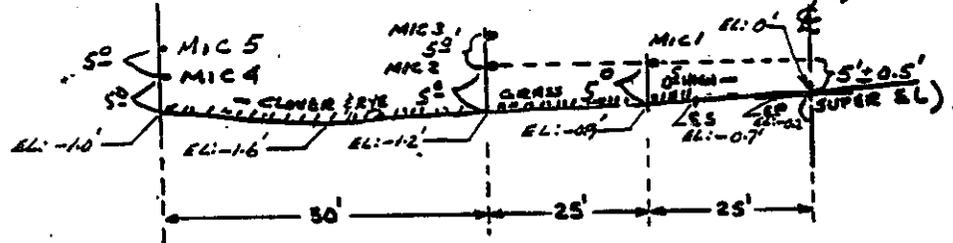
SITE NO: 16 (11015001)  
 ("HALF FIFTEEN")  
 EAST →  
 (Mark Direction)

SITE CHARACTERISTICS:  
 HARD:   
 SOFT:   
 OTHER:   
 (Describe Below)

RTE: 15

PAVEMENT: PCC

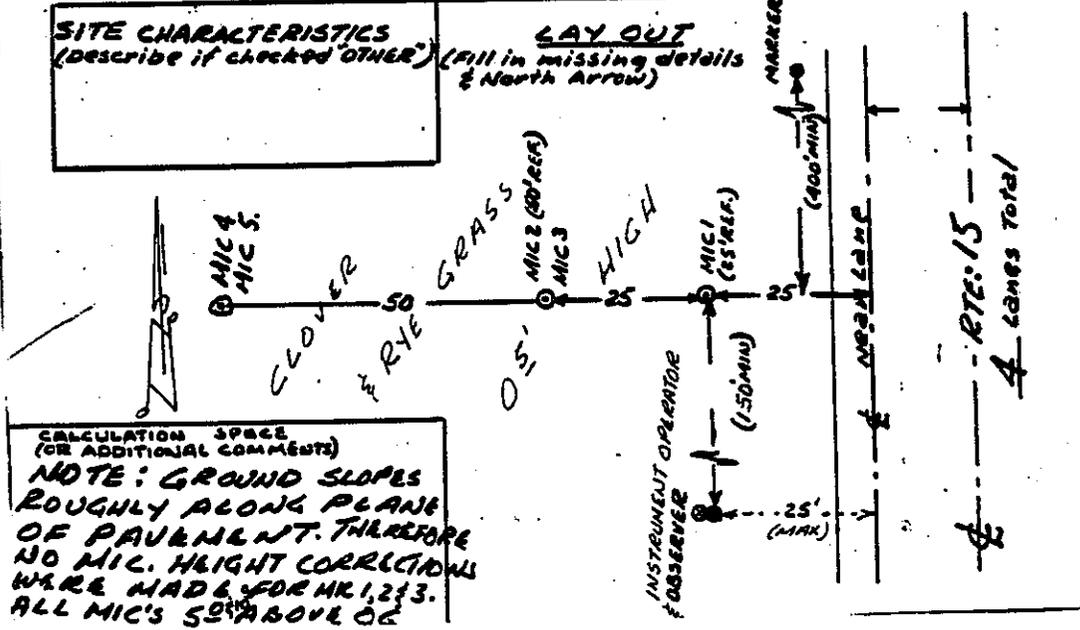
PAVEMENT CONDITION: GOOD FAIR  
 NEW PAVEMENT, DEEP GROOVES, MAY BE NOISY.  
 LANE NO. 2 (NEAR LANE)



X-SEC. (draw in groundline & dimension mic heights above ground)  
 (Mark heights of MIC 4 & 5 w/ respect to pavement & ground)  
 APPROX. SCALE: 1" = 20' HOR & VERT.

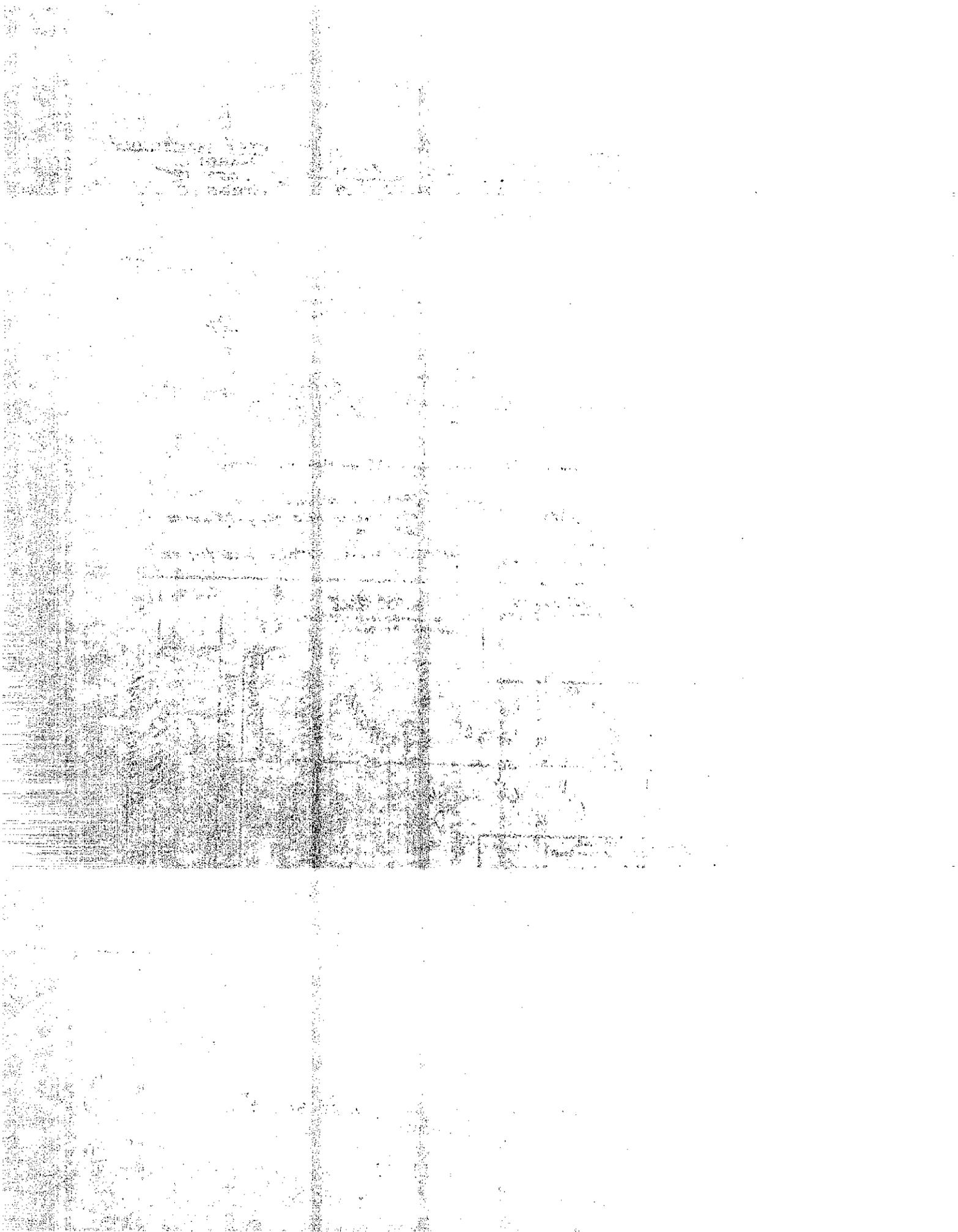
SITE CHARACTERISTICS  
 (Describe if checked "OTHER")

LAY OUT  
 (Fill in missing details & North Arrow)



CALCULATION SPACE  
 (OR ADDITIONAL COMMENTS)  
 NOTE: GROUND SLOPES ROUGHLY ALONG PLANE OF PAVEMENT. THEREFORE NO MIC. HEIGHT CORRECTIONS WERE MADE FOR MIC 1, 2 & 3. ALL MIC'S 50' ABOVE CG

Figure VIII-15 Site Data Sheet (Example)



## IX. DATA PROCESSING OF MEASUREMENT RESULTS

### Input and Merging of Data

During field measurements, data were recorded on four different charts or forms: GLR chart, vehicle observation sheet, datalogger printout and environmental data sheet. An interactive computer program named "VENO" was designed to allow separate input of the various data sources at different times and merge them into one masterfile by site and event number. In addition to merging the data, "VENO" incorporated many options such as listing selected data from the master file and performing statistical analyses. There were four input options: GLR data, vehicle (VEH) data, datalogger (D/L) data, and environmental (ENV) data. The required inputs for each of the options were:

#### GLR Data Input

- ° site number
- ° event number
- ° event quality code:
  - 0 = rejected due to contamination  
or any other reason(s)
  - 1 = valid peak, 6-9 dBA above background
  - 2 = valid peak, 10 dBA or more above  
background

### VEH Data Input

° site number

° event number

° event quality code:

0 = rejected due to contamination  
or any other reason(s).

1 = event accepted

° vehicle type (0-7)

° vehicle speed (mph)

### D/L Data Input

° site number

° mic numbers used

° event number

° event quality code:

0 = rejected due to operator error,  
malfunction or any other reason(s)

1 = event accepted

° maximum noise level measured by each mic

### ENV Data Input

° site number

° date measured

° event number

° event quality

0 = rejected due to adverse environmental  
condition(s) or any other reason(s)

1 = event accepted

° wind speed

° wind angle

After inputting data from all four sources, the "VENO" master file was arranged in the format shown in Figure IX-1, which illustrates an example of data summary output from "VENO". Note that the program calculated the cross-wind vector from the windspeed class and wind angle (wind direction) as was discussed in the Environmental Criteria section of the Field Measurements Chapter (Chapter VIII).

#### Data Summaries

Appendix C contains all data, summaries of the measured data for all sites and all events, including those rejected. Events that were rejected in any of the four quality categories, i.e., code 0 in GLR, VEH, D/L, or ENV were ignored in all data analyses.

# FIGURE IX-1 - DATA SUMMARY EXAMPLE

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	VE	DATE					
SITE	EVENT	TYPE	(1)	(2)	(3)	(4)	(5)	IN	IC							
	ENT	PE	5	5	10	5	10	NG	NT							
	R	E	DBA					DE	DL	DO						
	H	N						E	R							
	L	L														
	V	V														
7	1	2	1	1	1	5	61	89.4	81.8	83.8	72.0	75.8	3	50	2.9	1/10/83
7	2	2	1	1	1	5	57	87.3	79.9	81.8	69.0	72.9	3	50	2.9	1/10/83
7	3	1	1	1	1	5	57	86.9	80.2	82.2	71.3	74.2	3	50	2.9	1/10/83
7	4	0	1	1	1	2	58	87.0	78.8	81.6	71.9	75.3	3	50	2.9	1/10/83
7	5	2	1	1	1	5	63	86.7	79.4	82.5	70.0	73.7	3	50	2.9	1/10/83
7	6	2	1	1	1	5	61	90.3	82.4	84.5	73.3	76.2	3	50	2.9	1/10/83
7	7	2	1	1	1	5	61	90.6	83.5	85.7	72.9	76.7	3	50	2.9	1/10/83
7	8	1	1	1	1	3	52	86.7	79.8	81.2	69.5	73.3	3	90	0.0	1/10/83
7	9	2	1	1	1	5	58	91.4	84.9	86.3	78.4	78.7	3	90	0.0	1/10/83
7	10	2	1	1	1	5	54	88.7	81.4	84.0	73.3	75.2	3	90	0.0	1/10/83
7	11	2	1	1	1	5	65	90.2	83.0	84.2	73.0	76.3	3	90	0.0	1/10/83
7	12	1	1	1	1	2	55	86.9	79.0	81.2	68.1	73.2	3	90	0.0	1/10/83
7	13	2	1	1	1	5	45	87.1	79.9	81.5	71.6	73.8	3	90	0.0	1/10/83
7	14	2	1	1	1	5	54	92.5	84.5	86.4	74.2	77.7	0	50	0.0	1/10/83
7	15	1	1	1	1	2	54	84.2	77.3	78.9	67.2	71.0	0	50	0.0	1/10/83
7	16	2	1	1	1	2	53	86.2	78.4	80.9	67.8	71.9	3	100	-0.8	1/10/83
7	17	2	1	1	1	5	55	92.9	84.5	86.6	73.2	77.0	3	100	-0.8	1/10/83
7	18	2	1	1	1	5	60	88.8	82.3	84.1	75.1	78.1	3	100	-0.8	1/10/83
7	19	2	1	1	1	2	52	88.0	79.3	82.3	69.0	73.0	3	100	-0.8	1/10/83
7	20	1	1	1	1	5	57	88.2	81.3	83.2	71.9	75.5	3	100	-0.8	1/10/83
7	21	2	1	1	1	5	56	90.7	82.1	85.1	72.9	76.3	3	100	-0.8	1/10/83
7	22	2	1	1	1	2	57	90.3	82.2	84.5	70.9	75.0	0	0	0.0	1/10/83
7	23	2	1	1	1	5	60	89.2	83.5	84.1	74.1	77.0	0	0	0.0	1/10/83
7	24	2	1	1	1	1	53	88.5	81.8	83.3	72.1	75.3	0	0	0.0	1/10/83
7	25	0	1	1	1	1	58	82.0	74.5	77.0	63.8	69.7	0	0	0.0	1/10/83
7	26	2	1	1	1	0	59	78.3	72.3	74.1	61.8	66.1	0	0	0.0	1/10/83
7	27	1	1	1	1	5	56	89.9	82.6	84.5	73.3	77.0	0	0	0.0	1/10/83
7	28	2	1	1	1	0	59	78.8	72.8	73.8	62.5	66.9	0	0	0.0	1/10/83
7	29	1	1	1	1	2	57	85.0	78.0	80.0	67.8	72.4	0	0	0.0	1/10/83
7	30	1	1	1	1	3	60	90.6	83.1	84.1	75.6	77.5	0	0	0.0	1/10/83
7	31	0	1	1	1	2	47	83.5	76.7	78.5	68.3	71.6	0	110	0.0	1/10/83
7	32	2	1	1	1	5	53	89.5	82.6	84.2	72.7	76.3	0	110	0.0	1/10/83
7	33	1	1	1	1	2	61	84.0	76.8	78.7	65.6	70.3	3	110	-1.5	1/10/83
7	34	1	1	1	1	1	56	80.4	72.9	75.5	63.5	68.3	3	110	-1.5	1/10/83
7	35	2	1	1	1	2	61	86.4	78.2	80.6	67.4	72.1	3	110	-1.5	1/10/83
7	36	2	1	1	1	5	59	91.2	84.4	85.2	77.1	78.4	3	110	-1.5	1/10/83
7	37	2	1	1	1	5	57	85.8	79.3	81.0	68.7	72.7	3	110	-1.5	1/10/83
7	38	1	1	1	1	2	53	82.5	74.5	77.1	65.0	69.1	3	110	-1.5	1/10/83
7	39	1	1	1	1	3	53	87.8	80.5	82.6	71.8	74.8	3	110	-1.5	1/10/83
7	40	2	1	1	1	3	56	89.6	80.8	83.4	70.8	74.0	3	110	-1.5	1/10/83
7	41	2	1	1	1	5	55	87.8	80.3	82.0	71.3	74.3	3	110	-1.5	1/10/83
7	42	2	1	1	1	1	64	82.5	75.4	76.7	63.1	67.9	0	0	0.0	1/10/83
7	43	2	1	1	1	5	54	88.5	81.1	83.1	72.1	75.0	0	0	0.0	1/10/83
7	44	2	1	1	1	5	53	86.1	79.2	81.1	68.9	72.5	0	0	0.0	1/10/83
7	45	2	1	1	1	1	63	80.1	74.4	75.7	66.2	69.4	0	0	0.0	1/10/83
7	46	2	1	1	1	2	56	87.8	79.4	81.9	69.5	73.0	0	0	0.0	1/10/83
7	47	2	1	1	1	5	64	89.4	83.0	84.9	74.3	76.7	0	0	0.0	1/10/83
7	48	2	1	1	1	1	53	81.9	74.8	76.9	64.9	68.9	3	90	0.0	1/10/83
7	49	2	1	1	1	2	63	85.9	79.3	80.1	69.8	73.6	3	90	0.0	1/10/83
7	50	2	1	1	1	5	56	86.3	79.3	81.1	68.8	72.7	3	90	0.0	1/10/83
7	51	2	1	1	1	3	55	86.4	79.0	80.6	69.7	72.3	3	90	0.0	1/10/83
7	52	2	1	1	1	5	57	94.3	87.1	88.1	79.4	80.9	3	90	0.0	1/10/83
7	53	2	1	1	1	5	53	86.4	78.5	81.0	67.7	71.3	3	90	0.0	1/10/83
7	54	0	1	1	1	5	46	96.2	89.9	90.9	82.4	83.8	3	90	0.0	1/10/83
7	55	2	1	1	1	5	49	94.9	88.5	89.5	82.8	82.2	3	90	0.0	1/10/83
7	56	2	1	1	1	1	62	79.8	72.6	74.4	62.3	66.2	3	90	0.0	1/10/83
7	57	1	1	1	1	0	50	78.8	74.0	75.2	63.4	68.6	3	90	0.0	1/10/83
7	58	2	1	1	1	5	54	88.5	81.1	83.4	71.8	74.5	3	90	0.0	1/10/83
7	59	1	1	1	1	1	60	80.2	74.4	75.5	69.6	71.1	3	90	0.0	1/10/83
7	60	2	1	1	1	1	61	82.4	75.5	77.8	64.6	69.0	3	90	0.0	1/10/83
7	61	2	1	1	1	2	59	85.3	78.0	79.6	67.3	71.5	3	90	0.0	1/10/83
7	62	2	1	1	1	0	63	80.6	74.5	76.8	62.7	67.6	3	90	0.0	1/10/83
7	63	2	1	1	1	5	56	92.9	85.7	87.6	77.5	78.9	3	90	0.0	1/10/83
7	64	2	1	1	1	5	57	91.8	83.8	85.7	74.5	77.3	3	90	0.0	1/10/83
7	65	2	1	1	1	2	53	84.4	77.6	79.9	67.9	71.7	3	90	0.0	1/10/83
7	66	2	1	1	1	2	66	86.6	79.6	81.4	70.1	73.3	3	90	0.0	1/10/83
7	67	2	1	1	1	3	52	87.2	79.5	81.5	69.5	72.6	3	90	0.0	1/10/83
7	68	2	1	1	1	5	54	90.1	82.9	84.7	75.2	77.1	3	90	0.0	1/10/83
7	69	2	1	1	1	5	56	89.5	82.4	84.3	72.9	76.2	3	90	0.0	1/10/83
7	70	2	1	1	1	5	58	94.5	86.4	89.5	73.5	79.5	3	90	0.0	1/10/83

## X. DATA ANALYSES AND RESULTS

### Analyses

The following general analyses were performed on the data:

°Developing speed dependent emission levels for compact autos, standard autos, medium trucks, three-, four-, and five-axled heavy trucks and combining emission levels that were not significantly different.

°Examining effects of hard and soft sites on emission levels at the 50-foot reference distance, and the point source drop-off rates in the near and far fields by vehicle group.

°Examining geographical differences in emission levels for two regions designated Northern and Southern California.

°Examining effects of wind on emission level measurements.

### Emission Levels By Vehicle Type

Computation of the mean energy emission levels was performed by computer using the previously mentioned "VENO" program. The program computes emission levels by the two methods described in FHWA-OEP/HEV-78-1(8).

The first method of computation is the curve fitting method using the expression  $L_{OE} = A + 0.115(S_y)^2 + B \text{ LOG}$  (MPH) for each vehicle type, where:

$L_{OE}$  is the energy mean emission level

A and B are the y-intercept and slope, respectively in the linear regression equation.

$S_y$  is the standard error of y on LOG X.

The curve fitting form was derived from the general relationship:

$$L_{OE} = L_O + .115(\sigma)^2 \text{ where:}$$

$L_{OE}$  is the energy mean sound level of a source

$L_O$  is the measured mean sound level of a source

$\sigma$  is the standard deviation computed from the sound level measurements.

The above general relationship assumes a normal distribution of the sound levels.

The second method used by "VENO" is the computation of the energy mean sound level of each vehicle type in each speed class.

Instead of using the relationship:

$$L_{OE} = L_O + .115(\sigma)^2,$$

actual energy averaging was performed by the computer. Spot checks confirmed close agreement between the two methods of energy averaging.

The curve fitting method was used to develop the individual vehicle type energy mean noise emission speed curves for the reference distance of 50 feet, shown in Figures X-1 through X-5. Additional plots, including 95% confidence bands (intervals) for the curves are shown in Appendix D. In all plots LOE is identical to  $\overline{LOE}$ .

Figure X-1 shows a comparison of compact vs standard auto, (type 0 vs type 1 vehicles) energy mean emission levels vs speed, and respective regression equations. The data included all sites and quality of events was at least 1 in the four categories: GLR, VEH, D/L and ENV. The curves indicate that compact auto (4-cylinder) emission levels are between 1.2 dBA at 25 mph and 1.5 dBA at 65 mph lower than standard automobiles (6 or 8 cylinders). The reasons for this difference are unclear, but it is suspected that the compact car fleet contains more later model cars with better mufflers than the standard car fleet.

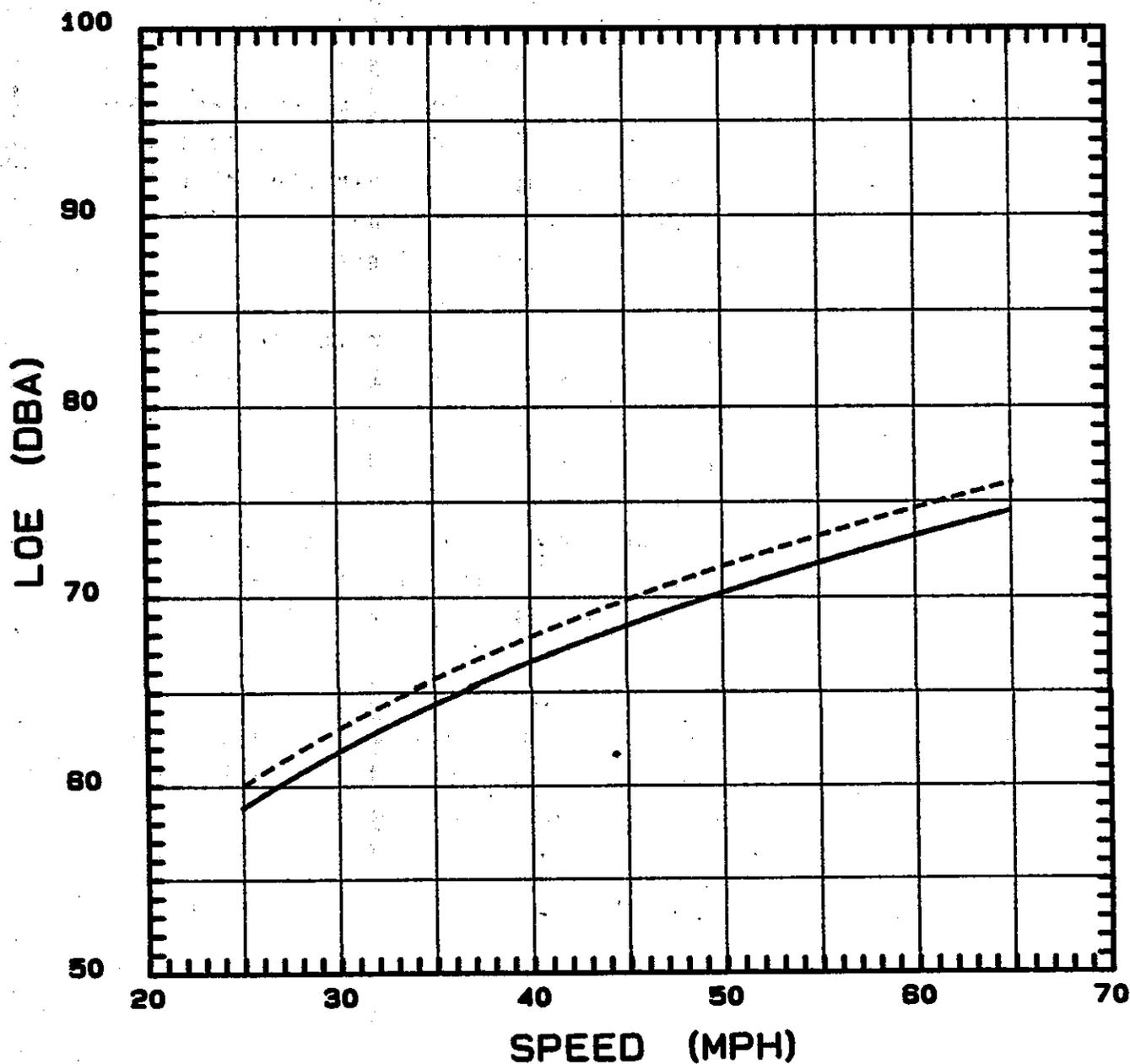
Because of the diversity in the sixteen sites and the reasonable assumption that no bias was present toward selection of either compact or standard auto events, it may be safe to assume that the ratio of sampled compact vs standard autos is representative of the state's ratio. A combined compact and standard auto emission curve is therefore, a good approximation for all autos, especially since the differences between the two are small.

A combined compact and standard auto curve for California is shown in Figure X-2 in comparison with the FHWA curve. Examination of both curves indicates that the California curve is from 0.7 dBA at 25 mph to 1.0 dBA at 65 mph higher than the FHWA curve (projected down to 25 mph and up to 65 mph).

# FIGURE X-1 CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES  
MIC.#2 HT-5FT. DIST-50FT.

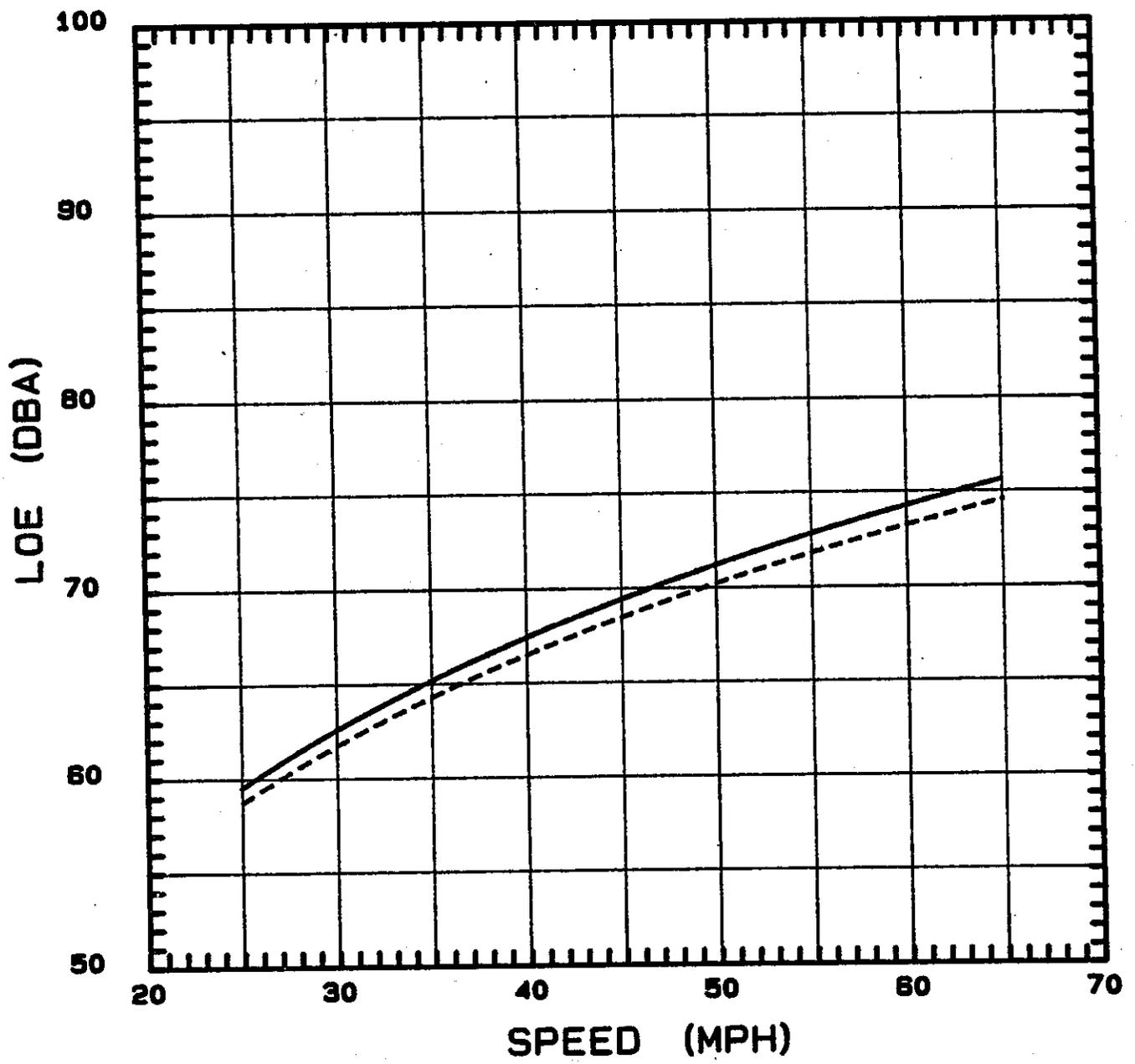
— VEH. TYPE: AUTO-COMP LOE=6+37.79\*LOG (MPH)  
- - - VEH. TYPE: AUTO-STD LOE=6.28+38.47\*LOG (MPH)



# FIGURE X-2 CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES  
MIC.#2 HT-5FT. DIST-50FT.

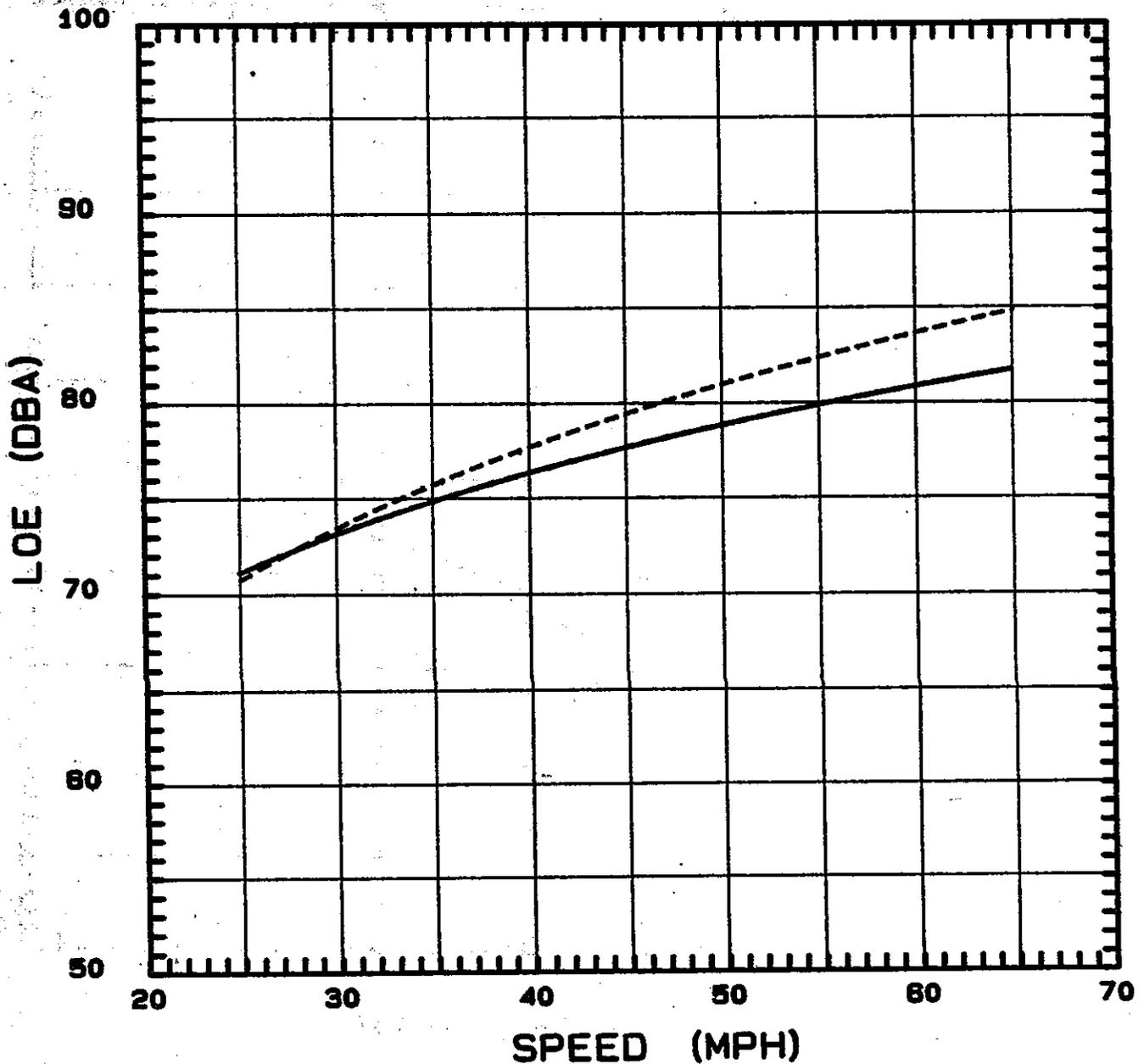
— VEH. TYPE: ALL AUTOS LOE=5.21+38.83\*LOG (MPH)  
- - - VEH. TYPE: FHWA AUTOS LOE=5.5+38.1\*LOG (MPH)



# FIGURE X-3 CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES  
MIC.#2 HT-5FT. DIST-50FT.

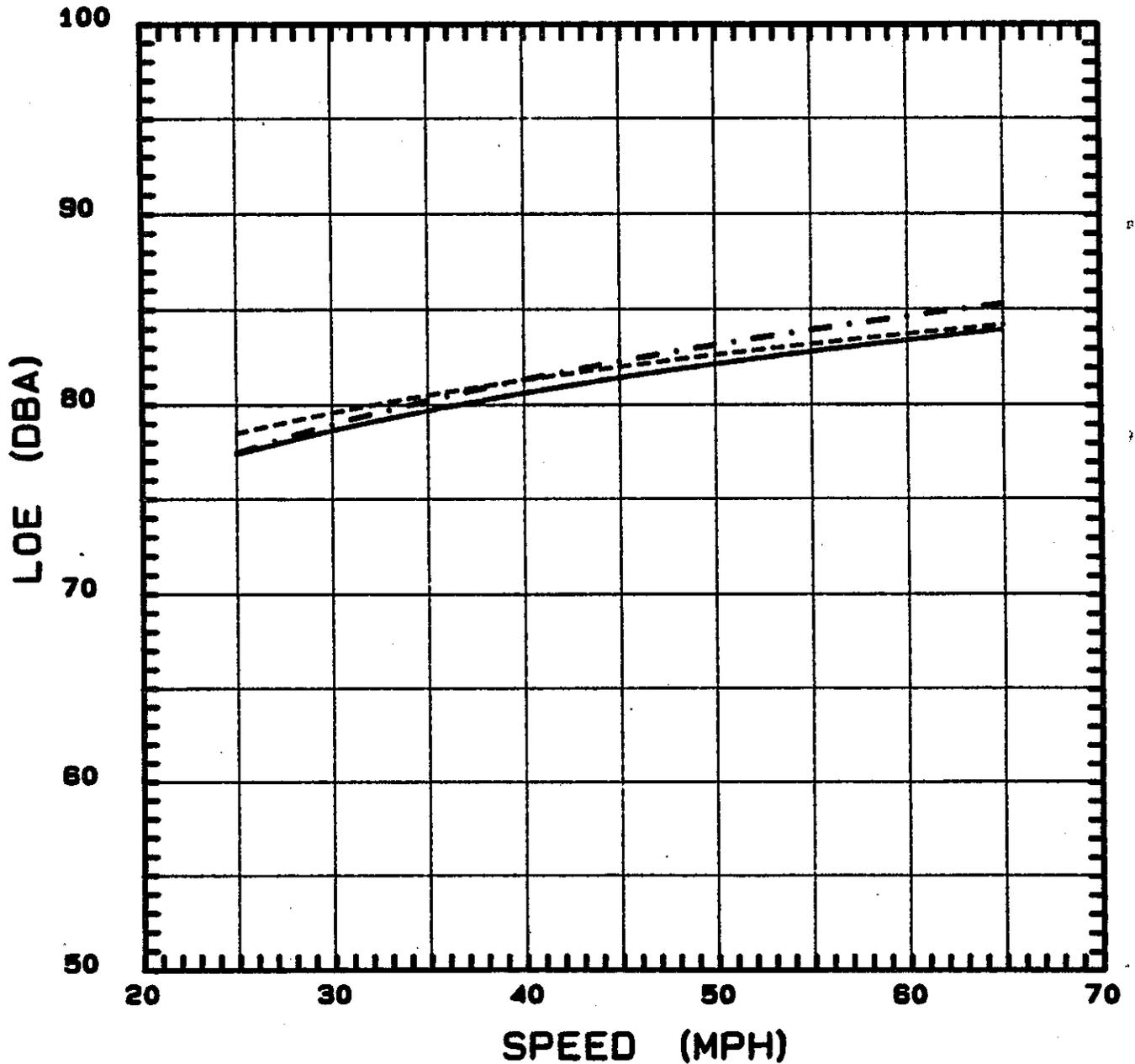
— VEH. TYPE: MEDIUM TRUCKS LOE=35.34+25.59\*LOG (MPH)  
- - - VEH. TYPE: FHWA MT LOE=23.4+33.9\*LOG (MPH)



# FIGURE X-4 CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES  
MIC.#2 HT-5FT. DIST-50FT.

- VEH. TYPE: HT 3-AXLE LOE=55.28+15.8\*LOG (MPH)
- - - VEH. TYPE: HT 4-AXLE LOE=59.37+13.69\*LOG (MPH)
- · - VEH. TYPE: HT 5-AXLE LOE=51.06+18.88\*LOG (MPH)



# FIGURE X-5 CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES  
MIC.#2 HT-5FT. DIST-50FT.

— VEH. TYPE: ALL HT LOE=50.37+19.18\*LOG (MPH)  
- - - VEH. TYPE: FHWA HT LOE=43.6+24.6\*LOG (MPH)

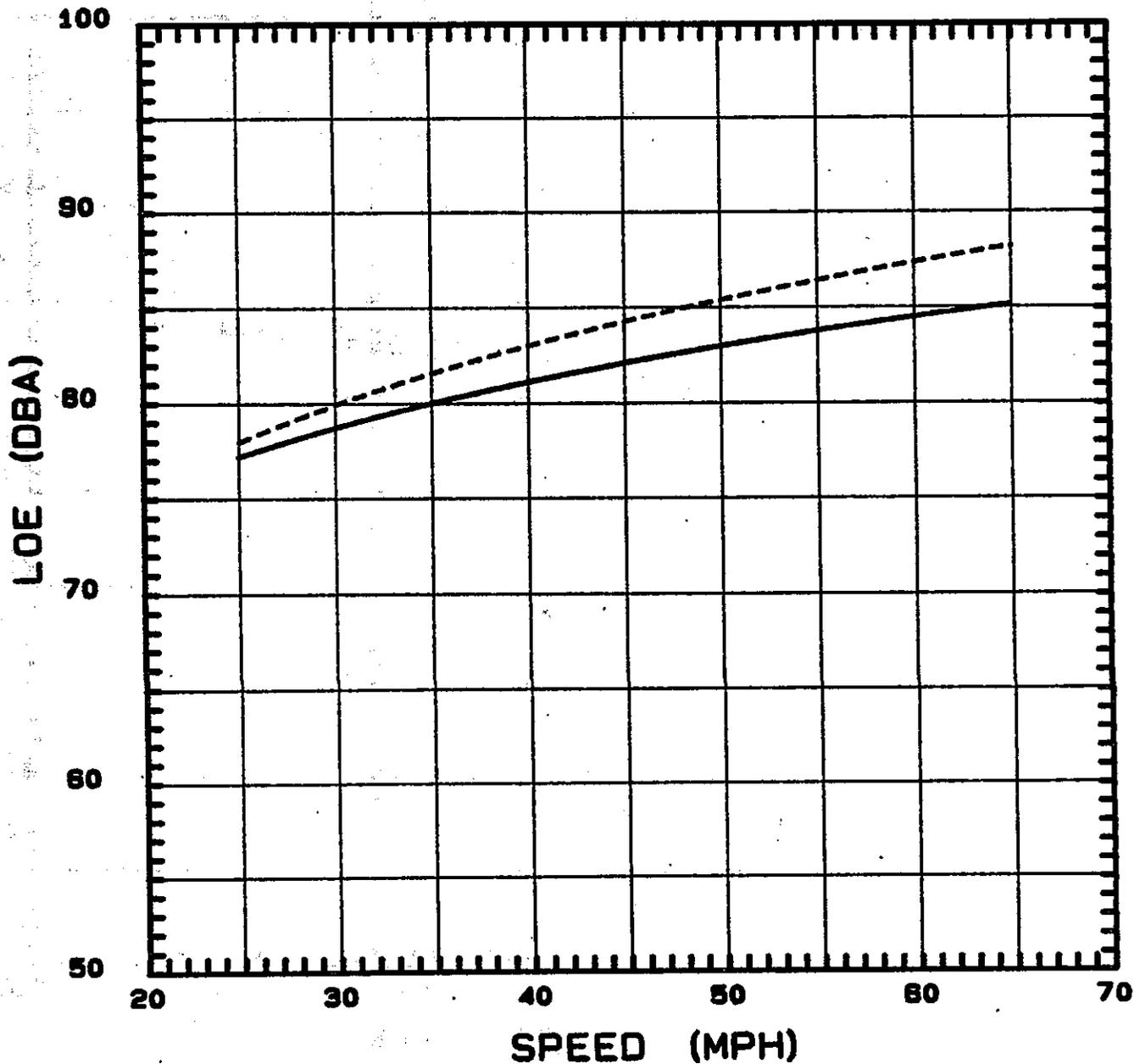


Figure X-3 shows California's medium truck (vehicle type 2) curve in comparison with FHWA's curve for the speed range of 25 to 65 mph. Again, all sites were included and all medium truck events of at least quality 1 were used to develop the curve. The California curve is from 0.3 dBA higher at 25 mph to 3.2 dBA lower at 65 mph.

Figure X-4 illustrates a comparison of 3, 4, and 5-axle trucks (vehicle types 3, 4 and 5) from data gathered at all sixteen sites. Because of the close agreement between the three curves, they were combined into one curve shown in comparison with the FHWA curve (projected up and down) for heavy trucks. There are very few 6- or more axle trucks (type 6 vehicles) in California. Only 1 passby was measured in that category.

Recently, however, as part of an FHWA truck test of three long truck configurations, seven 55 mph passbys of a seven-axle, three-trailer truck were measured at 50 feet, two of which were on 4% and 6% grades and five on level roads. The limited data suggested that there is no difference between this configuration and other heavy trucks.

The combined heavy truck curve for California is from 0.8 dBA at 25 mph to 3.1 dBA at 65 mph lower than the FHWA curve.

Type 7 vehicles (miscellaneous, such as motorcycles, etc.) also made up a very small portion of the observed vehicle population. They were not numerous enough to justify separate emission level curves as additional vehicle groups.

The preceding analyses indicate that the vehicle categories defined in FHWA-RD-77-108(2) provide enough resolution to define vehicle emission levels in California. Neither subdivision of these groups nor additional groups appear necessary. Table X-1 summarizes regression statistics for the three major groups.

The emission levels for the three vehicle groups were also plotted by energy mean noise levels for each speed class at 50 feet. Figure X-6 through X-8 shows the computer generated plots in comparison with the curve fitting method plots shown in Figure X-2, X-3, and X-5.

The computed values are shown in the "VENO" generated printouts in Appendix E, for autos, medium trucks and heavy trucks.

The plots show the inherent differences of the two methods of calculating the emission levels. The curve fitting method produces a smooth line of best fit through all data points, ignoring deviations possibly caused by vehicle operations in low, medium, and high gears.

The energy mean data by speed class, however, do show these deviations within discrete intervals defined by the speed classes.

Figure X-6 shows the plots for autos. Note that three deviations from the regression line exist for the data plotted by speed classes. The first deviation of about 2 to 3 dBA centers at about 23 mph (speed class of <25 mph), and 27 mph (speed class range of 25 to 38 mph), while the second and third deviations of 0.6 and 1.3 dBA center at

TABLE X-1

CALIFORNIA VEHICLE NOISE  
EMISSION LEVELS

SUMMARY OF REGRESSION STATISTIC  
FOR THE THREE VEHICLE GROUPS  
AT REFERENCE DISTANCE OF 50 FEET

AUTOS

Regression Equation (Mean):	4.3+38.8 LOG(MPH)
Regression Equation (Energy Mean):	5.2+38.8 LOG(MPH)
Number of Observations:	1263
Std. Error of Y on Log (X):	2.81
Index of Determination:	0.56
Coeff. of Correlation:	0.75
F-Ratio (Calculated):	1609.1
F-Ratio ( $F_{1,n-2,0.05}$ ):	3.8

MEDIUM TRUCKS

Regression Equation (Mean):	34.4+25.6 LOG(MPH)
Regression Equation (Energy Mean):	35.3+25.6 LOG(MPH)
Number of Observations:	317
Std. Error of Y on LOG(X):	2.83
Index of Determination:	0.42
Coeff. of Correlation:	0.65
F-Ratio (Calculated):	229.2
F-Ratio ( $F_{1,n-2,0.05}$ ):	3.9

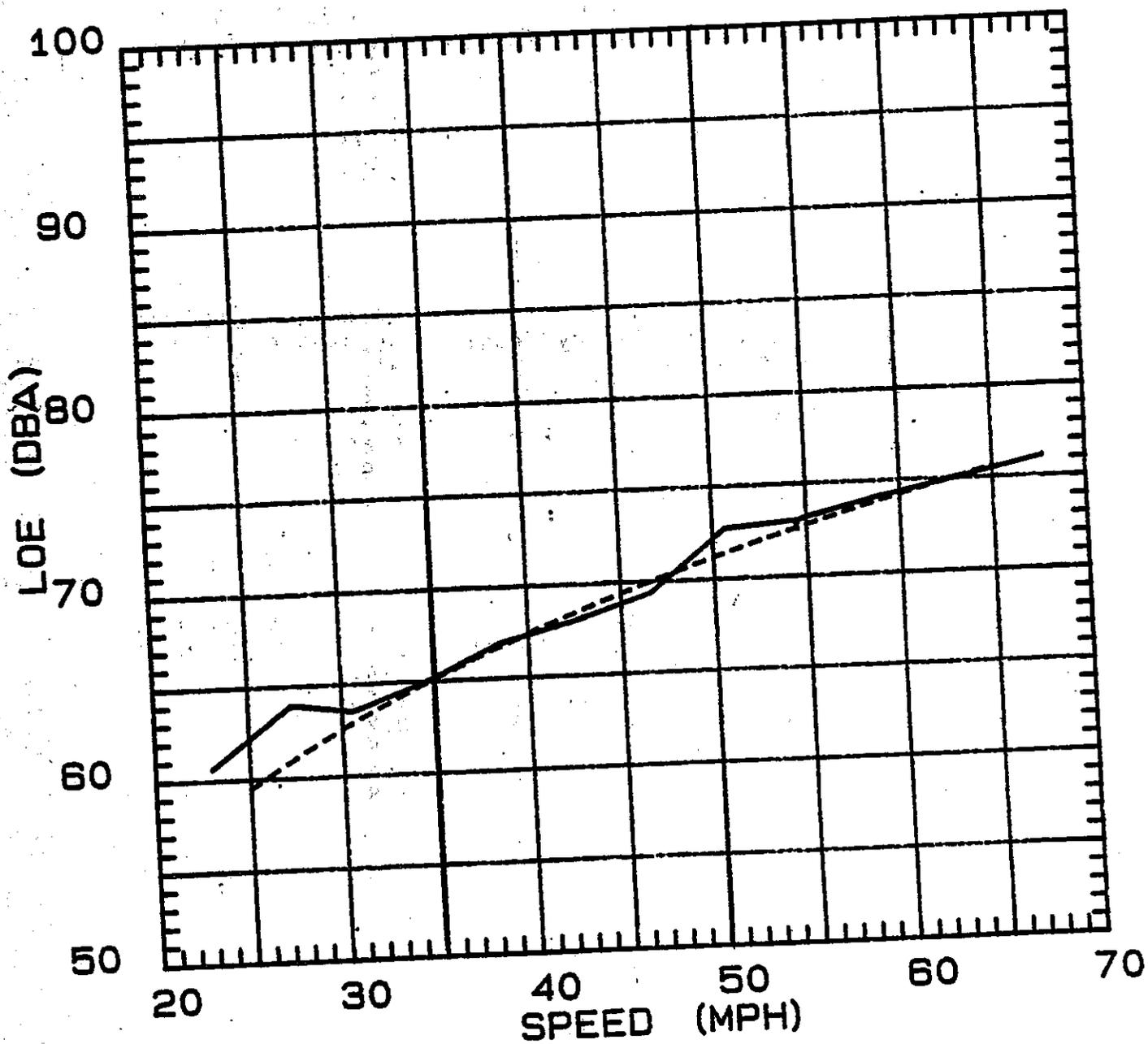
HEAVY TRUCKS

Regression Equation (Mean):	49.5+19.2 LOG(MPH)
Regression Equation (Energy Mean):	50.4+19.2 LOG(MPH)
Number of Observations:	1154
Std. Error of Y on LOG (X):	2.68
Index of Determination:	0.29
Coeff. of Correlation:	0.53
F-Ratio (Calculated):	459.7
F-Ratio ( $F_{1,n-2,0.05}$ ):	3.8

# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

VEHICLE TYPE: ALL AUTOS  
MIC.#2 HT-5FT. DIST-50FT.

----- ALL SITES  $LOE = 5.21 + 38.83 * LOG(MPH)$   
——— ALL SITES SPEED CLASS MEAN DATA



# FIGURE X-7 CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

VEHICLE TYPE: MEDIUM TRUCKS  
MIC.#2 HT-5FT. DIST-50FT.

----- ALL SITES  $LOE = 35.34 + 25.59 * LOG(MPH)$   
———— ALL SITES SPEED CLASS MEAN DATA

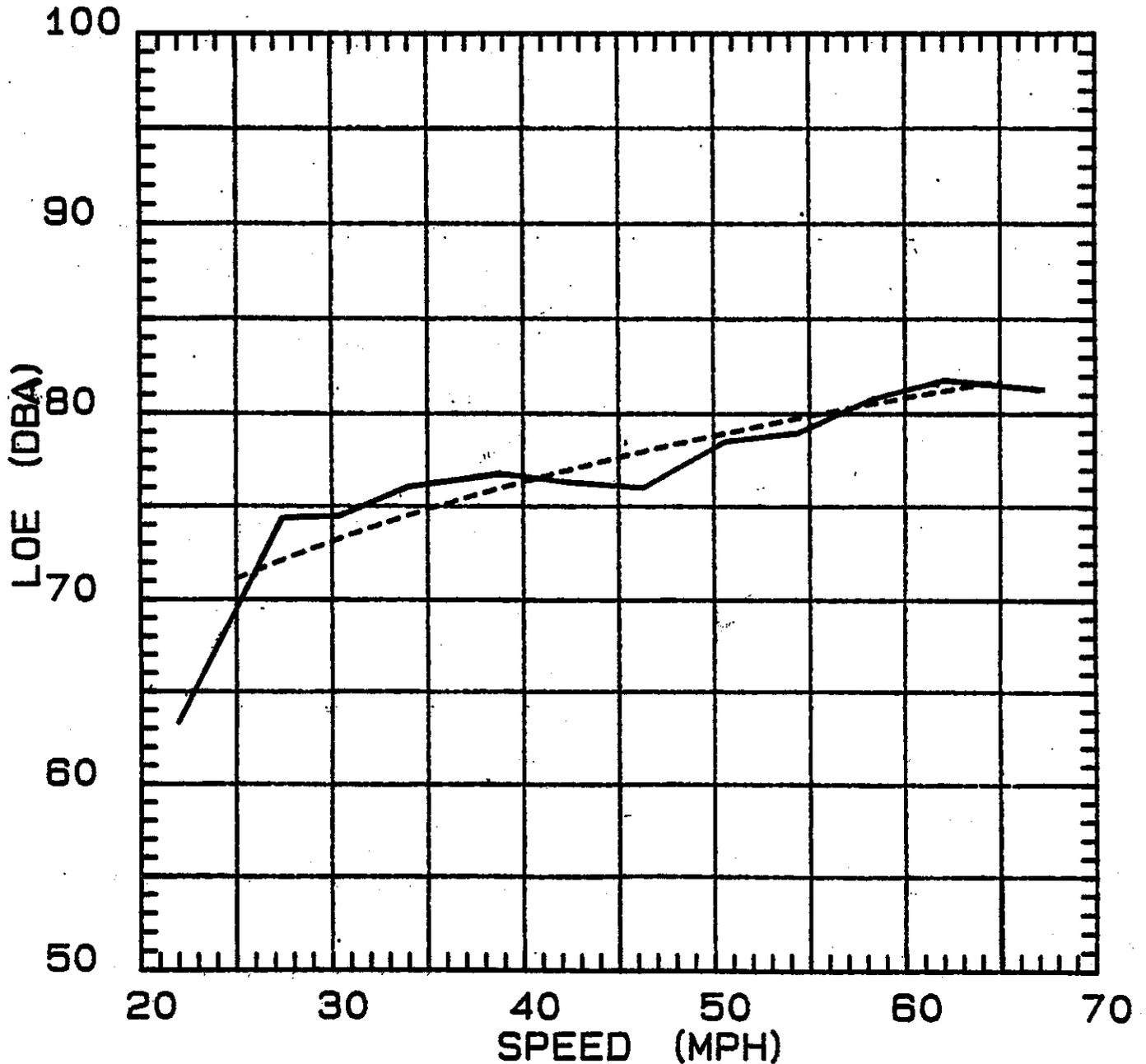
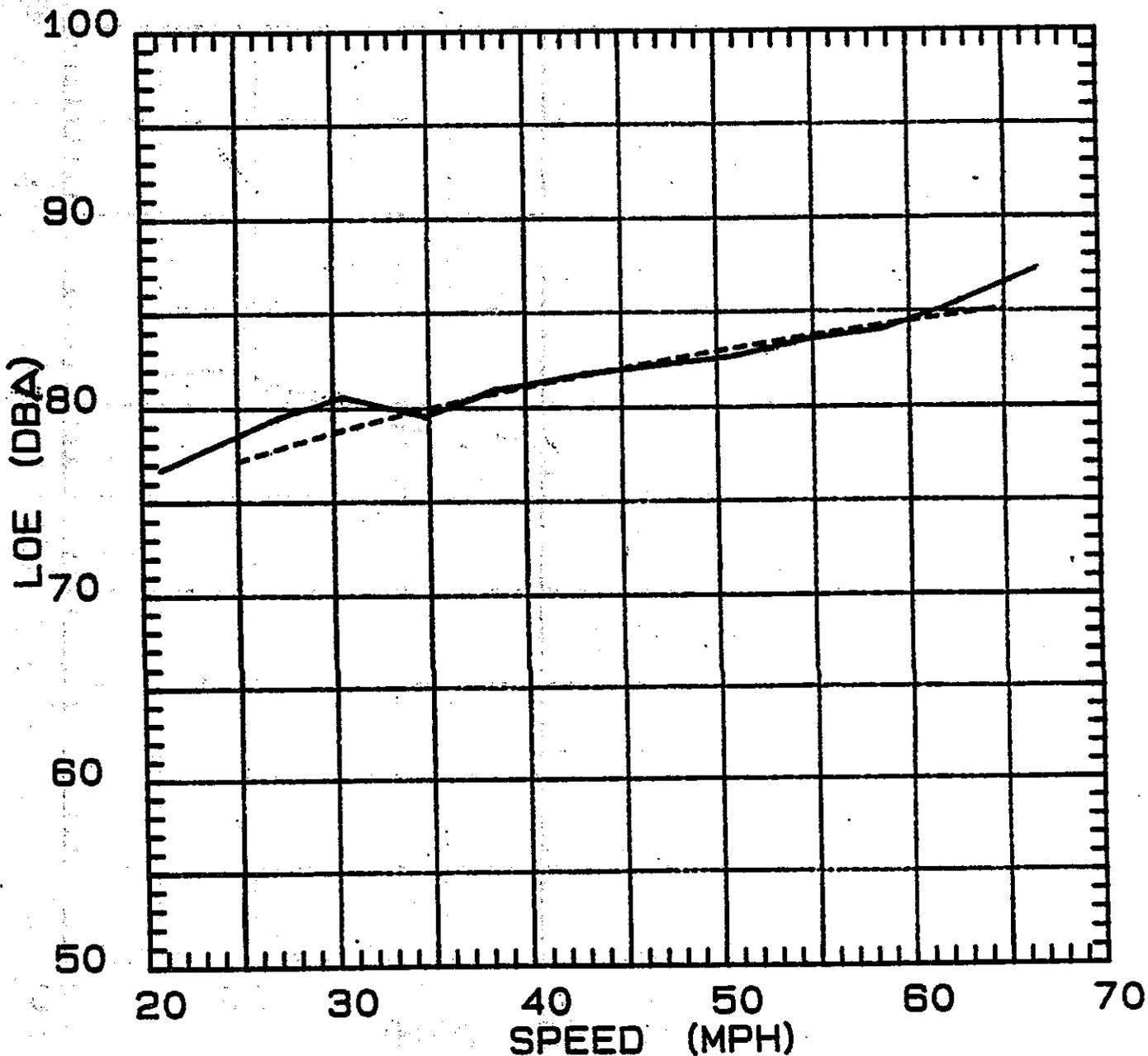


FIGURE X-8  
CALIFORNIA VEHICLE NOISE EMISSIONS  
LOE VS. SPEED

VEHICLE TYPE: HEAVY TRUCKS  
MIC.#2 HT-5FT. DIST-50FT.

----- ALL SITES LOE=50.37+19.18\*LOG (MPH)  
———— ALL SITES SPEED CLASS MEAN DATA



46.5 and 51 mph (45 to 48 mph and 49 to 52 mph speed classes), respectively. The deviations at 23 and 37 mph were caused by only nine data points (see Table VIII-1 in Chapter VIII, Field Measurements) and did not prove significant when subjected to a statistical "t"-test,  $\alpha=0.05$ (12).

The deviations of 0.6 and 1.3 dBA at 46.5 and 51 mph were judged to be too small to be considered significant. The regression line in Figure X-2 therefore adequately represents the California auto population.

The medium truck plots (Figure X-7) showed the same trend at the low end of the curve. The energy means for the speed-classes were above the regression line between 26 mph and 41 mph (only one data point at 22 mph caused the sharp dip at the extreme end), and below the regression line between 41 and 51 mph. From 51 mph to 65 mph deviations from the regression line were very small. Table VIII-1 in Chapter VIII, Field Measurement indicated that there was adequate data within each speed class for medium trucks only at speeds above 48 mph (beginning with 49 to 52 mph speed class), where deviations from the regression line are small. When the energy means by speed class were compared statistically with the energy mean regression line, only the data at 34.1 mph and 46.3 mph proved to be significantly different (significance level 0.05) when subjected to a Student's "t"-test(12). Since medium truck emission level contribution to total noise levels is relatively small, no refinement was made to the energy mean regression line.

The heavy truck plots of energy means by speed class (Figure X-8) showed generally good agreement with the

regression line, except at the lower and upper end of the line. At the upper end the deviation was caused by the energy mean of the >64 mph speed-class centered at 66.8 mph, beyond the practical 65 mph limit. This deviation was therefore ignored. The deviation of the energy mean of the 61 to 64 mph speed class was only 0.4 dBA, an insignificant amount.

At the lower end of the regression line, the energy means for speed classes 25 to 28 mph and 29 to 32 mph were significantly higher than the regression line by 1.4 and 1.7 dBA respectively or an average of 1.55 dBA. The two energy means were submitted to a "t" test(12) to determine whether they were significantly different from the regression line. The null hypothesis was:

$$H_0: \bar{Y} = \mu, \text{ in which:}$$

$\bar{Y}$  is the energy mean emission level for the average speed of the speed class of interest and,  $\mu$  is the energy mean emission level calculated from the regression equation for the same speed.

The "t" statistic was calculated from

$$t = \frac{(\bar{Y} - \mu)\sqrt{n}}{S}, \text{ in which}$$

n = number of samples to derive  $\bar{Y}$ , and

S = standard deviation of those samples.

The  $H_0$  was rejected when  $t(\text{calc}) > t_{(\alpha; n-1)}$ . The level of significance  $\alpha$  was set at 0.05.

For the 25 to 28 mph speed class centered at 27.1 mph the following statistics were derived:

$$\begin{aligned}\mu &= 77.9 \text{ dBA} & H_0: \bar{Y} &= \mu \\ \bar{Y} &= 79.5 \text{ dBA} \\ n &= 18 \\ S &= 3.4 \text{ dBA}\end{aligned}$$

$$\begin{aligned}t(\text{calculated}) &= 2.02 \\ t(0.05;17) &= 1.74 \\ \text{Reject } H_0.\end{aligned}$$

Conclusion: There was a significant difference between  $\bar{Y}$  and  $\mu$  at 27.1 mph.

The statistics for comparison of the energy mean of the 29 to 32 mph speed class (centered at 30.5 mph) and the regression line were:

$$\begin{aligned}\mu &= 78.9 \text{ dBA} & H_0: \bar{Y} &= \mu \\ \bar{Y} &= 80.6 \text{ dBA} \\ n &= 37 \\ S &= 3.5\end{aligned}$$

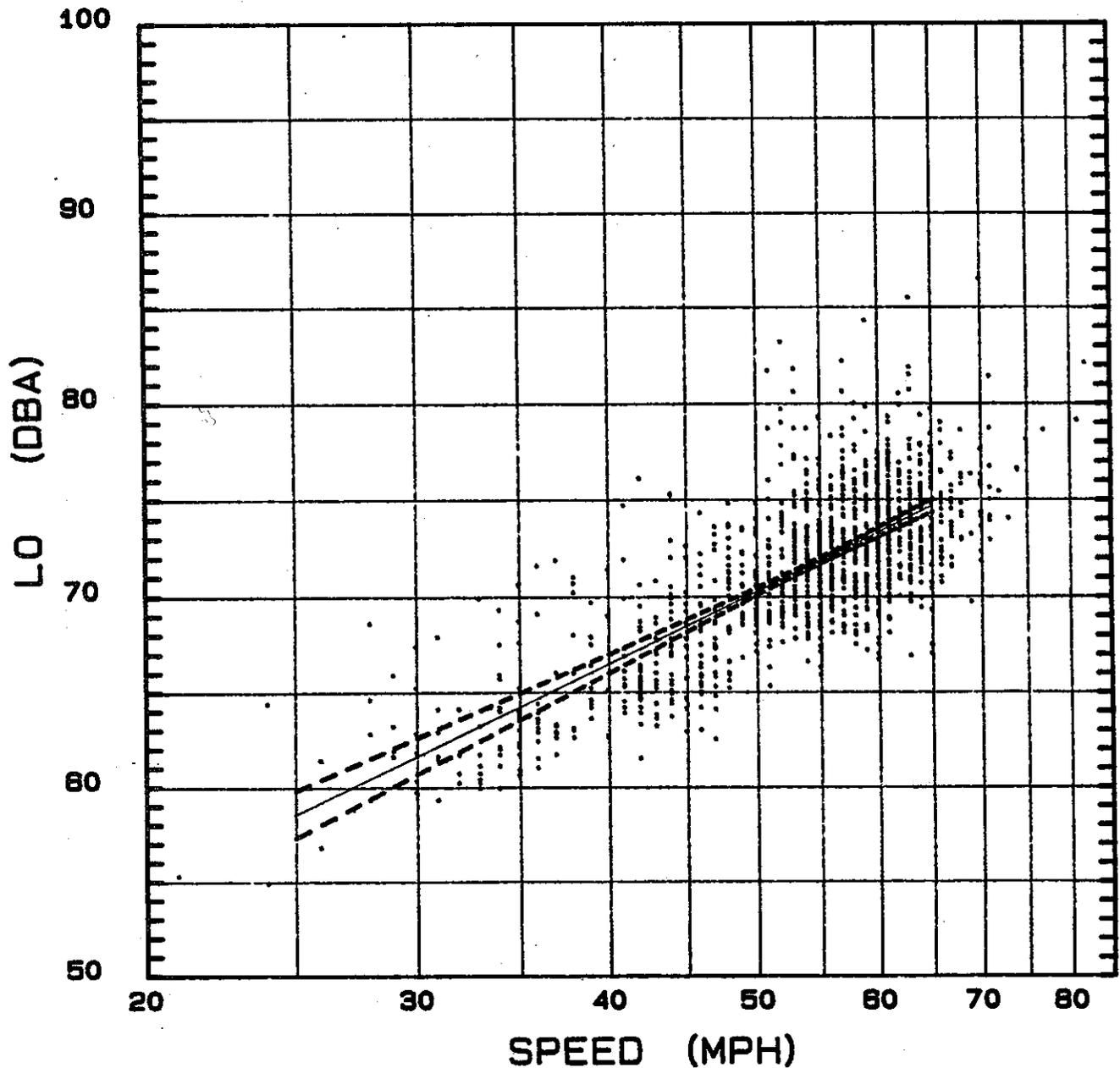
$$\begin{aligned}t(\text{calculated}) &= 2.96 \\ t(0.05;36) &= 1.69 \\ \text{Reject } H_0.\end{aligned}$$

Conclusion: There was a significant difference between  $\bar{Y}$  and  $\mu$  at 30.5 mph.

# CALIFORNIA VEHICLE NOISE EMISSIONS LO VS. SPEED

VEHICLE TYPE: ALL AUTOS  
MIC.#2 HT-5FT. DIST-50FT.

- ALL SITES -- ALL DATA POINTS
- ALL SITES  $LO = 4.31 + 38.83 \times \text{LOG}(\text{MPH})$
- - - - 95% CONFIDENCE INTERVALS FOR PREDICTION EQUATION



The deviations were, therefore, incorporated in the California heavy truck emission levels.

Appendix D presents additional emission level vs. speed plots. Final proposed California Vehicle Noise (CALVENO) Reference Energy Mean Emission Levels are presented in Chapter XI.

#### Hard vs. Soft Sites

Differences at 50 foot reference distance: The FHWA-RD-77-108 (2) report assumes that there are no differences between energy mean emission levels measured at hard sites and soft sites at 50 feet from the source. California data, however, suggest that there are differences between hard and soft sites at 50 feet.

There are several problems in comparing emission levels gathered at one group of sites with those from another group of sites: 1) There is no assurance that the vehicle populations measured at the one group of sites are identical to those of the second group of sites. 2) Environmental conditions (wind speed and direction) are likely to be different. 3) The speed distributions of the various vehicle types may also be different.

In the study, the first problem was reduced, if not eliminated, by assuming there were no differences between hard and soft sites at 25 feet from the source. In most cases this assumption proved to be valid. In both hard and soft sites, the source was assumed to be on the centerline of the near lane, or 6 feet from the edge of pavement. Most sites, hard or soft, had a paved shoulder of eight to ten

feet, and the remainder of the sites either had a partially paved (less than eight feet) or a smoothly graded hard dirt shoulder. The 6-foot distance from source to edge of pavement, plus eight- to ten-foot shoulder at all sites, therefore, guaranteed the first 14 to 16 feet to be hard. In most cases, the remaining 9 to 11 feet to the first microphone could also be considered hard. At any rate, the difference between hard and soft would be almost negligible in 9 to 11 feet.

The noise levels measured at 25 feet were assumed to be unaffected by site variability. Differences in environmental conditions were likewise considered to be negligible at 25 feet. Any differences in energy mean levels measured at 25 feet from the vehicular sources could then be assumed to have been caused by differences in vehicle populations.

The 50 foot mics could then be normalized by setting the 25-foot soft site emission levels equal to the 25-foot hard site levels for autos, medium trucks and heavy trucks. The correction necessary to accomplish this was applied to the 50-foot soft site mics also. Thus, the first two problems - different vehicle populations and environmental conditions - were eliminated. The remaining problem of different speed distributions was eliminated by comparing only those speed classes that had enough data within each speed class common to hard and soft sites.

Table X-2 shows a statistical comparison of normalized energy mean data, measured at 50 feet reference mic (mic 2). Note that the greatest difference of 2.0 dBA was for autos, while medium trucks were 1.9 dBA and heavy trucks

TABLE X-2

STATISTICAL COMPARISON  
HARD VS. SOFT SITES  
BY VEHICLE TYPE (SPEED CLASSES WITH  
ENOUGH DATA ONLY)

$\bar{X}$  = Hard Site Data- $\bar{X}$ =Energy Mean,  $S_x$ =Std.Dev.,  $n_x$ =No. of Samples  
 $\bar{Y}$  = Soft Site Data- $\bar{Y}$ =Energy Mean,  $S_y$ =Std.Dev.,  $n_y$ =No. of Samples

Vehicle Type	Energy Mean, dBA				50' Ref. Mic. Data				Student's "t" Test					
	(MPH) Speed Class	$\bar{X}$ @ 25'	$\bar{Y}$ @ 25'	$\bar{X}-\bar{Y}$ @ 25'	$\bar{X}$ @ 50'	$\bar{Y}$ @ 50'	$\bar{X}-\bar{Y}$ Norm. @ 50'	$S_x$	$n_x$	$S_y$	$n_y$	Calc. "t"	Crit. "t"*	Signif. $\alpha=0.05$
Autos	53-56	79.4	79.5	-0.1	74.2	72.3	2.0 dBA	2.9	84	2.3	174	6.0	1.66	Yes
	57-60	80.0	80.8	-0.8	74.8	73.6	2.0 dBA	3.3	96	2.4	176	5.7	1.66	Yes
	61-64	81.3	81.3	0	76.1	74.1	2.0 dBA	3.5	71	2.0	149	5.4	1.66	Yes
Med.Trks	57-60	87.3	87.2	+0.1	82.1	80.1	1.9 dBA	2.0	23	2.2	55	3.6	1.67	Yes
Hvy.Trks	49-56	88.2	89.3	-1.1	82.9	82.4	1.6 dBA	2.5	46	2.7	60	3.1	1.66	Yes
	53-56	89.2	89.8	-0.6	83.9	83.1	1.4 dBA	2.9	101	2.7	132	3.8	1.66	Yes
	57-60	90.0	90.2	-0.2	84.8	83.3	1.7 dBA	2.4	123	2.1	177	6.5	1.66	Yes
61-64	91.0	91.8	-0.8	85.7	84.9	1.6 dBA	2.3	81	2.4	131	4.8	1.66	Yes	

Student's "t" Test:  $t = \frac{\bar{X}-\bar{Y}}{\sqrt{\frac{(n_x-1)S_x^2+(n_y-1)S_y^2}{n_x+n_y-2} \cdot \left(\frac{n_x+n_y}{n_x \cdot n_y}\right)}}$

Hypothesis:  $H_0 : \mu_x = \mu_y$   
Reject  $H_0$  if  $\text{Calc. "t"} > \text{Crit. "t"}$   
The difference is then significant.

= Calculated "t" (Calc. "t")  
Critical "t" (Crit. "t") =  $t(0.05; n_x+n_y-2)$  from "t" Table\* (one-tailed)

\*Bowker, A. H., Lieberman, G. J., Engineering Statistics. 2nd edition, Prentice-Hall, Inc., New Jersey, 1972

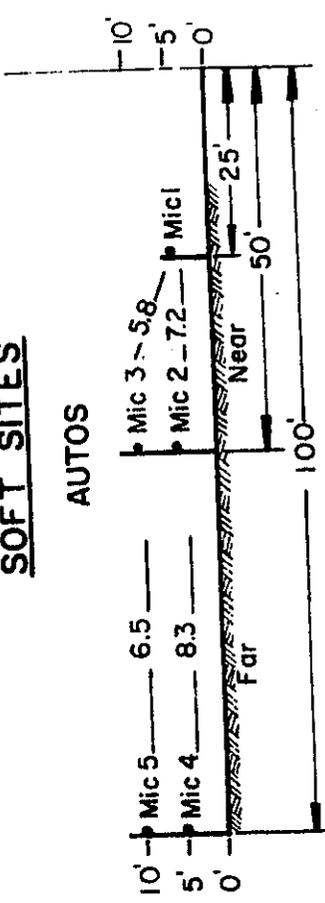
ranged from 1.4 to 1.7 dBA. The normalized differences between hard and soft sites at 50 feet appear to be smaller for higher noise source centroids than those for lower noise centroids. This seems reasonable because ground attenuations increase closer to the ground. According to FHWA-RD-77-108(2), the noise centroid for autos is 0 feet, for medium trucks it is 2.3 feet (0.7 m) and for heavy trucks 8 feet (2.44 m) above the pavement. For all instances shown in Table X-2, the differences between hard and soft sites were statistically significant (level of significance 0.05) when subjected to the Student's "t"-test(12).

Near and Far Field Drop-Off Rates. Figure X-9 and X-10 show single event drop-off rates for near (less than 50 feet from near lane) and far fields (50 feet or greater from near lane) as a function of hard and soft sites and vehicle groups. Figure X-9 shows data averaged from speed classes with minimum required data only, while Figure X-10 includes average data from all speed classes. As indicated in the figures, the drop-off rates from mic 1 to mics 2 and 3 include quality 1 and 2 data from all sites; the drop-off rates from mics 2 and 3 to mics 4 and 5 include quality 2 data from sites with five mic setups only.

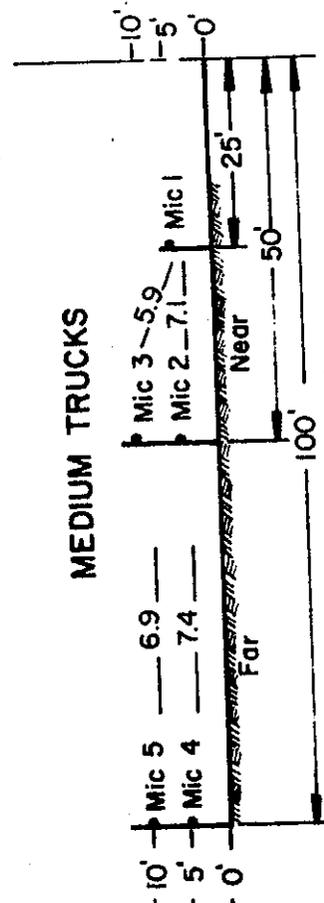
Theoretical drop-off rates for point sources at hard sites are 6.0 dBA per doubling of distance (/DD). The near field (25 to 50 feet) drop-off rates in Figures X-9 and X-10 indicated average drop-off rates of 5.2 dBA at 5- and 10-foot heights. This was probably caused by degradation of point sources at close distances.

**SOFT SITES**

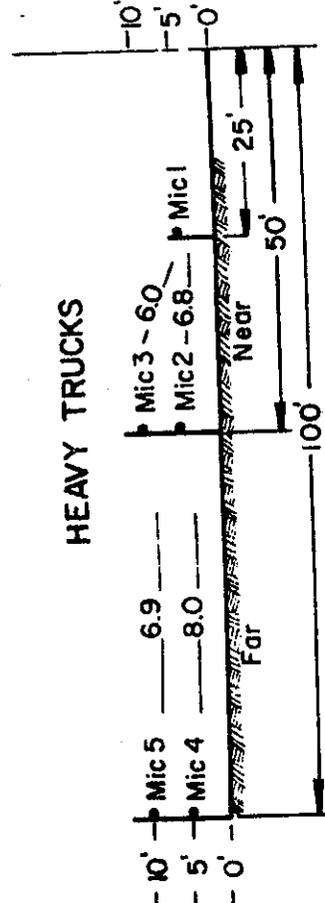
**AUTOS**



**MEDIUM TRUCKS**

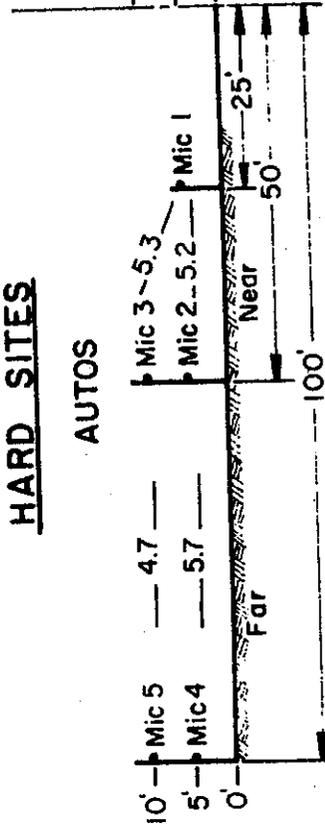


**HEAVY TRUCKS**

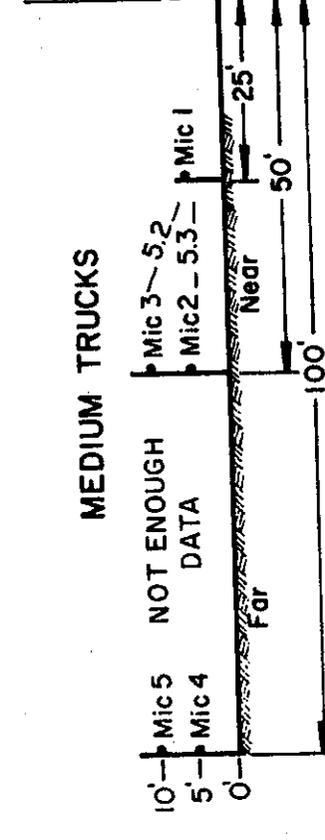


**HARD SITES**

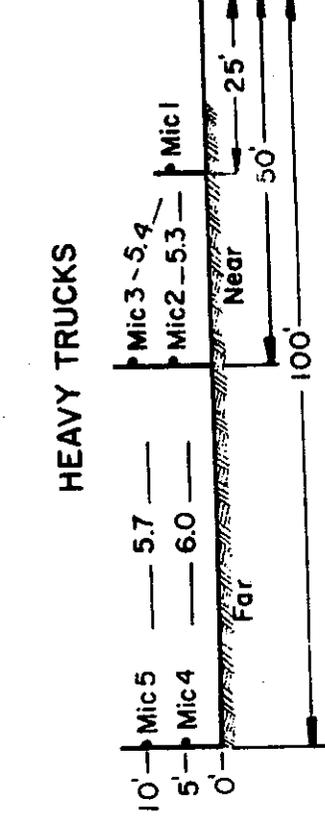
**AUTOS**



**MEDIUM TRUCKS**



**HEAVY TRUCKS**

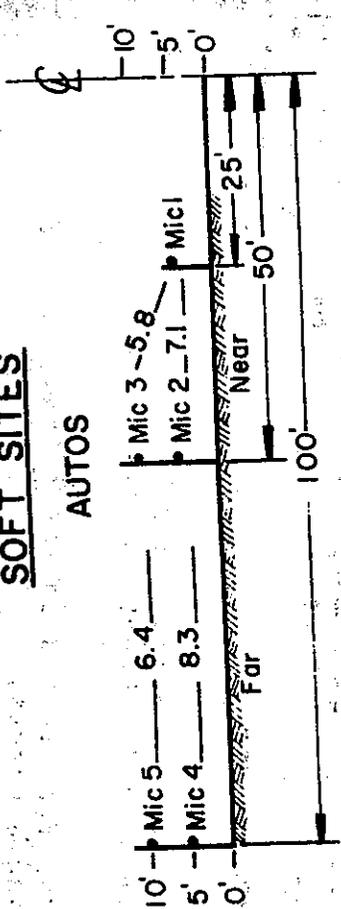


- Speed classes with minimum required data only
- Mic1 - Mic2 & Mic1 - Mic3: All sites; Event quality 1 and 2
- Mic2 - Mic4 & Mic3 - Mic5: Sites with 5 Mic's; Event quality 2 only.

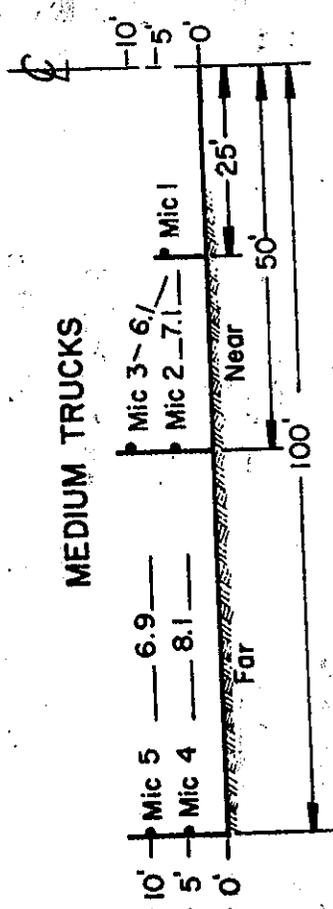
Figure X-9. Near and far field drop off rates, dBA single events.

**SOFT SITES**

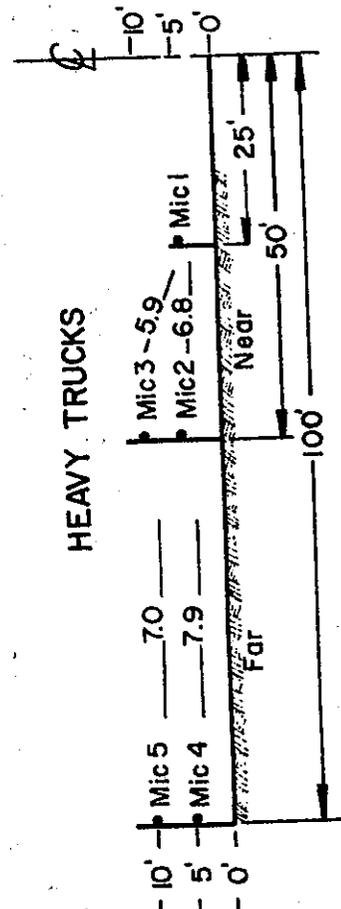
**AUTOS**



**MEDIUM TRUCKS**

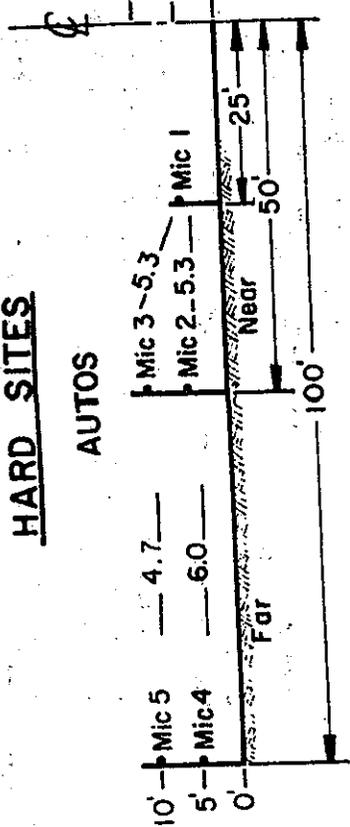


**HEAVY TRUCKS**

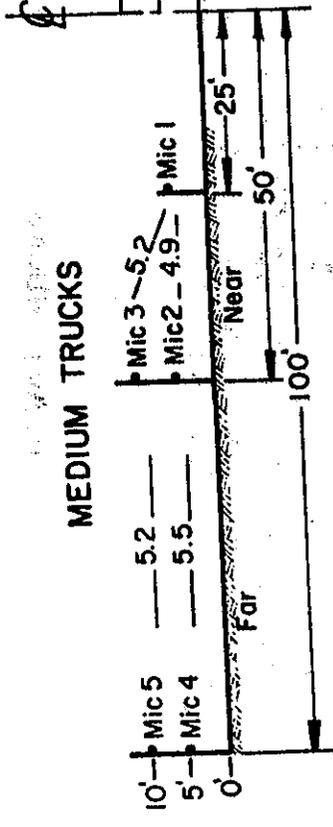


**HARD SITES**

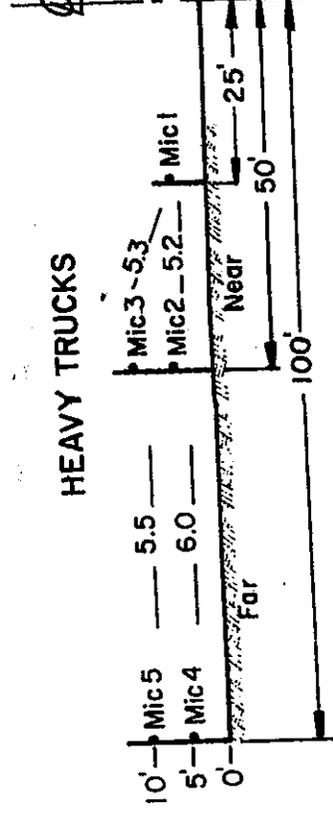
**AUTOS**



**MEDIUM TRUCKS**



**HEAVY TRUCKS**



- All speed classes included
  - Mic1 - Mic2 & Mic1 - Mic3:
  - Mic2 - Mic4 & Mic3 - Mic5:
- All sites; Event quality 1 and 2  
 Sites with 5 Mic's; Event quality 2 only.

Figure X-10. Near and far field drop off rates, dBA single events.

At the soft sites, the apparent degradation of the point source was offset by excess ground attenuation to approximately 7.0 dBA at a height of 5 feet. At a height of 5 to 10 feet, the average between hard and soft sites was 5.9 dBA, or, the excess ground attenuation barely offset the degradation of the point source.

Further analyses of the near field drop-off rates revealed that they were not dependent on speed.

Vehicle type had a slight effect on the near field drop-off rates at the 5-foot height. Auto and medium truck drop-offs differed by about 2 dBA between hard and soft sites. The difference in near field hard and soft sites drop-off rates for heavy trucks appeared to be approximately 1.5 dBA. The latter was probably due to the higher source height of heavy trucks compared to source heights of autos and medium trucks.

A 6 dBA/DD drop-off rate ( $20 \log \frac{D}{D_0}$ ) for point sources corresponds with a 3 dBA/DD rate ( $10 \log \frac{D}{D_0}$ ) for line sources, in that there exists no excess attenuation caused by ground absorption (i.e., the drop-off rates equal the rate of geometric spreading with distance).

At the present, FHWA-RD-77-108(2) recommends the use of  $10 \log \frac{D}{D_0}$  as a line source drop-off rate in the near field, regardless of site characteristic. Based on the data presented in Figures X-9 and X-10 continuation of this drop-off rate seems reasonable even though differences were measured between hard and soft sites.

In reality there are few true hard sites while variations in soft sites are endless. The degree at which excess attenuation offsets the degradation effect of point sources between 25 and 50 feet is therefore difficult to predict. The data presented in Figures X-9 and X-10 suggest that the average near field single event drop-off rates of equally distributed hard and soft sites would be approximately 6.2 dBA/DD for autos, 6.1 dBA/DD for medium trucks, and 6.0 dBA/DD for heavy trucks.

As expected, the far field drop-off rates at hard sites averaged approximately 6 dBA/DD for the five foot high mic's for all vehicle groups (see Figures X-9 and X-10). At the ten-foot high mic's the drop-off rates appeared to vary with the source height, ranging from 4.7 dBA/DD for autos to an average of 5.6 dBA/DD for heavy trucks.

This variation was probably caused by reflections off the pavement by lower sources, projected to the ten-foot high mic's at 100 feet. At the lower mic's, these reflections were apparently either absent because of a different angle of reflection or else scattered by irregularities in the hard surface.

The soft site far field drop-off rates indicated a greater difference between lower and higher mics for low sources (autos) than higher sources (trucks) as expected. Noise emitted by lower sources experiences greater excess attenuation at soft sites than high sources, due to the lower average height of the noise path to a receiver.

As was the case with hard sites, the noise drop-off rates at the ten-foot high mics was lower for autos and higher for trucks. Again, reflections by lower noise sources are suspected.

It also appears from the two figures (X-9 and X-10) that soft site ground attenuation still exists within 10 feet of the ground, a phenomenon noted in an earlier study (7).

At site 5, the far mics (misc 4 and 5) were positioned at 75 feet instead of 100 feet as at all other five mic sites. In order to include mics 4 and 5 data at site 5 with other far mics, a 75- to 100-foot distance adjustment was made to the data measured at site 5 far mics. This adjustment was calculated from noise level differences, dBA, between mics 2 and 4, and mics 3 and 5, in terms of  $X \text{ LOG} \left( \frac{D}{D_0} \right)$ , where X was first solved from dBA between 50- and 75-foot mics. The values of X were then applied to the  $D = 100$ -foot positions to derive the adjustments for mics 4 and 5.

#### Geographical Differences in Vehicle Populations

Table X-3 shows a statistical comparison between vehicle populations in Northern California vs those in Southern California. Northern California was represented by sites 1, 2, 3, 7, 9, 10, 18, and 19, while Southern California was represented by sites 5, 6, 11, 12, 14, 15, 16 and 17.

Only speed classes with enough data in both geographical categories were compared. To eliminate site and meteorological variations, only the energy mean levels measured at 25 feet were included in the statistical analysis.

TABLE X-3

STATISTICAL COMPARISON OF  
VEHICLE POPULATIONS  
NORTHERN CALIFORNIA VS. SOUTHERN CALIFORNIA

°Microphones at 25 Feet  
°Speed Classes With Enough Data Only

Vehicle Type	Speed Class (MPH)	Energy Means, dBA		Diff. X-Y	Std.Dev's		No.Samples		Student's "t"-Test		
		N.Calif. X	S.Calif. Y		Sx	Sy	nx	ny	Calc. "t"	Crit. "t"	Significant $\alpha=0.05^*$
Autos	45-48	76.7	75.4	1.3	2.2	2.9	45	47	2.4	1.99	Yes
	53-56	79.5	79.5	0	2.3	2.7	160	90	-0.2	1.98	No
	57-60	80.5	80.7	-0.2	2.4	3.2	129	134	-0.6	1.98	No
	61-64	81.5	81.2	0.3	2.3	3.1	96	119	0.6	1.98	No
	>64	83.4	82.3	1.1	2.8	3.2	41	62	1.7	1.99	No
Medium Trucks	53-56	85.6	84.7	0.9	2.1	3.1	33	34	1.4	2.00	No
	57-60	87.6	86.9	0.7	2.5	2.2	31	46	1.4	2.00	No
Heavy Trucks	49-52	89.5	87.4	2.1	2.7	2.4	63	41	4.1	1.99	Yes
	53-56	90.1	88.9	1.2	2.5	2.7	111	114	3.3	1.98	Yes
	57-60	90.8	89.7	1.1	2.3	2.1	119	178	4.3	1.98	Yes
	61-64	91.4	91.5	-0.1	2.1	2.6	68	142	-0.4	1.98	No

Student's "t"-Test: Hypothesis:  $H_0: \mu_X = \mu_Y$   
Reject  $H_0$  if Calc. " $t$ " > Crit. " $t$ "  
The difference is then significant.

$$\text{Calc. "t"} = \frac{X-Y}{\sqrt{\frac{(n_x-1)S_x^2 + (n_y-1)S_y^2}{n_x+n_y-2} \cdot \left(\frac{n_x+n_y}{n_x \cdot n_y}\right)}}$$

\*Crit. "t" = (two-tailed,  $\alpha=0.05$ ) =  $t_{(.025; n_x+n_y-2)}$  from "t"-Table\*

\*Bowker, A. H., Lieberman, G. J.; Engineering Statistics, 2nd Edition, Prentice-Hall, Inc., New Jersey, 1972.

Of the five auto speed classes tested, only one (45 to 48 mph) indicated a statistically significant difference of 1.3 dBA between the northern half and the southern half of the state.

No significant difference was detected in the medium trucks. The heavy trucks, however, were statistically different for speeds between 49 mph and 60 mph. The greatest difference was 2.1 dBA at 49 to 52 mph. The north-south differences in remaining speed classes (53 to 60 mph) averaged 1.1 dBA. Although statistically significant, these differences were ignored for practical reasons. By using north-south averages, deviations are limited to a maximum of 0.5 to 1.0 dBA.

### Wind Analyses

The wind data discussed in the Environmental Measurements and Criteria section of Chapter VIII were compared within the previously discussed crosswind vector intervals. The wind analyses presented the following problems:

1. Differences in vehicle populations needed to be eliminated.
2. Site differences had to be accounted for.

The first problem was solved by simply normalizing noise readings at all 25 -foot mics (mic 1) and adjusting the far field microphones accordingly.

The second problem could not be dealt with satisfactorily. Sites ranged from hard to various degrees of soft characteristics. Previous studies (13,14) have shown that the effects of wind on noise measurement results depend on distance and terrain characteristics, e.g., soft sites experience greater wind effects than hard sites. Ideally, studies involving the effects of wind on noise measurements should be performed on the same site for various wind angles and speeds.

Site effects may be minimized by limiting the source to receiver distance. Unfortunately, this strategy also reduces the effects of wind.

The primary objective of the wind study was to examine the effects, if any, at 50 feet. For this distance, the extremes were examined. These were soft site vector winds of 6 to 12 mph (blowing from source to receiver), and -6 to -12 mph (blowing from receiver towards source).

Table X-4 shows these conditions for autos and heavy trucks at mic's 2 and 3. Due to insufficient data for medium trucks, the comparisons were made with 3 to 6 mph vs -12 to -6 mph vector winds. Autos should have shown the greatest difference at mic 2. However, no significant difference could be detected after normalizing the 25 foot mic's, adjusting mics 2 and 3, and subjecting these data to the statistical Student "t"-test(12) with a level of significance of 0.05.

Table X-5 shows the effects for all sites, at mic's 2 and 3. Again, no significant difference was detected at 50 feet.

**TABLE: X-4  
COMPARISON OF WIND EFFECTS  
+6 TO +12 MPH VS -6 TO -12 MPH\*  
SOFT SITES, MIC 2 & 3  
(50 FEET)**

\*T\* TEST: COMPARISON OF WIND VECTOR EFFECTS.

\*\*\*\*\*

\*\*SOFT SITE--MIC. #2\*\*

--ALL AUTOS--

VECTOR RANGE (MPH)	MEAN (DBA)	#VEH.	DIF. (X-Y)	CALC. "T"	CRIT. "T"	SIG. &=.05
6 TO 12	69.27	7	:			
-12 TO -6	69.55	48	:	-.28	-.286	1.676 NO

\*\*\*\*\*

--MEDIUM TRUCKS--

3 TO 6	76.46	29	:			
-12 TO -6	76.95	7	:	-.49	-.326	1.692 NO

\*\*\*\*\*

--HEAVY TRUCKS--

6 TO 12	81.06	7	:			
-12 TO -6	81.35	7	:	-.29	-.151	1.762 NO

\*\*\*\*\*

\*\*\*\*\*

\*\*SOFT SITE--MIC. #3\*\*

--ALL AUTOS--

VECTOR RANGE (MPH)	MEAN (DBA)	#VEH.	DIF. (X-Y)	CALC. "T"	CRIT. "T"	SIG. &=.05
6 TO 12	71.11	7	:			
-12 TO -6	71.39	48	:	-.28	-.278	1.676 NO

\*\*\*\*\*

--MEDIUM TRUCKS--

3 TO 6	77.59	29	:			
-12 TO -6	77.95	7	:	-.36	-.245	1.692 NO

\*\*\*\*\*

--HEAVY TRUCKS--

6 TO 12	81.83	7	:			
-12 TO -6	81.60	7	:	0.23	0.125	1.782 NO

\*\*\*\*\*

--NOTE: SECOND MEAN ADJUSTED BY THE DIFFERENCE AT MIC. #1.

\* Due to insufficient data for medium trucks in this wind category, 3 to 6 vs -12 to -6 mph was used for medium trucks.

**TABLE: X-5**  
**COMPARISON OF WIND EFFECTS**  
**+6 TO +12 MPH VS -6 TO -12MPH**  
**ALL SITES, MIC. 2 & 3**  
**(50 FEET)**

"T" TEST: COMPARISON OF WIND VECTOR EFFECTS.

\*\*\*\*\*

\*\*ALL SITES--MIC. #2\*\*

--ALL AUTOS--

VECTOR RANGE (MPH)	MEAN (DBA)	#VEH.	DIF. (X-Y)	CALC. "T"	CRIT. "T"	SIG. E=.05
6 TO 12	74.08	24	:			
-12 TO -6	73.92	124	:	0.16	0.154	1.658 NO

\*\*\*\*\*

--MEDIUM TRUCKS--

6 TO 12	83.33	3	:			
-12 TO -6	84.67	26	:	-1.34	-.566	1.703 NO

\*\*\*\*\*

--HEAVY TRUCKS--

6 TO 12	83.92	48	:			
-12 TO -6	84.31	52	:	-.39	-.646	1.663 NO

\*\*\*\*\*

\*\*\*\*\*

\*\*ALL SITES--MIC. #3\*\*

--ALL AUTOS--

6 TO 12	74.55	24	:			
-12 TO -6	74.43	122	:	0.12	0.139	1.658 NO

\*\*\*\*\*

--MEDIUM TRUCKS--

6 TO 12	84.00	3	:			
-12 TO -6	84.29	24	:	-.29	-.148	1.708 NO

\*\*\*\*\*

--HEAVY TRUCKS--

6 TO 12	84.35	46	:			
-12 TO -6	84.30	52	:	0.05	0.083	1.663 NO

\*\*\*\*\*

--NOTE: SECOND MEAN ADJUSTED BY THE DIFFERENCE AT MIC. #1.

It was concluded that if noise measurements are made with wind speeds of 12 mph or less, the wind direction does not have an effect on noise levels at 50 feet from the source for all vehicle groups.

In order to examine the wind effects at 100 feet from the source, the wind effects at mics 4 and 5 were examined. Table X-6 shows the results. At mic 4, the normalized auto noise levels were 3.4 dBA higher with 6 to 12 mph positive (source to receiver) wind vectors than with 6 to 12 mph negative (receiver to source) wind vectors. The difference was statistically significant when tested with the Student "t"-test (12), ( $\alpha=0.05$ ). No difference was detected for other vehicle groups or at mic 5. This was probably due to less interference of the ground plane with noise propagation.

The difference at mic 4 may be explained by site variation, wind direction, or both. It is not possible to separate individual contributions by each. No conclusions pertaining to the effects of wind at 100 feet should be drawn from those data.

**TABLE: X-6**  
**COMPARISON OF WIND EFFECTS**  
**+6 TO +12 MPH VS -6 TO -12 MPH**  
**SITES WITH FIVE MIC'S, MIC 4 & 5**  
**(100 FEET)**

"T" TEST: COMPARISON OF WIND VECTOR EFFECTS.

\*\*\*\*\*  
 \*\*5 MIC SITES--MIC. #4\*\*

--ALL AUTOS--

VECTOR RANGE (MPH)	MEAN (DBA)	#VEH.	DIF. (X-Y)	CALC. "T"	CRIT. "T"	SIG. &=.05
6 TO 12	68.42	17				
-12 TO -6	65.00	48	3.42	4.336	1.670	YES

\*\*\*\*\*  
 --MEDIUM TRUCKS--

6 TO 12	76.70	3				
-12 TO -6	75.37	7	1.33	0.610	1.860	NO

\*\*\*\*\*  
 --HEAVY TRUCKS--

6 TO 12	77.87	41				
-12 TO -6	77.80	7	0.07	0.066	1.680	NO

\*\*\*\*\*  
 \*\*5 MIC SITES--MIC. #5\*\*

--ALL AUTOS--

VECTOR RANGE (MPH)	MEAN (DBA)	#VEH.	DIF. (X-Y)	CALC. "T"	CRIT. "T"	SIG. &=.05
6 TO 12	69.88	17				
-12 TO -6	69.23	48	0.65	0.939	1.670	NO

\*\*\*\*\*  
 --MEDIUM TRUCKS--

6 TO 12	76.83	3				
-12 TO -6	77.44	7	-.61	-.325	1.860	NO

\*\*\*\*\*  
 --HEAVY TRUCKS--

6 TO 12	78.15	41				
-12 TO -6	77.59	7	0.56	0.565	1.680	NO

\*\*\*\*\*  
 --NOTE: SECOND MEAN ADJUSTED BY THE DIFFERENCE AT MIC. #1.

VI. CALIFORNIA VEHICLE NOISE REFERENCE  
ENERGY MEAN EMISSION LEVELS

Figure XI-1 presents the California Vehicle Noise Reference Energy Mean Emission levels. The speed dependent curves were developed from the measured data at 50 feet from the centerline of vehicle travel at a height of 5 feet, using the methodologies and criteria discussed in the previous chapters. The curves should be used only for vehicles traveling at constant speed from 25 mph to 65 mph, on level roadways (within ± 1% gradient).

Definitions of the three vehicle groups are identical to those defined in FHWA-RD-77-108(2).

This study did not attempt to verify existing source heights reported by FHWA-RD-77-108, nor did this study attempt to determine new source heights for autos, medium and heavy trucks.

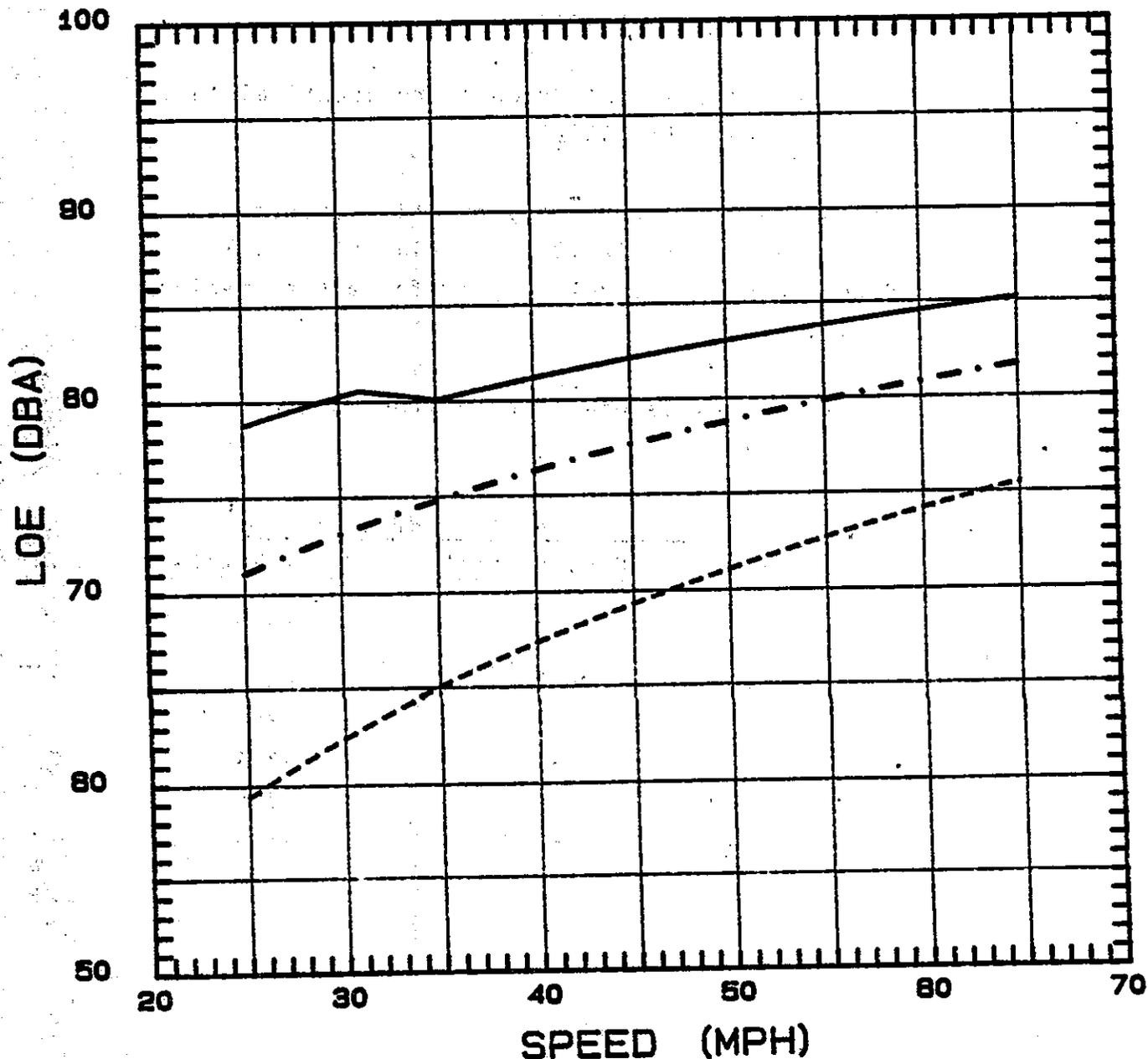
A summary of differences between the California and FHWA-RD-77-108 follows:

<u>Speed (mph)</u>	<u>California - FHWA, dBA</u>		
	<u>Autos</u>	<u>Medium Trucks</u>	<u>Heavy Trucks</u>
31	0.8	-0.5	+0.2
35	0.8	-0.9	-1.6
40	0.8	-1.4	-1.8
45	0.8	-1.8	-2.2
50	0.9	-2.2	-2.4
55	0.9	-2.5	-2.6
60	1.0	-2.9	-2.8

# FIGURE XI-1 CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

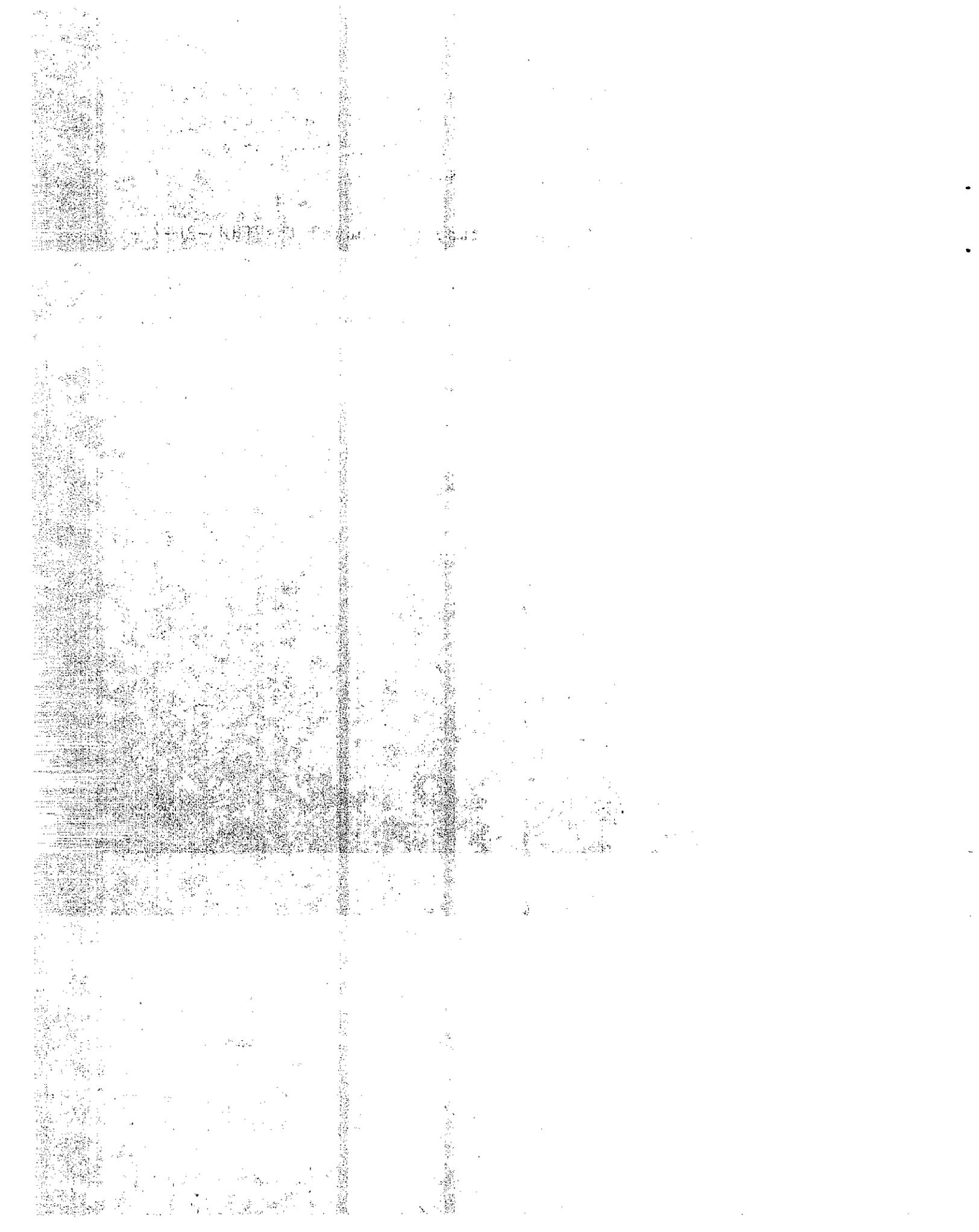
ALL SITES  
MIC.#2 HT-5FT. DIST-50FT.

- |           |                          |                                |               |
|-----------|--------------------------|--------------------------------|---------------|
| -----     | VEH. TYPE: ALL AUTOS     | $LOE = 5.2 + 38.8 * LOG(MPH)$  |               |
| - · - · - | VEH. TYPE: MEDIUM TRUCKS | $LOE = 35.3 + 25.6 * LOG(MPH)$ |               |
| ————      | VEH. TYPE: HEAVY TRUCKS  | $LOE = 51.9 + 19.2 * LOG(MPH)$ | 25 < MPH < 31 |
|           |                          | $LOE = 50.4 + 19.2 * LOG(MPH)$ | 35 < MPH < 65 |
|           |                          | STRAIGHT LINE TRANSITION       | 31 < MPH < 35 |



It is estimated that for average traffic conditions at 55 mph, noise levels predicted with the California emission levels will be approximately 2 dBA lower than those predicted with the National emission levels.

A 1981 California TransLab study (7) showed the FHWA-RD-77-108(2) to overpredict by 3 to 4 dBA. This overprediction was partially due to the use of National emission levels. With California emission levels, the overpredictions would be reduced to about 1 to 2 dBA.



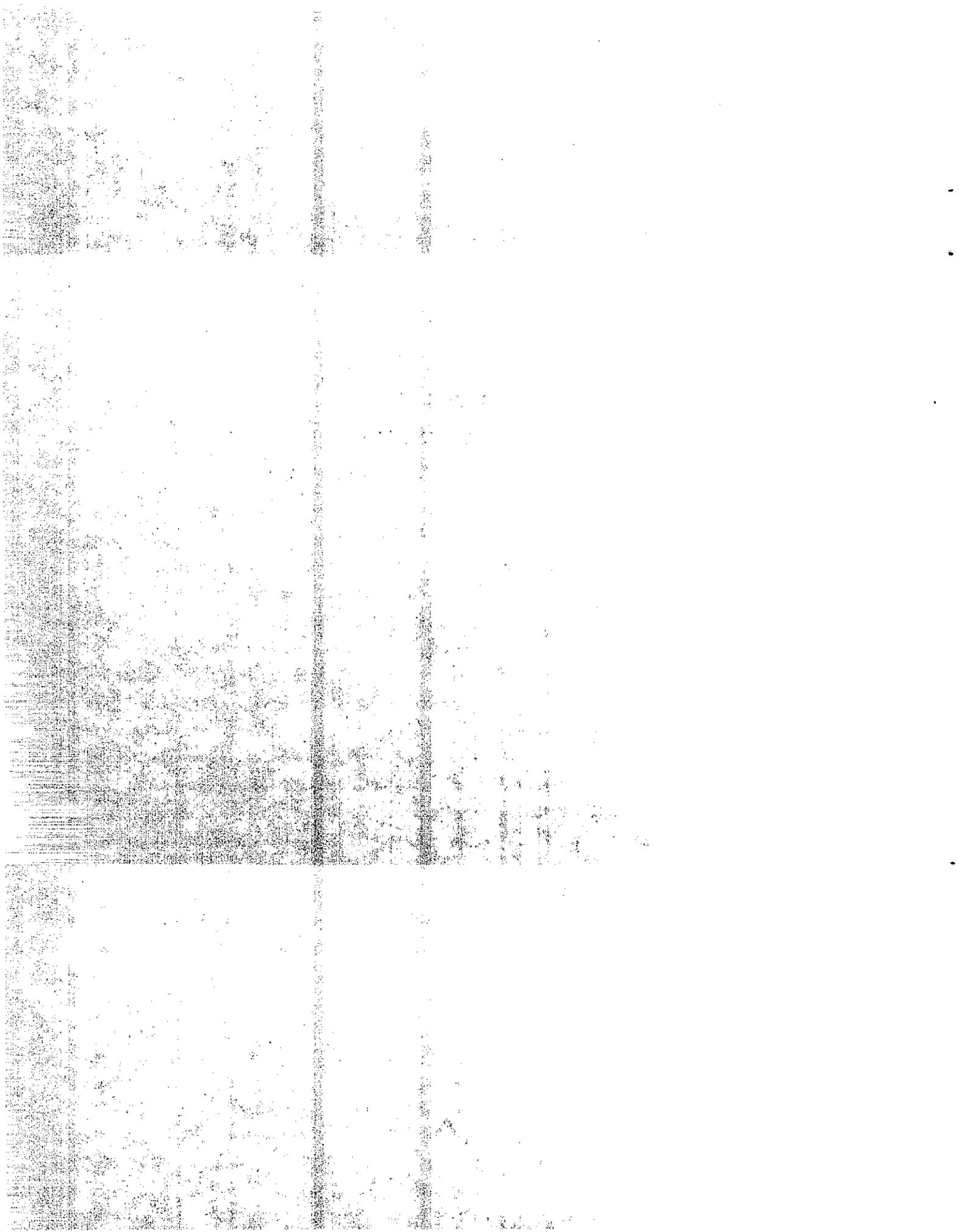
## REFERENCES

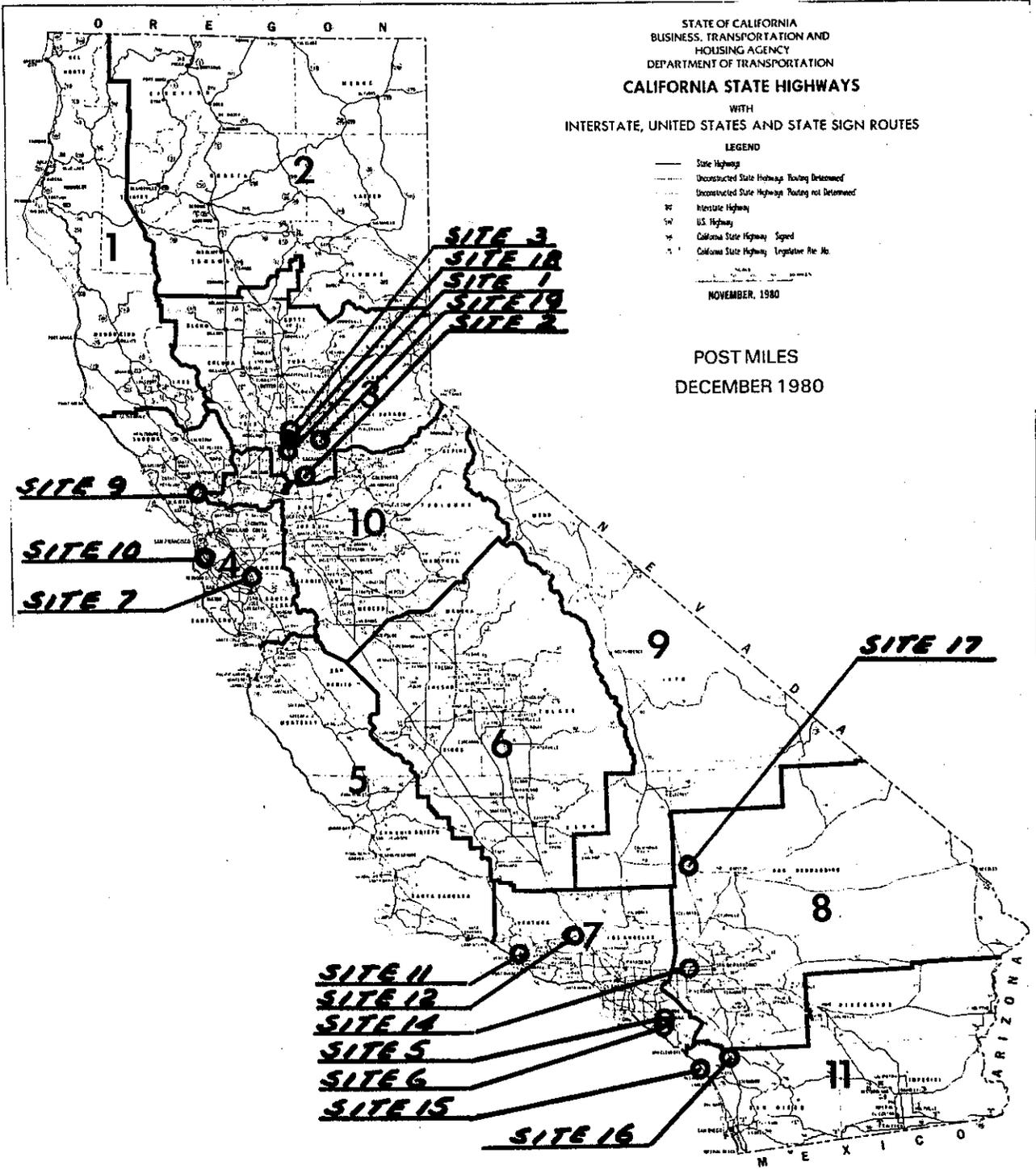
1. Federal-Aid Highway Program Manual, Vol. 7, Ch. 7, Sec. 3, Federal Highway Administration, August 9, 1982.
2. Barry, T. M., and Reagan, J. A., FHWA Highway Traffic Noise Prediction Model, Federal Highway Administration, FHWA-RD-77-108, December 1978.
3. Bowlby, W., Sound Procedures for Measuring Highway Noise: Final Report, Federal Highway Administration, FHWA-DPO-45-1R, August 1981.
4. Rudder, F. F., Jr., and Lam, P., Update of TSC Highway Traffic Noise Prediction Code (1974), Federal Highway Administration, FHWA-RD-77-19, January 1977.
5. Ma, Y. Y., and Rudder, F. F., Jr., Statistical Analysis of FHWA Traffic Noise Data, Federal Highway Administration, FHWA-RD-78-64, July 1978.
6. Rickley, E. J., Ford, D. W., and Quinn, R. W., Highway Noise Measurements for Verification of Prediction Models, Federal Highway Administration, DOT-TSC-FHAW-78-1, April 1976.
7. Hendriks, R. W., and Hatano, M. M., Evaluation of Noise Barriers, California Department of Transportation, Office of Transportation Laboratory, June 1981.

8. Reagan, J. A., Determination of Reference Energy Mean Emission Levels, Federal Highway Administration, FHWA-OEP/HEV-78-1, July 1978.
9. Design Information Bulletin No. 58 - Noise Barrier, California Department of Transportation, Office of Planning and Design, Memorandum dated December 8, 1980.
10. Specification for Sound Level Meters, American National Standards Institute (ANSI), S 1.4 - 1983.
11. Sasor, R. S., Determination of Truck Noise Levels for New Jersey, New Jersey Department of Transportation, Division of Research and Development, July 1980.
12. Bowker, A. H., Lieberman, G. J., Engineering Statistics, Second Edition, Prentice-Hall, Inc., 1972.
13. Scholes, W. E., Salridge, A. C., and Sargent, J. W., "Field Performance of a Noise Barrier," Reprint from Journal of Sound and Vibration, Vol. 16, No. 4, 1971 pp. 627-642, Building Research Station Current Paper 24/71, August 1971.
14. Foss, R. N., Ground Plane Wind Shear Interaction on Acoustic Transmission, Washington State Highway Commission, June 1978.

APPENDIX A  
SITE DETAILS

A



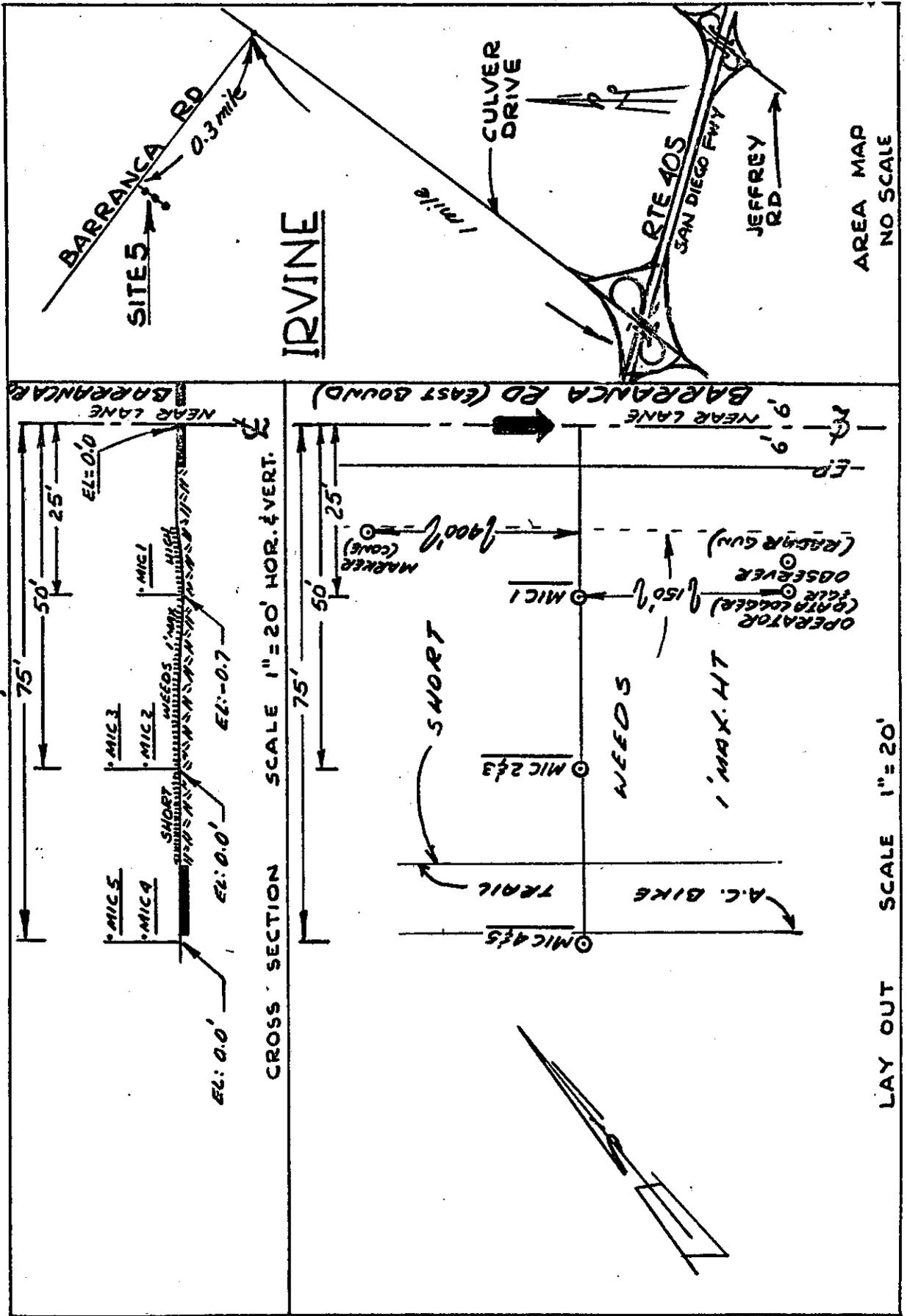


*Figure A-1 Locations Of  
Noise Measurement Sites*



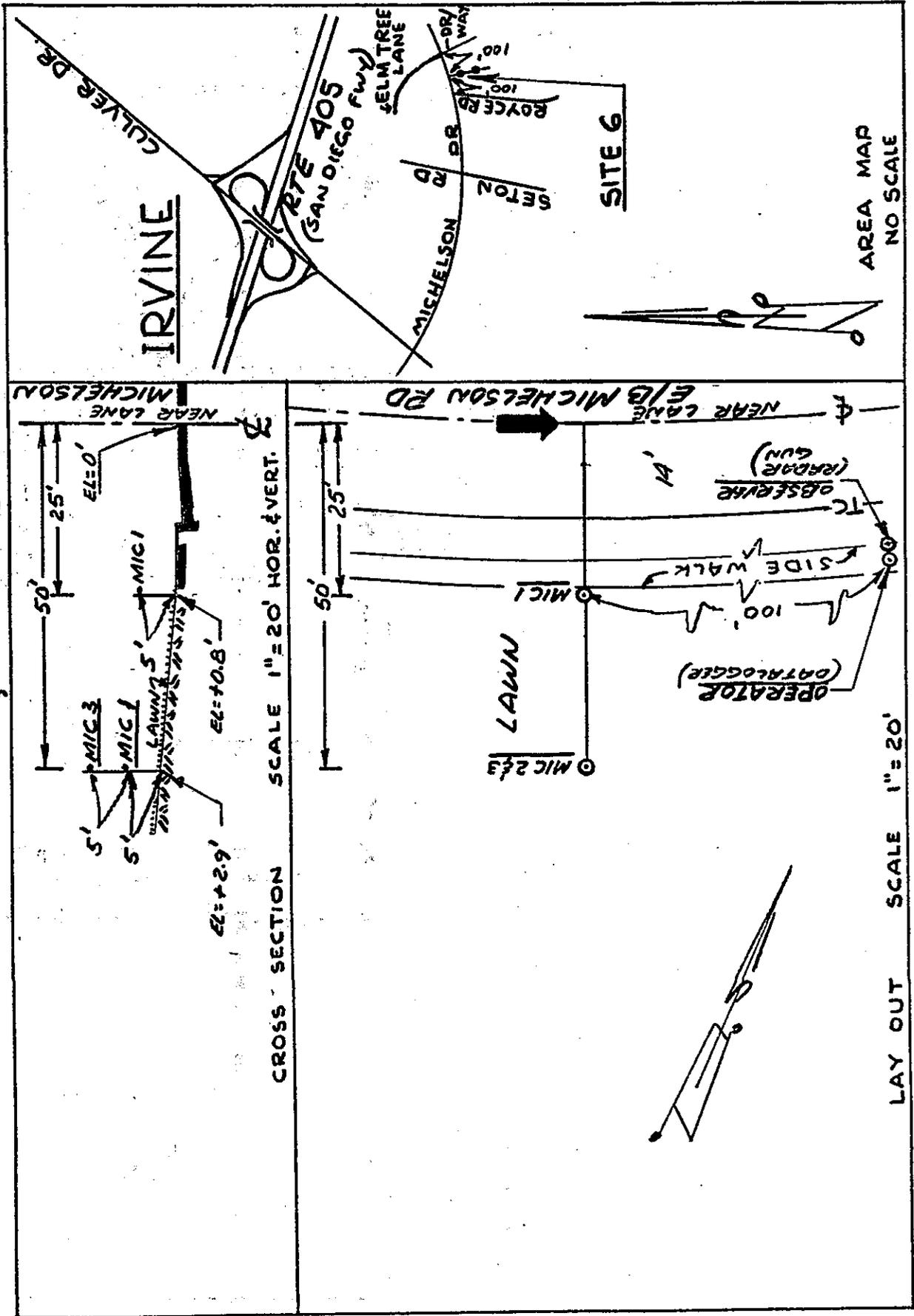
FIGURE A-5 SITE: 5, "BARRANCA"

CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
SITE: 5, "BARRANCA"



CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 6, "MICHELSON"

FIGURE A-6 SITE 6, "MICHELSON"



CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 7, "MISSION"

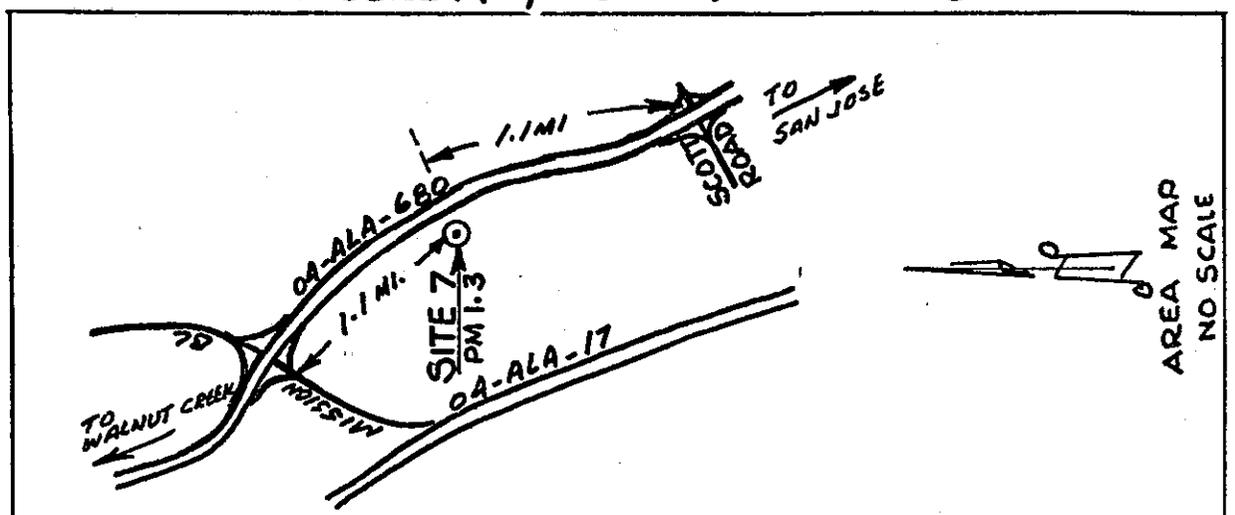
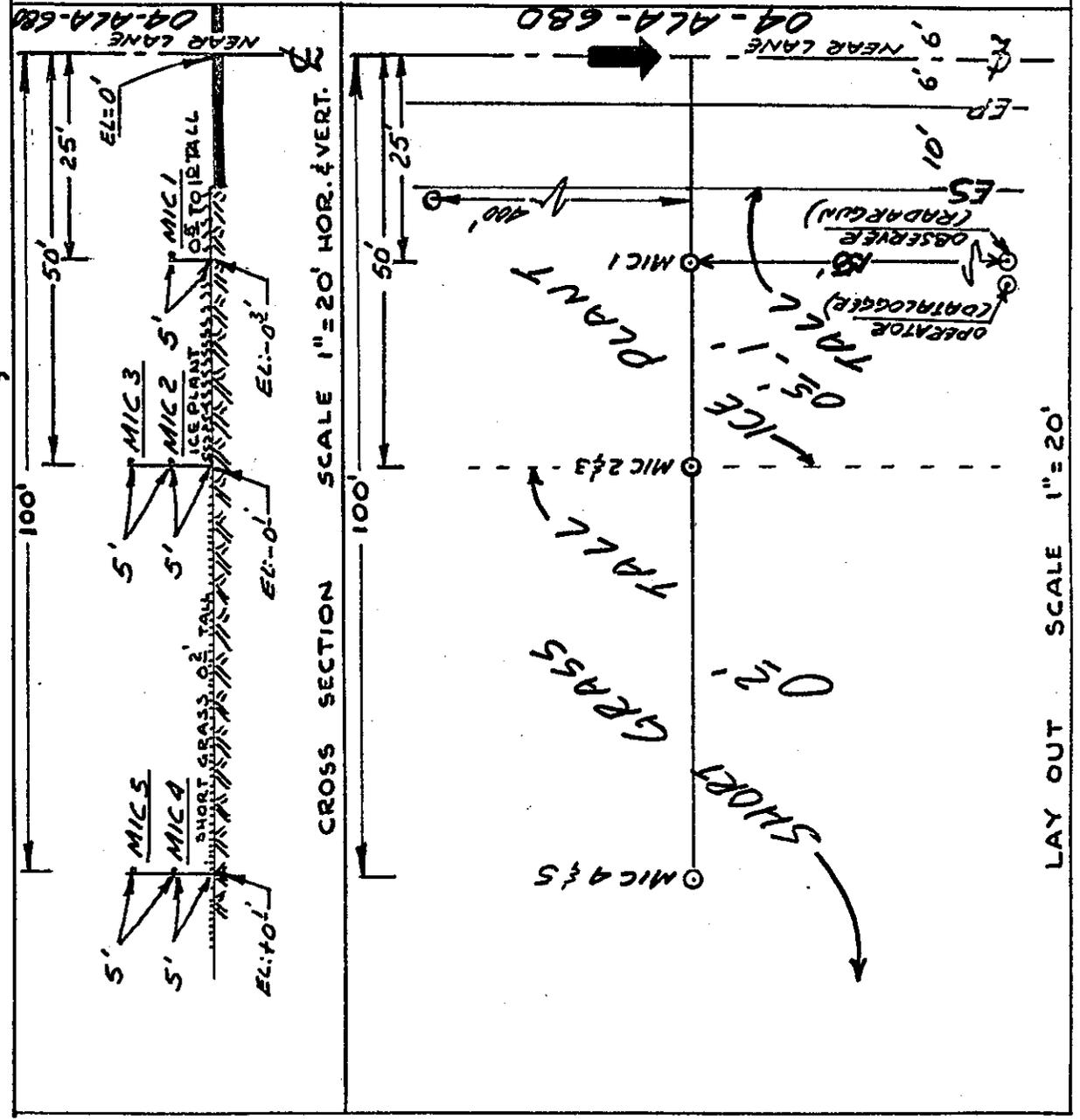


FIGURE A-8 SITE 9, "WEIGH STATION"

CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
SITE: 9, "WEIGH STATION"

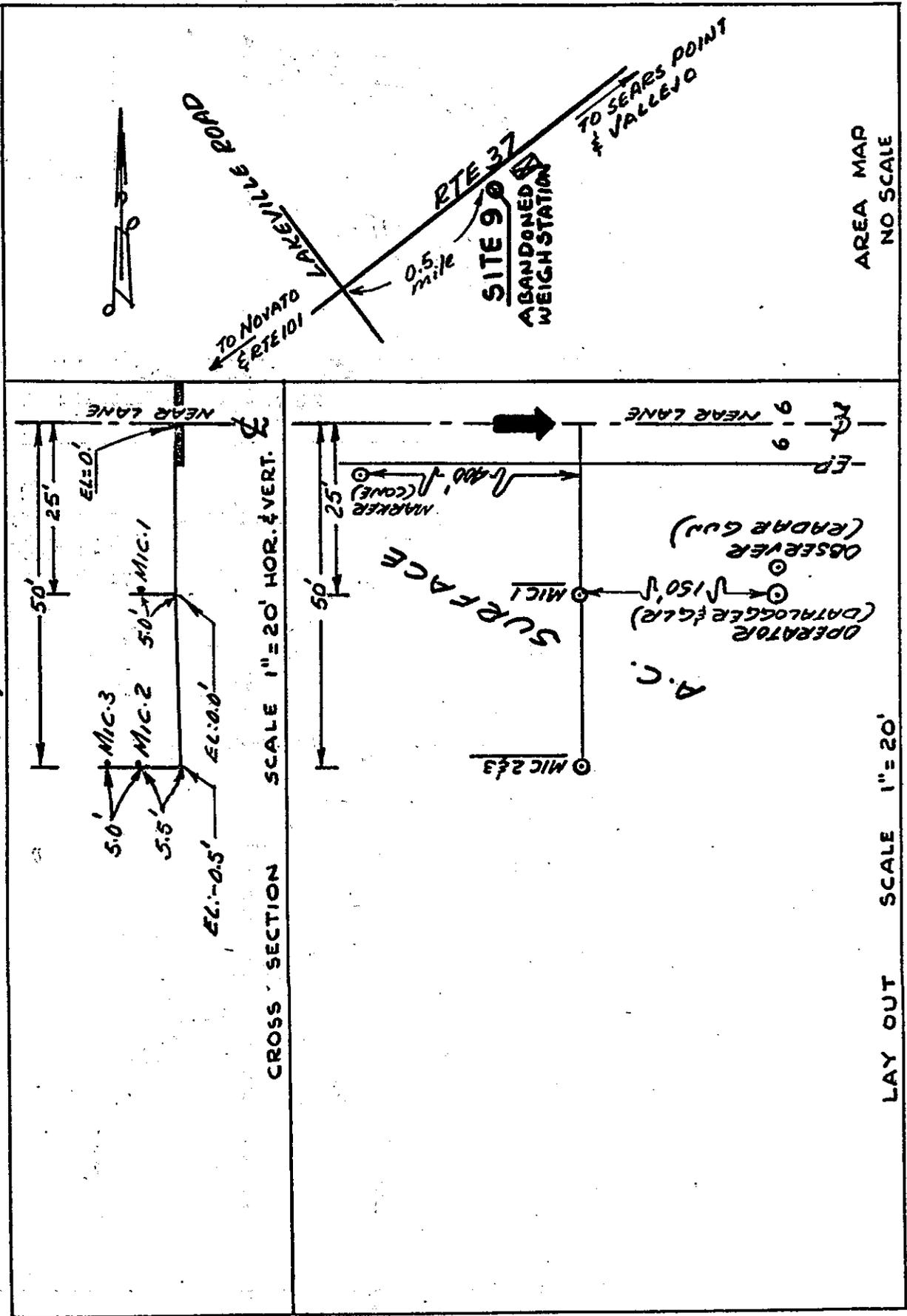


FIGURE A-9 SITE 10

CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 10, "HILLSBOROUGH"

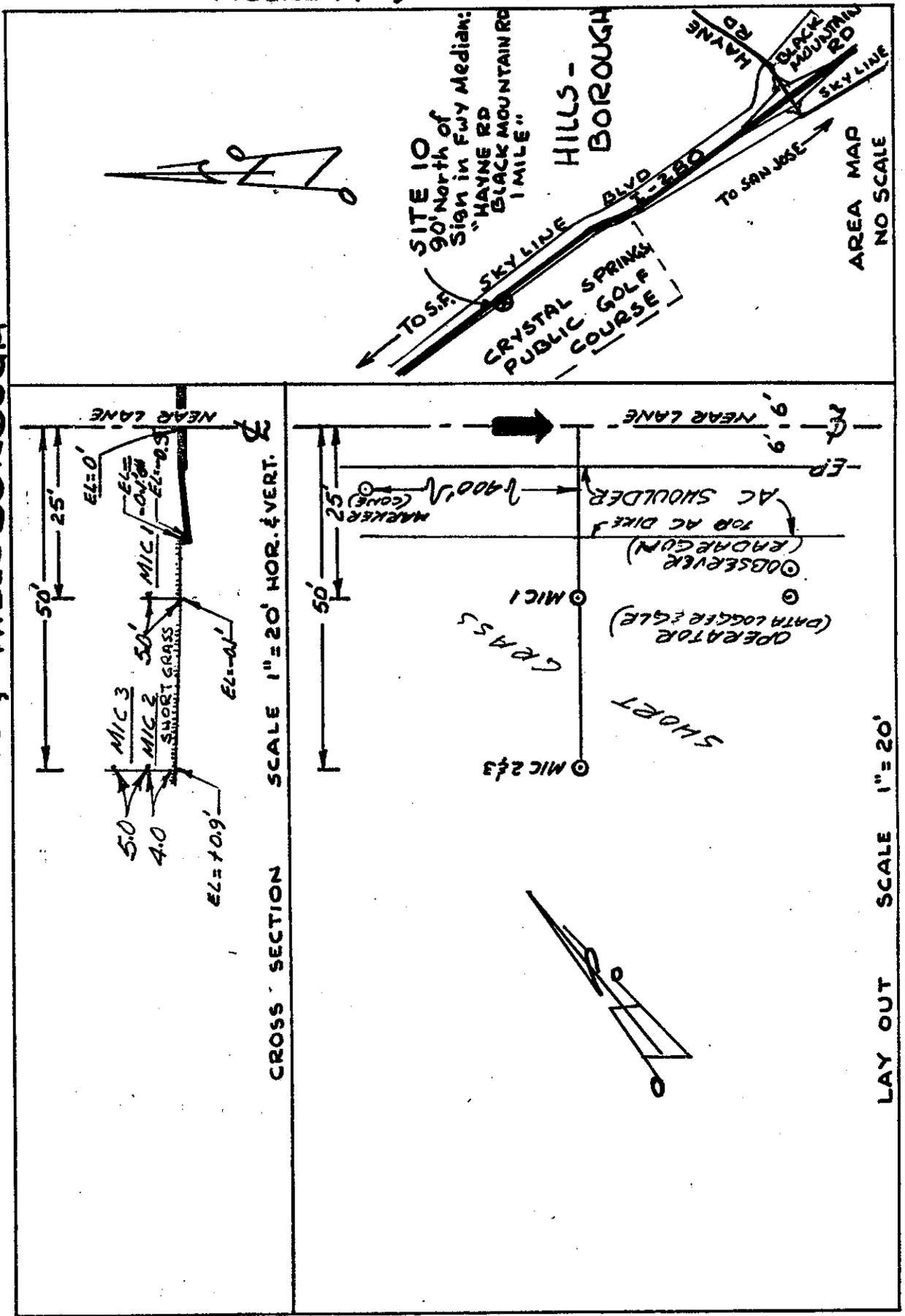
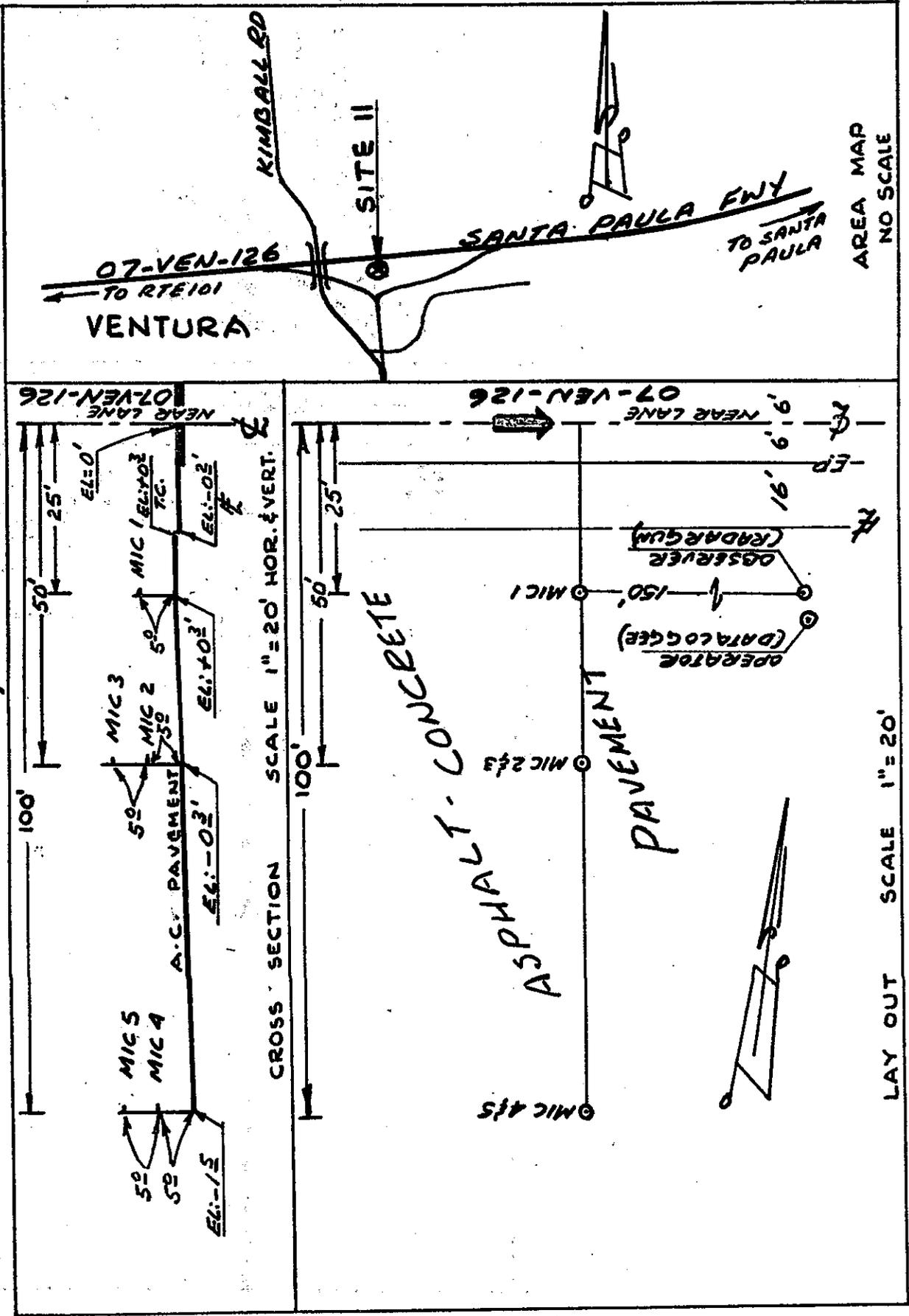


FIGURE A-10 SITE II

CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: II, "KIMBALL"



AREA MAP  
NO SCALE

LAY OUT SCALE 1" = 20'

CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 12, "INDIAN DUNES"

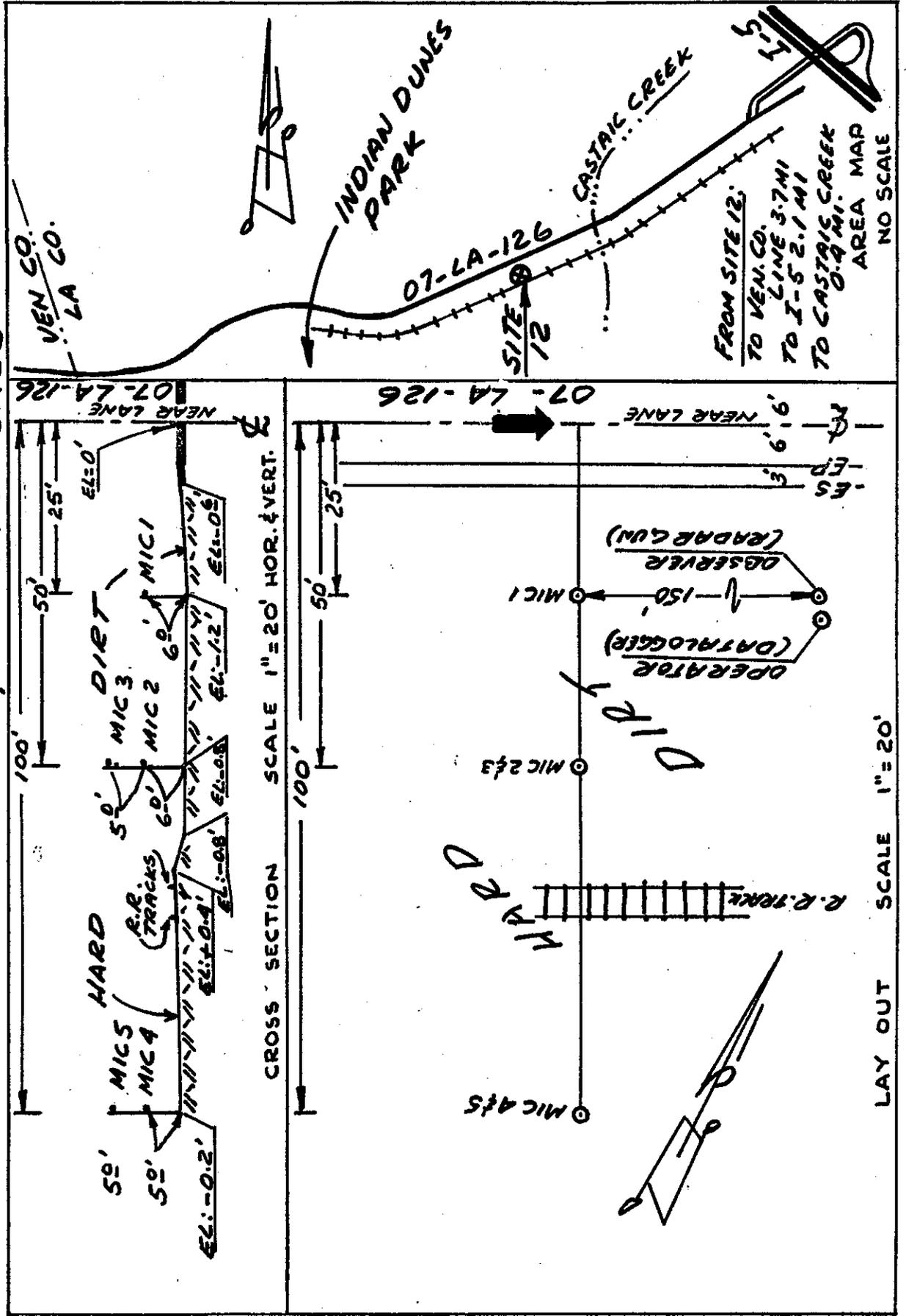
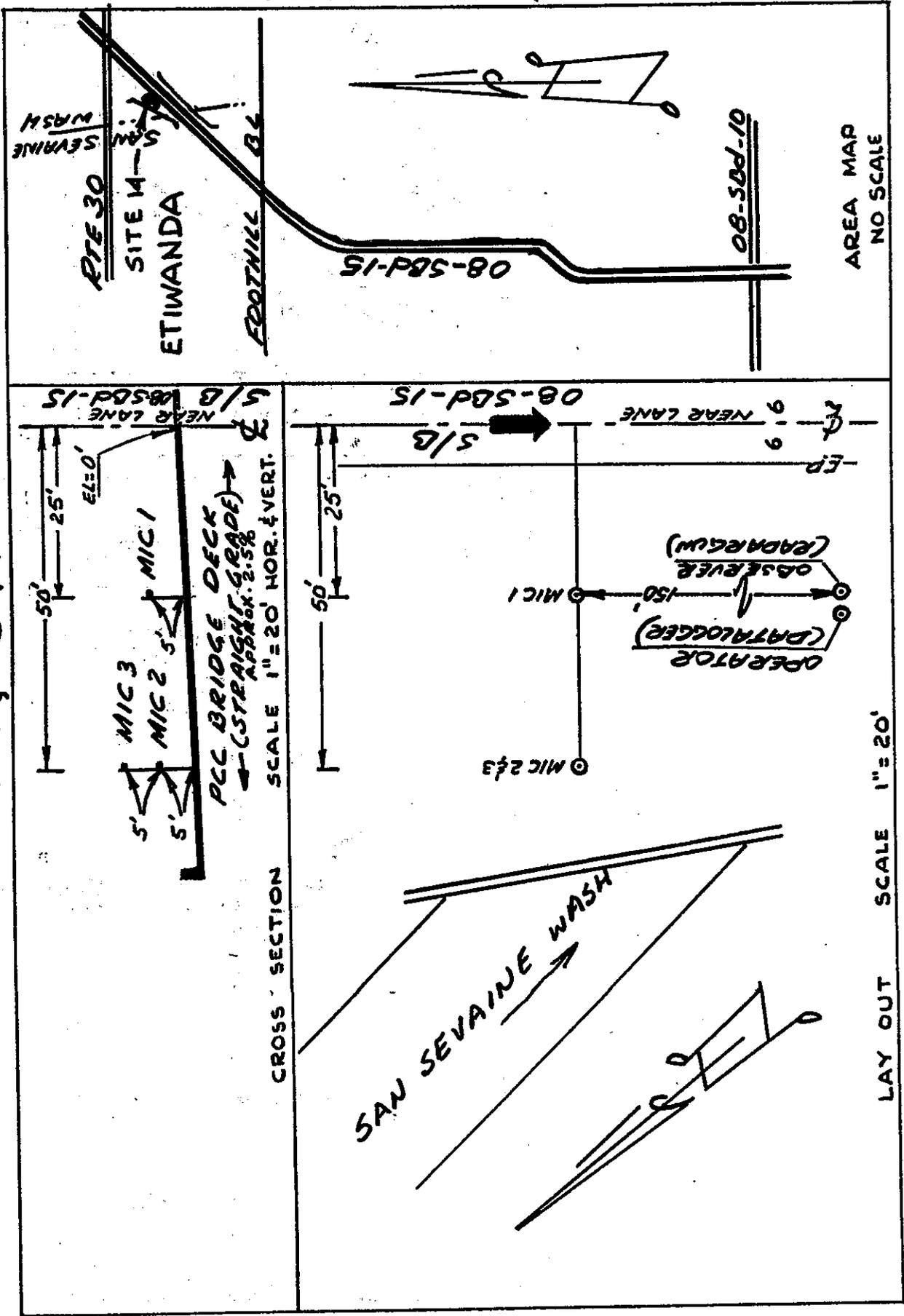


FIGURE A-12 SITE 14

CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 14, "SAN SEVAINÉ"



CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 15, "OCEANSIDE"

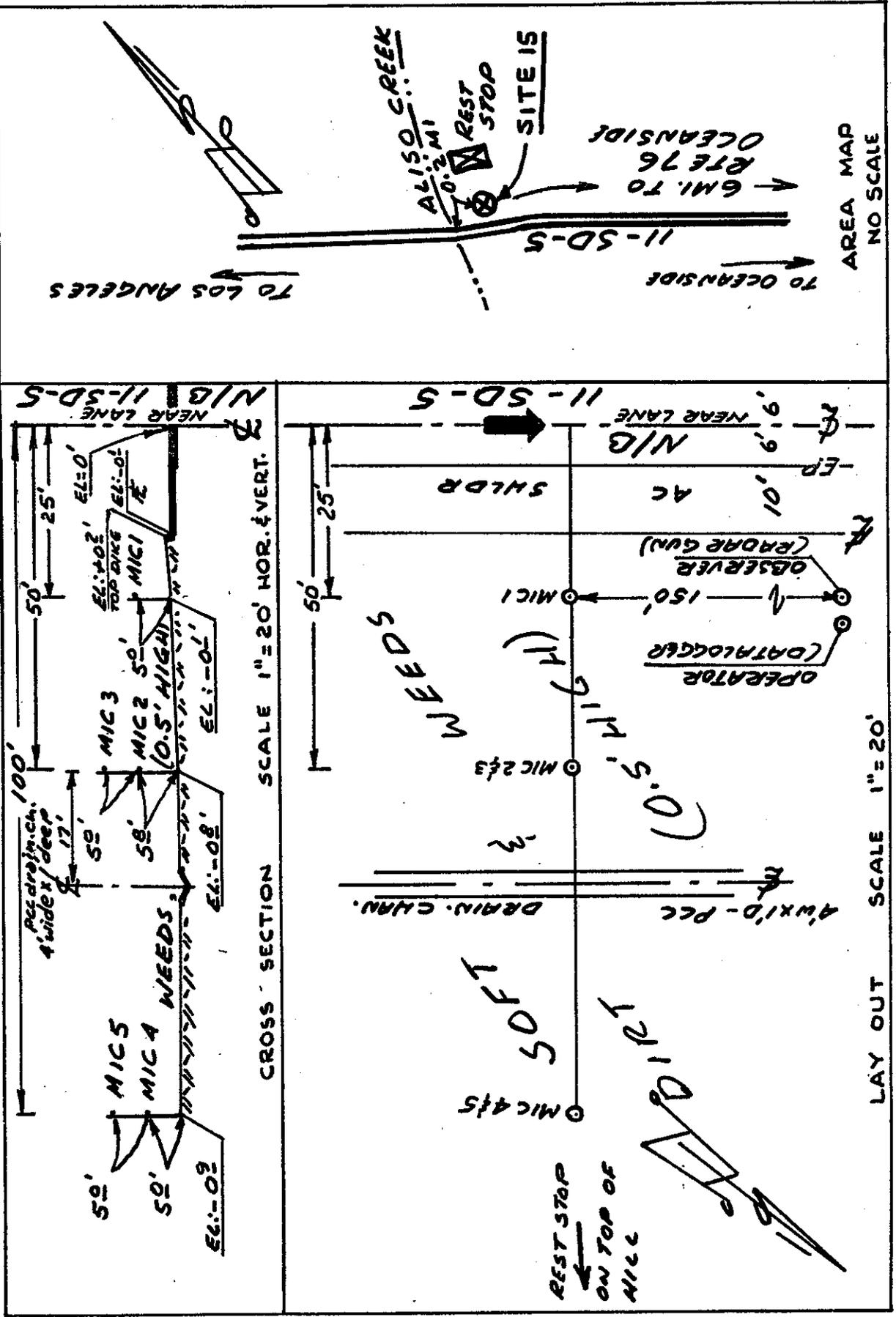
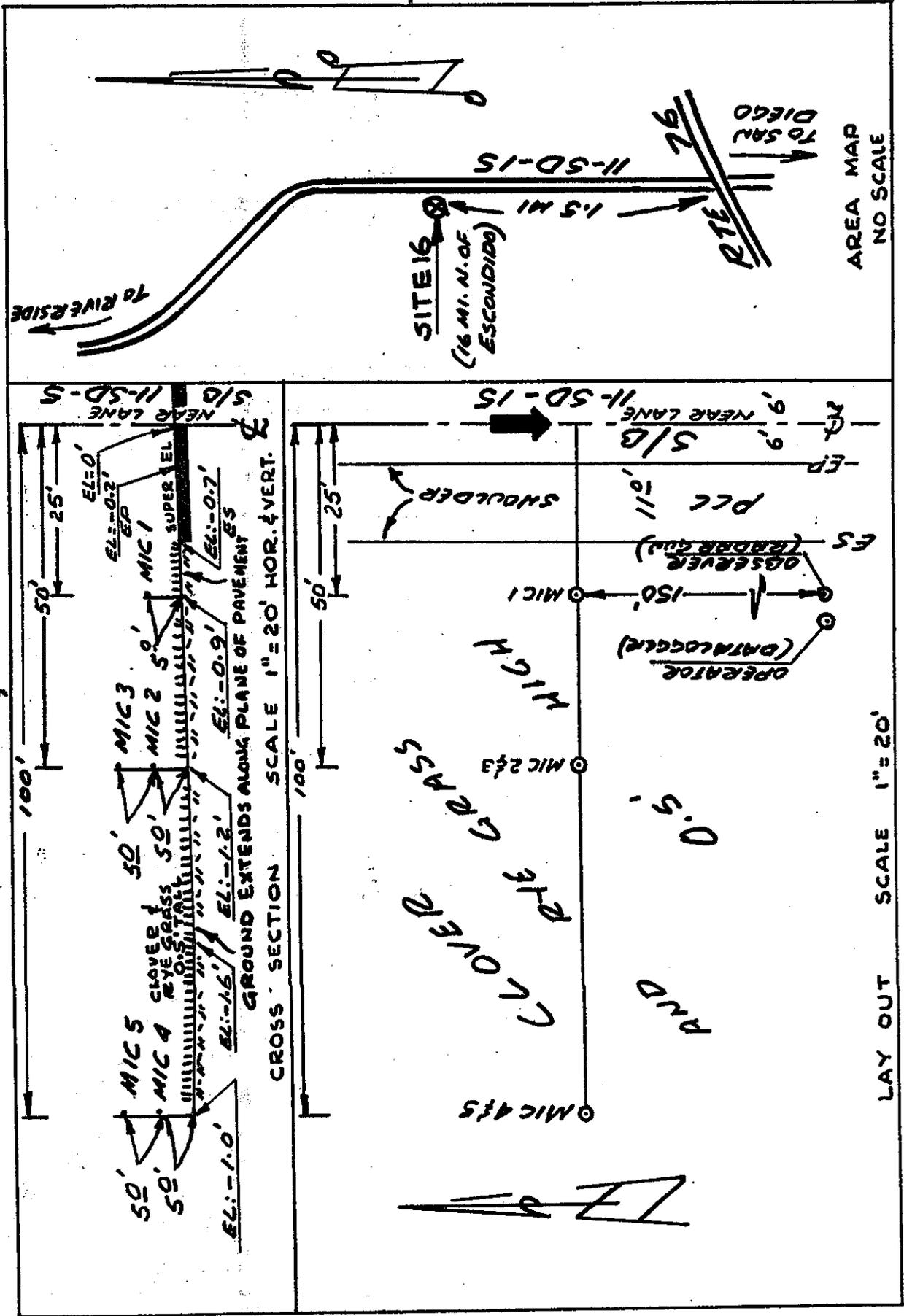
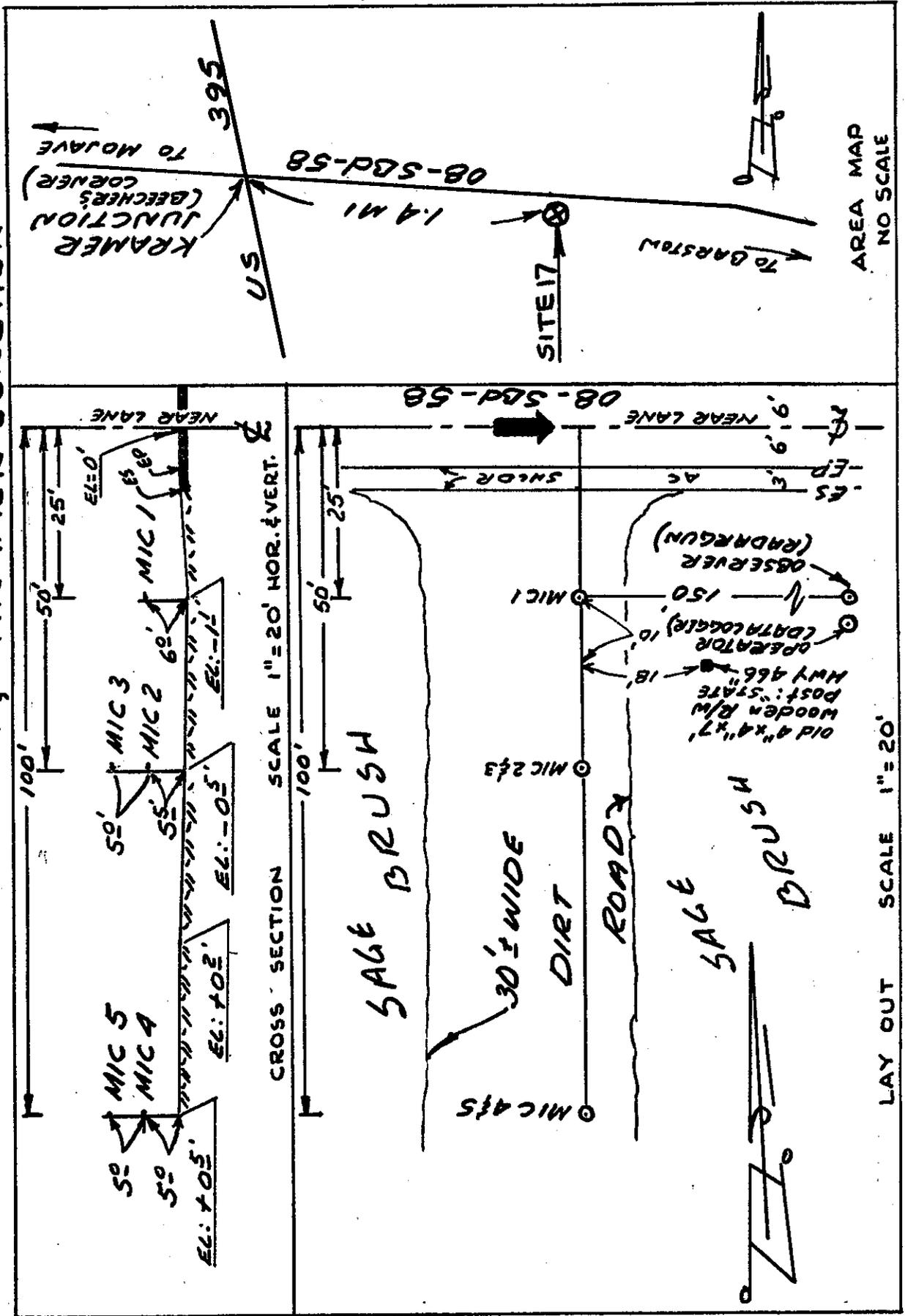


FIGURE A-14 SITE 16

CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 16, "HALF FIFTEEN"

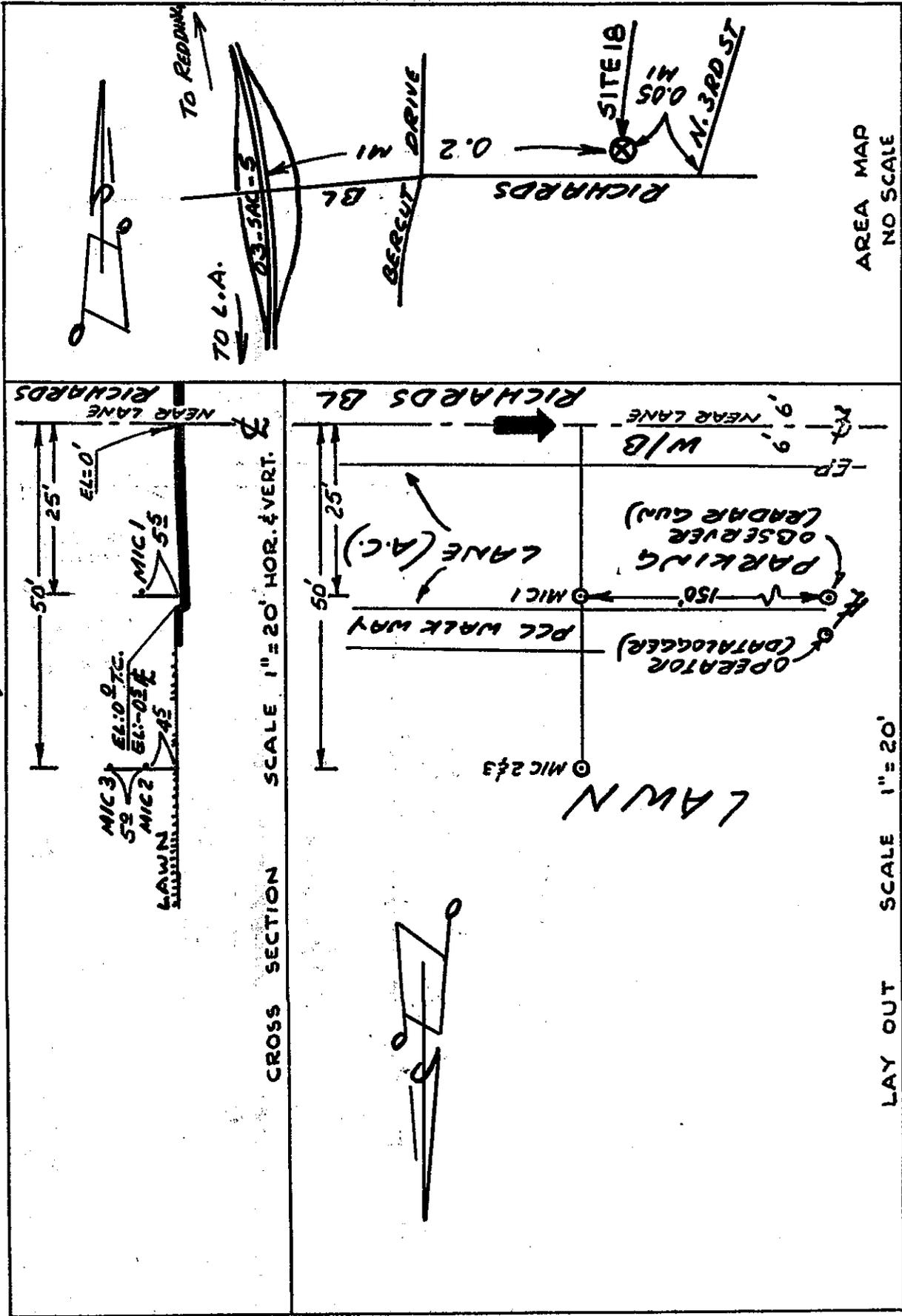


CALIFORNIA VEHICLE NOISE EMISSION LEVELS  
 SITE: 17, "KRAMER JUNCTION"



# CALIFORNIA VEHICLE NOISE EMISSION LEVELS SITE: 18, "RICHARDS"

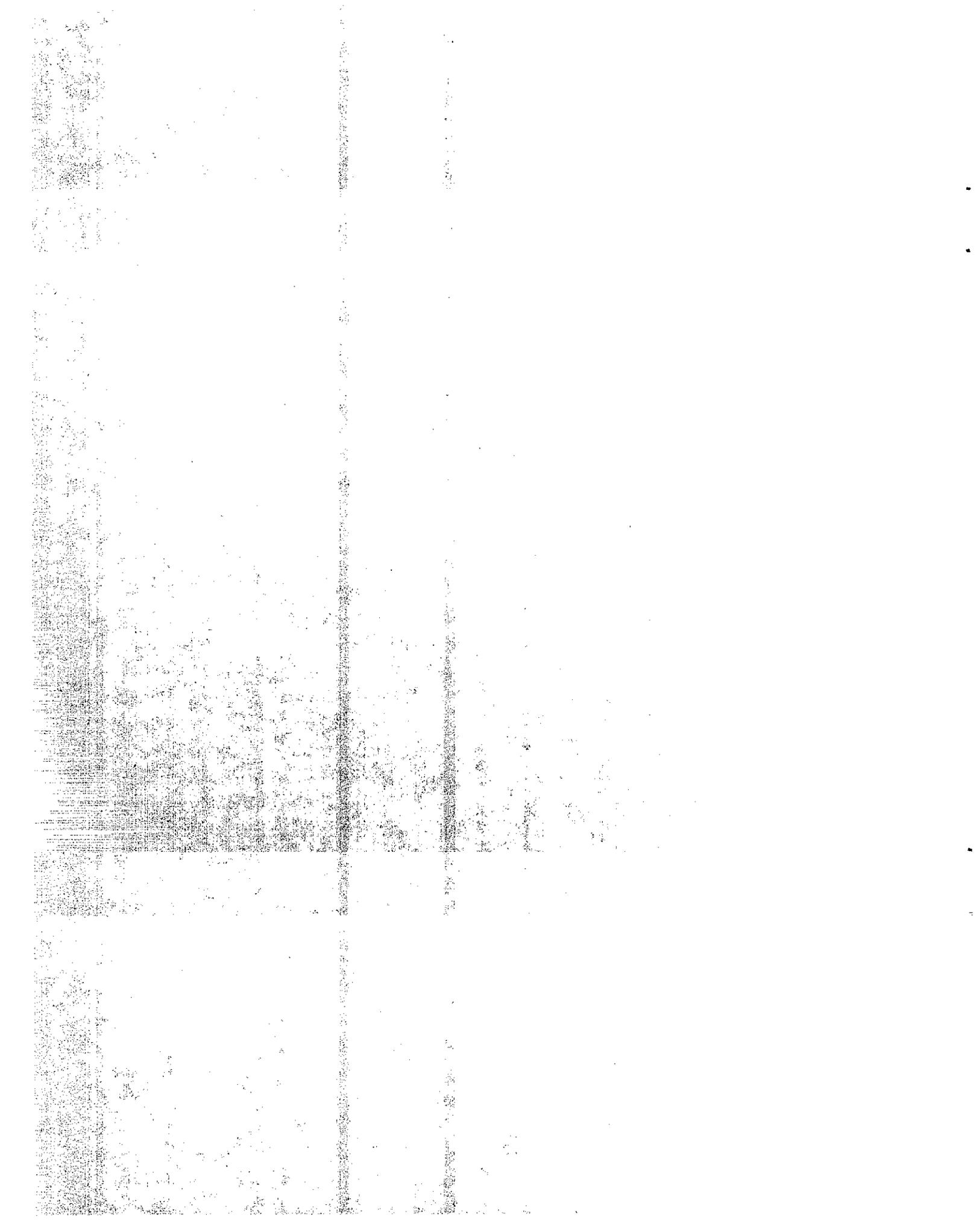
FIGURE A-16 SITE 18







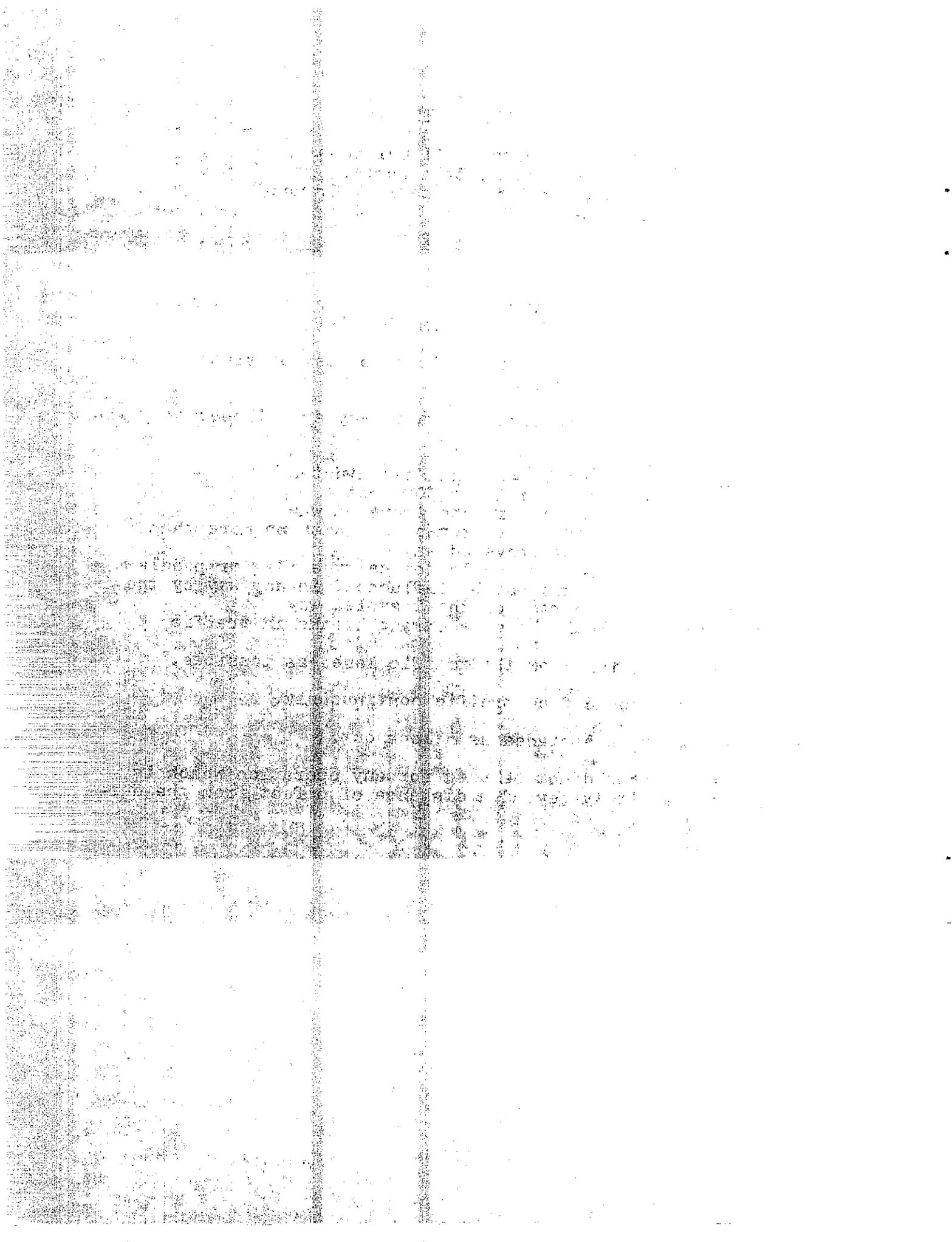
APPENDIX B  
SAFETY



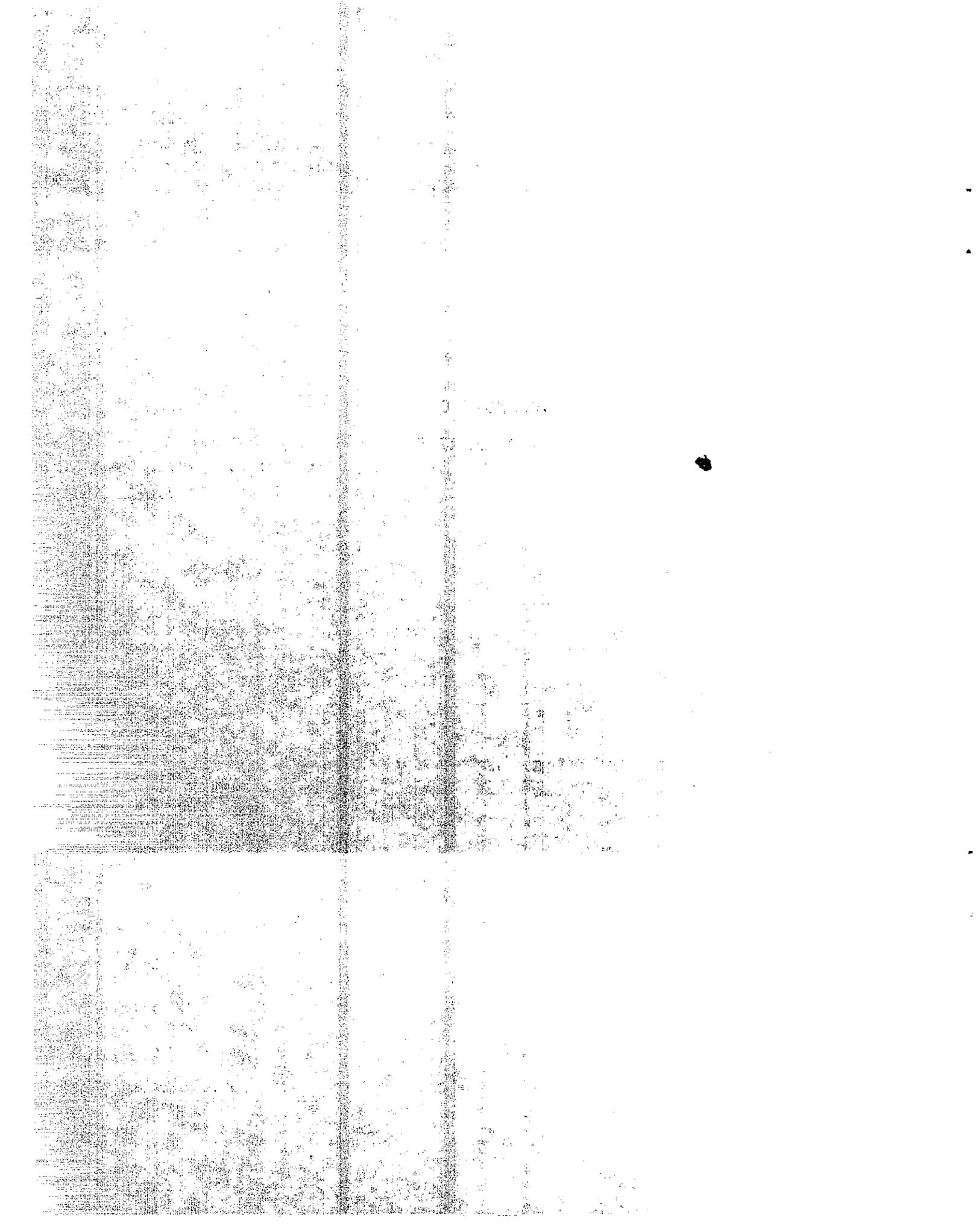
## ROADSIDE SAFETY

(References: Chapter VIII Caltrans  
Maintenance Manual, Transportation  
Laboratory And Enviro-Chemical Branch  
Safety Codes.)

1. All personnel must wear hard hats, orange shirts or vests, and safety glasses when working in the field.
2. When ever practical, maintain at least 6 feet of spabe between moving traffic and work area.
3. Brief excursions on the outside travel way are allowed only when:
  - \* Traffic is light
  - \* Excursion is not longer than two minutes
  - \* Sight distance is at least 500 feet
  - \* Vehicles are parked off the traveled way
  - \* Crew consists of at least two men, with no more than one person on the traveled way
  - \* The look out person should not carry a flag or paddle
  - \* The traffic should not be influenced in any way by the presence of a person on the traveled way
  - \* Excursions should be done during breaks in traffic
4. Park vehicles as far from the traffic lanes as possible.
5. Crews on foot should face traffic continuously.
6. One person must be assigned as a look out.
7. Warning signs should not be used for any operation which is carried out entirely beyond a distance of 6 feet from the outside edge of shoulder.



APPENDIX C  
DATA SUMMARIES



\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	WE	DATE					
SITE	QUAL.	TYPE	(1)	(2)	(3)	(4)	(5)					
EVENT	G L E	D N V	(1)	(2)	(3)	(4)	(5)					
TYPE	R H L	N V	5	5	10	5	10					
			DBA									
1	1	2 1 1 1	1 63	80.3	74.4	74.5	62.5	70.1	3	180	-4.5	8/17/82
1	2	2 1 1 1	3 58	90.7	83.9	85.0	77.5	78.4	3	180	-4.5	8/17/82
1	3	2 1 1 1	4 59	91.0	84.1	84.9	75.8	79.4	3	180	-4.5	8/17/82
1	4	2 1 1 1	1 58	75.7	70.3	71.8	59.0	66.8	3	180	-4.5	8/17/82
1	5	2 0 0 1	5 61	91.4	86.2	86.4	76.6	81.0	3	180	-4.5	8/17/82
1	6	2 1 1 1	5 63	90.6	84.3	85.7	75.4	79.2	3	180	-4.5	8/17/82
1	7	2 1 1 1	5 64	90.3	83.8	84.1	76.3	79.0	3	180	-4.5	8/17/82
1	8	2 1 1 1	5 61	95.1	88.7	89.2	81.7	83.6	3	180	-4.5	8/17/82
1	9	2 0 0 1	7 56	79.9	73.9	74.3	66.1	70.2	3	180	-4.5	8/17/82
1	10	2 0 0 1	7 58	75.0	55.6	62.2	50.3	56.5	3	180	-4.5	8/17/82
1	11	2 1 1 1	3 55	83.5	77.2	77.4	69.0	71.4	3	180	-4.5	8/17/82
1	12	2 1 1 1	1 58	79.6	73.2	73.3	64.9	68.1	3	180	-4.5	8/17/82
1	13	2 1 1 1	1 60	82.1	75.8	76.2	65.1	69.9	3	180	-4.5	8/17/82
1	14	2 1 1 1	1 53	79.8	73.2	74.0	60.3	68.5	3	180	-4.5	8/17/82
1	15	2 1 1 1	1 66	85.7	79.0	79.6	69.1	73.0	3	180	-4.5	8/17/82
1	16	2 1 1 1	5 69	94.9	88.4	89.9	81.7	83.3	3	180	-4.5	8/17/82
1	17	2 1 1 1	1 56	77.9	72.0	72.7	62.7	67.7	3	180	-4.5	8/17/82
1	18	2 1 1 1	5 54	90.4	84.8	84.1	76.2	78.6	3	180	-4.5	8/17/82
1	19	2 1 1 1	5 57	92.9	86.3	87.6	75.4	80.6	3	180	-4.5	8/17/82
1	20	2 1 1 1	5 59	91.0	84.8	85.4	75.5	79.7	3	180	-4.5	8/17/82
1	21	2 1 1 1	1 64	81.4	75.5	74.9	64.7	71.1	3	180	-4.5	8/17/82
1	22	2 1 1 1	5 59	90.2	84.0	84.2	74.6	78.2	3	180	-4.5	8/17/82
1	23	2 1 1 1	5 63	88.5	82.6	83.0	73.5	76.6	3	180	-4.5	8/17/82
1	24	2 1 1 1	5 61	89.0	82.2	83.0	73.6	77.5	3	180	-4.5	8/17/82
1	25	2 1 1 1	1 54	82.0	76.3	76.8	62.8	70.0	3	180	-4.5	8/17/82
1	26	2 1 1 1	1 61	79.9	74.4	74.7	62.8	69.3	3	180	-4.5	8/17/82
1	27	2 1 1 1	1 54	78.9	73.5	74.7	62.7	68.8	3	180	-4.5	8/17/82
1	28	2 1 1 1	1 56	79.3	73.0	72.9	61.7	68.0	3	180	-4.5	8/17/82
1	29	2 1 1 1	5 57	90.2	83.7	84.6	76.0	78.0	3	180	-4.5	8/17/82
1	30	2 1 1 1	1 57	75.8	70.4	70.9	59.9	66.1	3	180	-4.5	8/17/82
1	31	2 1 1 1	5 59	89.6	84.0	84.6	75.1	80.3	3	180	-4.5	8/17/82
1	32	2 1 1 1	1 61	80.2	74.6	74.4	61.9	69.8	3	180	-4.5	8/17/82
1	33	2 1 1 1	5 60	91.4	85.0	85.1	76.1	79.6	3	180	-4.5	8/17/82
1	34	2 1 1 1	1 64	81.7	74.6	74.5	60.2	70.5	3	180	-4.5	8/17/82
1	35	2 1 1 1	5 62	95.2	89.2	89.2	82.5	83.1	3	180	-4.5	8/17/82
1	36	2 1 1 1	3 52	87.5	81.0	82.3	72.9	75.8	3	180	-4.5	8/17/82
1	37	2 0 0 1	5 61	95.6	89.5	91.3	83.6	86.3	3	180	-4.5	8/17/82
1	38	2 1 1 1	1 61	76.6	70.9	71.3	58.8	66.7	3	180	-4.5	8/17/82
1	39	2 1 1 1	2 58	83.4	77.4	77.7	64.4	72.5	3	180	-4.5	8/17/82
1	40	2 1 1 1	5 46	89.2	83.9	83.4	72.9	77.2	3	180	-4.5	8/17/82
1	41	2 1 1 1	5 64	91.5	84.7	85.7	77.2	79.8	3	180	-4.5	8/17/82
1	42	2 1 1 1	5 58	89.4	84.0	84.5	73.5	79.0	3	180	-4.5	8/17/82
1	43	2 1 1 1	5 56	88.2	82.0	82.5	73.5	76.1	3	180	-4.5	8/17/82
1	44	2 1 1 1	5 62	91.1	84.3	85.5	74.1	79.3	3	180	-4.5	8/17/82
1	45	2 1 1 1	1 61	79.3	72.9	72.7	62.9	67.9	3	180	-4.5	8/17/82
1	46	2 1 1 1	5 62	88.3	82.1	83.0	74.0	76.5	3	180	-4.5	8/17/82
1	47	2 1 1 1	1 62	82.5	76.2	76.6	63.7	70.4	3	180	-4.5	8/17/82
1	48	2 1 1 1	5 65	91.8	85.6	86.3	75.7	81.1	3	180	-4.5	8/17/82
1	49	2 0 0 1	5 60	85.2	80.4	81.1	72.5	76.6	3	180	-4.5	8/17/82
1	50	2 1 1 1	5 61	88.4	81.6	82.7	73.6	76.9	3	180	-4.5	8/17/82
1	51	2 1 1 1	5 56	90.5	84.5	84.5	76.0	79.1	3	180	-4.5	8/17/82
1	52	2 1 1 1	5 55	89.5	83.5	83.8	71.0	78.5	3	180	-4.5	8/17/82
1	53	2 1 1 1	1 60	79.8	72.9	74.0	62.2	68.1	3	180	-4.5	8/17/82
1	54	2 1 1 1	5 56	92.1	86.2	86.1	76.4	81.0	3	180	-4.5	8/17/82
1	55	2 0 0 1	5 44	86.5	80.0	80.4	70.1	75.6	3	180	-4.5	8/17/82
1	56	2 1 1 1	5 44	85.6	79.6	79.7	70.7	73.6	3	180	-4.5	8/17/82
1	57	2 1 1 1	5 63	90.5	84.0	85.4	75.1	78.9	3	180	-4.5	8/17/82
1	58	2 1 1 1	5 59	92.9	86.1	86.7	76.2	80.9	3	180	-4.5	8/17/82
1	59	2 1 1 1	5 61	88.2	82.2	82.7	72.5	77.4	3	180	-4.5	8/17/82
1	60	2 0 0 1	5 32	92.7	87.7	87.2	77.6	81.9	3	180	-4.5	8/17/82
1	61	2 1 1 1	5 60	87.2	81.4	82.5	72.8	77.0	3	180	-4.5	8/17/82
1	62	2 0 0 1	1 54	81.2	75.0	74.6	62.9	69.7	3	180	-4.5	8/17/82
1	63	2 0 0 1	1 63	83.7	76.9	78.3	66.4	72.8	3	180	-4.5	8/17/82
1	64	2 1 1 1	5 61	91.6	84.5	85.5	73.2	79.2	3	180	-4.5	8/17/82
1	65	2 1 1 1	5 60	89.5	82.9	83.9	75.9	78.9	3	180	-4.5	8/17/82
1	66	2 1 1 1	5 62	94.0	87.2	88.2	76.8	80.5	3	180	-4.5	8/17/82
1	67	2 1 1 1	5 55	91.8	85.3	86.1	75.0	79.1	3	180	-4.5	8/17/82
1	68	2 1 1 1	5 54	89.2	83.0	83.5	71.9	78.0	3	180	-4.5	8/17/82
1	69	2 1 1 1	5 62	92.5	86.2	87.2	77.0	81.3	3	180	-4.5	8/17/82
1	70	1 1 1 1	5 56	88.4	81.5	82.3	72.0	76.1	3	180	-4.5	8/17/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	VE	DATE					
SITE	QUAL.	TYPE	SPEED	IP	ING	IC						
E	GVDEN	PE	(1)	NE	DL	NT						
T	RHLV	E	(2)	DE	E	DO						
		D	(3)	D		R						
			(4)									
			(5)									
			DBA									
1	71	2 0 0 1	1 54	78.9	74.2	76.0	66.3	73.5	3	180	-4.5	8/17/82
1	72	2 1 1 1	5 60	92.6	85.9	86.4	76.6	79.8	3	180	-4.5	8/17/82
1	73	2 1 1 1	1 57	82.2	76.5	76.5	62.7	72.7	3	180	-4.5	8/17/82
1	74	2 1 1 1	2 60	91.0	83.3	83.9	71.0	77.2	3	180	-4.5	8/17/82
1	75	0 0 0 1	1 50	79.1	74.3	75.7	64.8	71.8	3	180	-4.5	8/17/82
1	76	2 1 1 1	5 62	90.8	84.3	85.3	76.7	79.5	3	180	-4.5	8/17/82
1	77	2 1 1 1	5 55	92.4	84.9	85.2	77.0	80.8	3	180	-4.5	8/17/82
1	78	2 1 1 1	5 64	90.4	84.2	85.1	75.4	79.0	3	180	-4.5	8/17/82
1	79	2 1 1 1	5 54	90.3	84.3	84.9	72.9	78.0	3	180	-4.5	8/17/82
1	80	2 1 1 1	5 58	90.3	83.5	84.0	73.5	78.4	3	180	-4.5	8/17/82
1	81	2 1 1 1	5 62	90.1	83.6	84.4	73.3	78.0	3	180	-4.5	8/17/82
1	82	2 1 1 1	5 61	90.4	84.4	84.7	73.7	79.6	3	180	-4.5	8/17/82
1	83	2 1 1 1	5 63	90.5	84.9	86.0	73.1	79.0	3	180	-4.5	8/17/82
1	84	2 1 1 1	5 56	94.0	87.4	87.5	76.4	80.9	3	180	-4.5	8/17/82
1	85	2 1 1 1	5 60	91.3	85.0	85.4	75.9	80.2	3	180	-4.5	8/17/82
1	86	2 1 1 1	5 61	89.1	82.6	83.1	71.1	77.4	3	180	-4.5	8/17/82
1	87	2 1 1 1	5 60	92.6	86.2	87.2	75.6	80.5	3	180	-4.5	8/17/82
1	88	2 1 1 1	5 54	87.1	80.0	80.8	71.7	75.1	3	180	-4.5	8/17/82
1	89	1 1 1 1	5 60	87.4	80.8	81.5	72.1	75.5	3	180	-4.5	8/17/82
1	90	2 1 1 1	1 57	75.6	69.8	69.6	58.4	64.4	3	180	-4.5	8/17/82
1	91	0 0 0 1	1 63	80.5	75.0	76.1	67.9	72.5	3	180	-4.5	8/17/82
1	92	2 1 1 1	5 56	88.4	81.9	82.7	73.2	76.3	3	180	-4.5	8/17/82
1	93	2 1 1 1	5 60	91.4	84.6	85.8	72.7	78.8	3	180	-4.5	8/17/82
1	94	2 1 1 1	5 59	89.6	83.4	83.5	74.4	78.0	3	180	-4.5	8/17/82
1	95	2 1 1 1	5 58	92.1	85.5	85.7	76.2	80.6	3	180	-4.5	8/17/82
1	96	0 1 0 1	1 56	76.9	70.8	71.4	61.2	66.0	3	180	-4.5	8/17/82
1	97	0 1 1 1	1 47	72.4	66.9	66.9	58.0	64.8	3	180	-4.5	8/17/82
1	98	2 1 1 1	5 62	93.5	87.1	88.3	79.7	83.0	3	180	-4.5	8/17/82
1	99	2 1 1 1	5 56	90.8	85.5	85.5	77.4	80.7	3	180	-4.5	8/17/82
1	100	2 1 1 1	7 57	80.9	74.9	75.1	59.7	68.3	3	180	-4.5	8/17/82
1	101	2 1 1 1	5 61	91.5	84.8	85.5	77.0	80.4	3	180	-4.5	8/17/82
1	102	2 1 1 1	1 52	86.8	79.7	79.8	66.6	75.2	3	180	-4.5	8/17/82
1	103	2 1 1 1	2 55	88.9	83.0	82.7	70.1	77.8	3	180	-4.5	8/17/82
1	104	2 1 1 1	5 59	91.8	85.5	86.1	75.6	79.1	3	180	-4.5	8/17/82
1	105	2 1 1 1	5 59	89.5	83.4	85.0	76.3	78.0	3	180	-4.5	8/17/82
1	106	2 1 1 1	5 62	92.8	86.1	87.0	77.8	81.1	3	180	-4.5	8/17/82
1	107	2 1 1 1	5 60	88.5	81.9	82.7	72.1	76.7	3	180	-4.5	8/17/82
1	108	2 1 1 1	5 60	91.3	84.2	84.9	76.1	79.8	3	180	-4.5	8/17/82
1	109	0 0 0 1	1 59	80.5	74.6	76.0	65.0	72.4	3	180	-4.5	8/17/82
1	110	0 0 0 1	1 55	78.9	73.2	73.7	62.9	71.5	3	180	-4.5	8/17/82
1	111	2 1 1 1	5 64	94.5	88.1	89.1	76.6	82.5	3	180	-4.5	8/17/82
1	112	2 1 1 1	5 66	92.1	85.4	86.1	77.7	80.1	3	180	-4.5	8/17/82
1	113	2 1 1 1	5 50	95.3	88.8	89.1	79.6	83.8	3	180	-4.5	8/17/82
1	114	2 1 1 1	2 55	82.2	76.8	77.4	66.0	70.6	3	180	-4.5	8/17/82
1	115	2 1 1 1	5 60	88.8	82.3	82.7	74.3	77.3	3	180	-4.5	8/17/82
1	116	2 1 1 1	5 55	93.4	87.1	87.9	75.9	80.4	3	180	-4.5	8/17/82
1	117	2 1 1 1	5 62	89.4	83.8	84.2	74.7	79.1	3	180	-4.5	8/17/82
1	118	2 1 1 1	5 70	92.8	86.2	86.6	75.1	80.5	3	180	-4.5	8/17/82
1	119	2 1 1 1	7 55	83.2	76.6	77.1	65.4	70.8	3	180	-4.5	8/17/82
1	120	2 1 1 1	5 65	91.1	84.6	85.8	76.6	79.8	3	180	-4.5	8/17/82
1	121	2 1 1 1	5 59	90.8	83.7	85.4	73.1	78.2	3	180	-4.5	8/17/82
1	122	2 1 1 1	5 48	84.4	78.8	79.3	68.9	72.8	3	180	-4.5	8/17/82
1	123	2 1 1 1	5 57	92.9	86.0	86.8	76.8	80.4	3	180	-4.5	8/17/82
1	124	2 1 1 1	5 63	90.7	83.6	84.3	74.1	78.8	3	180	-4.5	8/17/82
1	125	2 1 1 1	1 59	79.4	72.3	71.9	60.8	66.1	3	180	-4.5	8/17/82
1	126	2 1 1 1	5 59	87.8	81.3	82.4	72.1	76.9	3	180	-4.5	8/17/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH TYPE	SPEED	MIC DBA	(1) 5	(2) 5	(3) 10	(4) 5	(5) 10	WS IP NE DE	WA IN NG DL	V WE IC NT DO	DATE
2	1	2 1 1 1	5 57	87.1	83.9	84.8	80.2	80.2	3	315	3.2	8/18/82	
2	2	2 1 1 1	5 59	90.5	83.7	84.9	77.7	77.4	3	315	3.2	8/18/82	
2	3	2 1 1 1	1 61	79.0	74.4	73.9	66.8	68.1	3	315	3.2	8/18/82	
2	4	2 1 1 1	5 59	90.1	84.4	84.2	77.1	77.5	3	315	3.2	8/18/82	
2	5	2 1 1 1	5 62	90.2	84.3	85.0	77.4	77.4	3	315	3.2	8/18/82	
2	6	2 1 1 1	2 59	89.9	83.4	84.5	76.7	77.7	3	315	3.2	8/18/82	
2	7	2 1 1 1	5 58	90.0	84.2	85.1	77.3	78.0	3	315	3.2	8/18/82	
2	8	2 1 1 1	2 58	89.7	82.4	83.6	76.2	75.7	3	315	3.2	8/18/82	
2	9	2 1 1 1	5 62	93.3	86.6	86.9	79.1	79.3	3	315	3.2	8/18/82	
2	10	2 1 1 1	5 60	92.8	87.1	87.7	80.7	80.9	3	315	3.2	8/18/82	
2	11	2 1 1 1	5 58	89.2	83.4	83.4	76.1	76.9	3	315	3.2	8/18/82	
2	12	1 1 1 1	5 64	91.0	85.8	86.2	78.7	78.6	3	315	3.2	8/18/82	
2	13	2 1 1 1	5 57	89.9	84.4	84.7	77.3	78.0	3	315	3.2	8/18/82	
2	14	2 1 1 1	1 56	80.3	75.0	74.3	66.9	68.3	3	315	3.2	8/18/82	
2	15	2 1 1 1	1 54	80.9	74.8	75.1	67.6	68.8	3	315	3.2	8/18/82	
2	16	2 1 1 1	5 61	93.7	87.3	89.0	81.3	80.6	3	315	3.2	8/18/82	
2	17	2 1 1 1	5 57	87.8	82.4	83.0	76.0	75.9	3	315	3.2	8/18/82	
2	18	2 1 1 1	5 61	90.4	85.1	85.2	78.3	78.6	3	315	3.2	8/18/82	
2	19	2 1 1 1	5 60	88.7	82.9	83.4	75.3	76.0	3	315	3.2	8/18/82	
2	20	2 1 1 1	1 57	88.2	82.2	82.5	74.2	75.3	3	315	3.2	8/18/82	
2	21	2 0 1 1	1 57	89.0	83.1	84.0	77.0	77.3	3	315	3.2	8/18/82	
2	22	2 1 1 1	5 62	91.7	86.3	86.8	78.6	79.4	3	315	3.2	8/18/82	
2	23	2 1 1 1	2 57	88.1	82.5	82.6	76.6	76.5	3	315	3.2	8/18/82	
2	24	0 0 1 1	1 62	79.6	75.7	76.2	68.0	71.2	3	315	3.2	8/18/82	
2	25	0 1 1 1	1 62	82.5	78.9	78.4	73.2	75.4	3	315	3.2	8/18/82	
2	26	1 0 1 1	5 56	85.8	81.2	81.5	74.5	74.8	3	315	3.2	8/18/82	
2	27	2 1 1 1	5 58	91.9	86.3	86.5	79.0	79.4	3	315	3.2	8/18/82	
2	28	0 0 1 1	1 60	84.5	80.4	79.8	74.4	75.3	3	315	3.2	8/18/82	
2	29	2 1 1 1	1 66	82.6	78.6	78.2	69.8	71.5	3	315	3.2	8/18/82	
2	30	2 1 1 1	2 61	94.2	87.5	88.7	82.1	82.3	3	315	3.2	8/18/82	
2	31	0 1 1 1	1 57	79.4	74.7	74.8	66.7	69.8	3	315	3.2	8/18/82	
2	32	2 1 1 1	5 63	93.4	87.6	87.2	79.3	79.7	3	315	3.2	8/18/82	
2	33	2 1 1 1	5 61	91.8	86.7	86.2	78.8	79.0	3	315	3.2	8/18/82	
2	34	0 0 1 1	1 64	82.8	80.0	80.2	77.9	78.8	3	315	3.2	8/18/82	
2	35	1 1 1 1	5 64	90.4	84.6	84.8	76.8	77.7	3	315	3.2	8/18/82	
2	36	2 1 1 1	2 56	84.6	78.2	78.8	71.0	72.1	3	315	3.2	8/18/82	
2	37	2 1 1 1	5 62	90.2	85.4	86.1	77.6	78.0	3	315	3.2	8/18/82	
2	38	2 1 1 1	2 50	85.1	80.3	80.2	74.1	75.1	3	315	3.2	8/18/82	
2	39	1 1 1 1	5 56	91.2	85.2	84.8	77.8	78.0	3	315	3.2	8/18/82	
2	40	2 1 1 1	5 57	90.1	83.9	84.3	78.1	78.0	3	315	3.2	8/18/82	
2	41	0 0 1 1	5 52	85.0	80.1	80.1	73.5	74.5	3	315	3.2	8/18/82	
2	42	1 1 1 1	1 61	82.4	77.4	76.7	70.8	72.4	3	315	3.2	8/18/82	
2	43	2 1 1 1	5 58	88.3	83.1	82.9	75.5	75.4	3	315	3.2	8/18/82	
2	44	2 1 1 1	1 64	82.2	77.3	76.9	67.7	70.2	3	315	3.2	8/18/82	
2	45	2 1 1 1	1 62	82.3	76.3	76.6	70.2	71.1	3	315	3.2	8/18/82	
2	46	2 1 1 1	5 53	89.5	83.8	84.3	76.8	77.5	3	315	3.2	8/18/82	
2	47	1 1 1 1	5 57	89.3	83.8	84.3	76.2	76.7	3	315	3.2	8/18/82	
2	48	2 1 1 1	5 57	89.9	84.3	84.9	77.9	77.3	3	315	3.2	8/18/82	
2	49	2 1 1 1	5 59	88.2	82.2	82.4	75.1	75.4	3	315	3.2	8/18/82	
2	50	2 1 1 1	1 59	81.0	75.2	74.9	66.0	68.7	3	315	3.2	8/18/82	
2	51	0 0 1 1	5 61	88.3	83.6	84.0	76.5	77.2	3	315	3.2	8/18/82	
2	52	2 1 1 1	5 63	90.4	85.1	85.1	78.4	79.2	3	315	3.2	8/18/82	
2	53	2 1 1 1	5 53	86.7	81.0	80.8	73.5	74.1	3	315	3.2	8/18/82	
2	54	1 1 1 1	5 55	89.8	83.7	85.1	77.6	77.6	3	315	3.2	8/18/82	
2	55	2 1 1 1	5 58	89.9	85.1	84.9	78.3	78.8	6	315	6.4	8/18/82	
2	56	0 0 1 1	5 62	81.5	80.7	82.0	75.2	75.6	6	315	6.4	8/18/82	
2	57	2 1 1 1	5 56	90.7	85.4	87.5	78.8	79.3	6	315	6.4	8/18/82	
2	58	2 1 1 1	5 59	89.8	83.8	83.9	76.5	76.5	6	315	6.4	8/18/82	
2	59	2 1 1 1	5 51	88.3	82.7	83.8	77.3	77.4	6	315	6.4	8/18/82	
2	60	2 1 1 1	1 62	84.7	80.5	79.5	71.4	73.3	6	315	6.4	8/18/82	
2	61	2 1 1 1	5 58	93.4	87.7	87.5	82.0	81.5	6	315	6.4	8/18/82	
2	62	2 1 1 1	5 56	88.8	83.6	84.0	79.0	78.4	6	315	6.4	8/18/82	
2	63	2 1 1 1	5 57	90.9	85.1	85.9	79.2	78.9	6	315	6.4	8/18/82	
2	64	2 1 1 1	1 70	92.0	86.5	86.9	79.1	78.7	6	315	6.4	8/18/82	
2	65	2 1 1 1	1 62	79.3	75.0	74.7	65.6	67.8	6	315	6.4	8/18/82	
2	66	2 1 1 1	1 53	78.2	73.3	73.6	65.7	68.1	6	315	6.4	8/18/82	
2	67	2 1 1 1	5 60	91.5	86.6	86.3	79.1	79.8	6	315	6.4	8/18/82	
2	68	2 1 1 1	5 61	89.6	83.6	84.2	77.0	77.8	6	315	6.4	8/18/82	
2	69	1 1 1 1	1 61	81.8	77.8	77.4	68.4	70.7	6	315	6.4	8/18/82	
2	70	2 0 1 1	5 60	86.0	81.3	81.5	75.3	76.5	6	315	6.4	8/18/82	

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	V	DATE	
	QUAL.							IP	IN	WE		
S	E	T	(1)	(2)	(3)	(4)	(5)	NE	NG	IC		
I	V	Y	5	5	10	5	10	DE	DL	NT		
T	N	E	5	5	10	5	10	DE	DL	DO		
E	R	E	DBA					D	E	R		
2	71	1 1 1 1	1 48	76.4	73.0	72.5	65.6	66.8	6	315	6.4	8/18/82
2	72	2 1 1 1	5 60	90.4	85.1	85.7	78.9	78.8	6	315	6.4	8/18/82
2	73	2 0 1 1	5 64	89.1	82.9	83.7	76.9	77.8	6	315	6.4	8/18/82
2	74	0 1 1 1	1 58	78.2	73.3	72.8	65.2	68.5	6	315	6.4	8/18/82
2	75	2 1 1 1	5 61	89.5	85.0	85.2	77.5	78.4	6	315	6.4	8/18/82
2	76	0 1 1 1	1 52	66.6	65.1	66.9	59.7	62.1	6	315	6.4	8/18/82
2	77	2 1 1 1	5 55	90.6	84.2	84.6	78.0	78.9	6	315	6.4	8/18/82
2	78	1 1 1 1	2 57	90.1	83.8	84.0	77.1	78.2	6	315	6.4	8/18/82
2	79	0 1 1 1	1 63	79.4	73.5	74.4	66.5	69.5	6	315	6.4	8/18/82
2	80	2 1 1 1	5 58	90.2	84.2	85.0	77.9	78.1	6	315	6.4	8/18/82
2	81	1 1 1 1	1 65	82.0	77.4	77.2	70.7	71.8	6	315	6.4	8/18/82
2	82	2 1 1 1	5 60	87.4	81.6	81.6	73.8	73.9	6	315	6.4	8/18/82
2	83	2 1 1 1	5 54	86.9	82.4	81.4	74.8	75.7	6	315	6.4	8/18/82
2	84	2 1 1 1	2 64	90.8	84.3	84.6	77.6	77.3	6	315	6.4	8/18/82
2	85	2 1 1 1	1 65	83.7	78.4	77.7	70.6	71.4	6	315	6.4	8/18/82
2	86	2 1 1 1	5 48	87.4	80.8	81.7	75.8	75.7	6	315	6.4	8/18/82
2	87	2 1 1 1	1 53	78.5	73.7	73.3	66.3	67.7	6	315	6.4	8/18/82
2	88	2 1 1 1	5 56	90.2	83.9	85.0	77.3	76.9	6	315	6.4	8/18/82
2	89	2 1 1 1	5 58	88.2	82.9	83.0	75.1	75.7	6	315	6.4	8/18/82
2	90	2 1 1 1	2 59	87.9	81.9	83.4	75.4	75.0	6	315	6.4	8/18/82
2	91	2 1 1 1	5 59	92.5	87.3	87.5	80.8	81.2	6	315	6.4	8/18/82
2	92	0 1 1 1	1 58	79.6	74.6	75.4	69.7	71.2	6	315	6.4	8/18/82
2	93	2 1 1 1	1 62	77.9	72.8	72.7	66.5	67.4	6	315	6.4	8/18/82
2	94	2 1 1 1	5 60	93.9	87.0	88.3	81.2	81.1	6	315	6.4	8/18/82
2	95	0 1 1 1	1 56	78.4	73.6	73.6	65.9	67.3	6	315	6.4	8/18/82
2	96	1 1 1 1	1 52	79.5	74.3	73.9	65.6	67.2	6	315	6.4	8/18/82
2	97	0 1 1 1	2 52	85.0	80.1	80.4	74.3	75.4	6	315	6.4	8/18/82
2	98	2 1 1 1	5 61	90.8	85.4	85.6	79.3	79.2	6	315	6.4	8/18/82
2	99	2 1 1 1	5 56	87.6	82.2	81.9	75.5	76.1	6	315	6.4	8/18/82
2	100	0 1 1 1	2 50	85.0	77.8	78.8	71.2	72.4	6	315	6.4	8/18/82
2	101	2 1 1 1	1 63	78.3	73.1	73.9	65.5	67.1	6	315	6.4	8/18/82
2	102	2 1 1 1	5 59	91.3	86.0	86.5	81.1	79.1	6	315	6.4	8/18/82
2	103	0 1 1 1	1 60	80.6	75.3	75.1	68.5	70.5	6	315	6.4	8/18/82
2	104	2 1 1 1	5 60	90.4	84.5	85.2	77.5	77.6	6	315	6.4	8/18/82
2	105	2 1 1 1	5 63	90.3	85.0	86.3	78.4	78.9	6	315	6.4	8/18/82
2	106	2 1 1 1	5 55	86.4	80.1	80.7	74.4	74.6	6	315	6.4	8/18/82
2	107	2 1 1 1	5 54	87.9	82.9	82.7	77.2	78.1	6	315	6.4	8/18/82
2	108	2 1 1 1	1 53	83.1	77.3	77.2	70.0	71.6	6	315	6.4	8/18/82
2	109	2 1 1 1	5 60	91.2	84.7	85.3	78.6	79.1	6	315	6.4	8/18/82
2	110	2 1 1 1	5 60	93.1	87.0	87.0	80.1	80.5	6	315	6.4	8/18/82
2	111	0 1 1 1	5 49	87.3	81.7	81.9	75.1	75.6	6	315	6.4	8/18/82
2	112	2 1 1 1	1 58	78.9	74.4	74.2	66.7	69.3	6	315	6.4	8/18/82
2	113	2 1 1 1	5 58	87.8	82.4	81.9	74.9	75.8	6	315	6.4	8/18/82
2	114	1 1 1 1	1 54	77.2	71.0	71.7	66.0	67.0	6	315	6.4	8/18/82
2	115	2 1 1 1	5 59	90.0	83.3	83.9	76.7	76.8	6	315	6.4	8/18/82
2	116	2 1 1 1	5 61	88.4	83.5	83.2	75.3	75.7	6	315	6.4	8/18/82
2	117	2 1 1 1	5 57	90.3	84.2	84.8	79.1	79.6	6	315	6.4	8/18/82
2	118	2 1 1 1	5 64	92.2	86.6	87.2	80.0	80.4	6	315	6.4	8/18/82
2	119	2 1 1 1	5 62	95.2	88.6	89.2	82.3	82.3	6	315	6.4	8/18/82
2	120	0 0 1 1	1 65	83.5	78.8	79.1	74.9	75.3	6	315	6.4	8/18/82
2	121	0 0 1 1	1 59	81.2	77.9	77.6	71.5	73.0	6	315	6.4	8/18/82
2	122	2 1 1 1	5 62	91.3	86.3	85.7	78.5	79.9	6	315	6.4	8/18/82
2	123	0 0 1 1	1 62	82.2	79.3	79.6	75.7	76.0	6	315	6.4	8/18/82
2	124	2 1 1 1	5 54	89.4	83.6	83.7	76.8	76.7	6	315	6.4	8/18/82
2	125	2 1 1 1	5 59	92.0	85.9	85.8	78.3	79.0	6	315	6.4	8/18/82
2	126	2 1 1 1	5 61	90.7	85.2	85.5	78.2	78.8	6	315	6.4	8/18/82
2	127	1 1 1 1	5 58	90.4	84.4	85.1	77.9	78.3	6	315	6.4	8/18/82
2	128	1 1 1 1	1 64	82.2	77.0	77.4	70.4	71.4	6	315	6.4	8/18/82
2	129	1 1 1 1	1 63	82.6	77.6	77.7	69.0	70.7	6	315	6.4	8/18/82
2	130	2 1 1 1	5 51	86.8	81.2	81.9	74.4	74.8	6	315	6.4	8/18/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	QUAL.	VEH	TYP	SP	MIC	(1)	(2)	(3)	(4)	(5)	WS	WA	V	DATE	
SITE	ENT	RLH	DLV	ENE	PEE	DBA	5	5	10	5	10	IP	ING	IC		
												DE	DL	DO		
3	1	2	1	1	1	5	46	88.2	81.8	82.3	0.0	0.0	3	345	4.3	9/21/82
3	2	2	1	1	1	1	51	87.3	78.7	81.2	0.0	0.0	3	345	4.3	9/21/82
3	3	0	0	0	1	0	43	90.1	83.9	84.2	0.0	0.0	3	345	4.3	9/21/82
3	4	2	1	1	1	1	48	80.7	73.6	75.3	0.0	0.0	3	345	4.3	9/21/82
3	5	2	1	1	1	1	60	80.1	73.8	74.6	0.0	0.0	0	5	0.0	9/21/82
3	6	2	1	1	1	1	85	85.7	79.7	80.4	0.0	0.0	0	5	0.0	9/21/82
3	7	2	1	1	1	5	43	87.5	81.0	81.8	0.0	0.0	0	5	0.0	9/21/82
3	8	2	1	1	1	1	50	76.9	70.0	71.7	0.0	0.0	0	5	0.0	9/21/82
3	9	2	1	1	1	1	58	77.8	70.8	72.3	0.0	0.0	0	5	0.0	9/21/82
10	10	2	1	1	1	0	54	77.3	70.8	71.9	0.0	0.0	0	5	0.0	9/21/82
3	11	2	1	1	1	1	44	77.8	69.6	71.7	0.0	0.0	0	5	0.0	9/21/82
3	12	2	1	1	1	1	48	76.2	69.3	70.1	0.0	0.0	0	5	0.0	9/21/82
3	13	2	1	1	1	1	52	-1.0	74.0	-1.0	0.0	0.0	0	5	0.0	9/21/82
3	14	2	1	1	1	1	58	77.7	72.2	72.1	0.0	0.0	0	5	0.0	9/21/82
3	15	2	1	1	1	0	47	72.8	65.3	66.8	0.0	0.0	0	5	0.0	9/21/82
3	16	2	1	1	1	0	68	81.3	74.1	75.3	0.0	0.0	0	5	0.0	9/21/82
3	17	2	1	1	1	1	65	78.9	72.2	73.5	0.0	0.0	0	5	0.0	9/21/82
3	18	2	1	1	1	1	53	78.9	72.5	74.1	0.0	0.0	0	5	0.0	9/21/82
3	19	2	1	1	1	1	54	75.9	68.9	71.0	0.0	0.0	0	5	0.0	9/21/82
3	20	2	1	1	1	0	47	74.7	67.5	69.0	0.0	0.0	0	5	0.0	9/21/82
3	21	2	1	1	1	1	52	78.0	70.5	72.3	0.0	0.0	0	5	0.0	9/21/82
3	22	2	1	1	1	1	65	87.5	77.7	81.5	0.0	0.0	0	5	0.0	9/21/82
3	23	2	1	1	1	7	38	82.3	73.5	75.3	0.0	0.0	3	5	4.5	9/21/82
3	24	2	1	1	1	1	55	84.9	77.1	78.5	0.0	0.0	3	5	4.5	9/21/82
3	25	0	0	0	1	1	53	78.4	71.2	72.9	0.0	0.0	3	5	4.5	9/21/82
3	26	2	1	1	1	1	71	80.8	72.9	74.7	0.0	0.0	3	5	4.5	9/21/82
3	27	2	1	1	1	1	52	78.5	70.8	72.3	0.0	0.0	3	5	4.5	9/21/82
3	28	2	1	1	1	5	47	90.8	84.0	85.1	0.0	0.0	3	5	4.5	9/21/82
3	29	2	1	1	1	1	61	78.3	72.4	74.7	0.0	0.0	3	5	4.5	9/21/82
3	30	2	1	1	1	0	56	75.9	68.6	69.9	0.0	0.0	3	5	4.5	9/21/82
3	31	2	1	1	1	1	61	77.2	69.7	72.0	0.0	0.0	3	5	4.5	9/21/82
3	32	2	1	1	1	5	45	89.4	83.6	83.9	0.0	0.0	3	5	4.5	9/21/82
3	33	2	1	1	1	1	46	79.6	71.1	73.4	0.0	0.0	3	5	4.5	9/21/82
3	34	2	1	1	1	1	58	80.2	72.9	75.4	0.0	0.0	3	5	4.5	9/21/82
3	35	2	1	1	1	5	43	92.3	85.5	85.5	0.0	0.0	3	5	4.5	9/21/82
3	36	2	1	1	1	0	60	77.7	70.9	72.6	0.0	0.0	3	5	4.5	9/21/82
3	37	2	1	1	1	1	57	84.9	75.2	78.3	0.0	0.0	3	5	4.5	9/21/82
3	38	2	1	1	1	2	38	77.5	70.0	72.0	0.0	0.0	3	5	4.5	9/21/82
3	39	2	1	1	1	5	45	86.9	80.1	81.7	0.0	0.0	3	5	4.5	9/21/82
3	40	2	1	1	1	0	44	74.9	67.8	69.1	0.0	0.0	3	5	4.5	9/21/82
3	41	2	1	1	1	1	52	76.8	69.0	70.2	0.0	0.0	3	5	4.5	9/21/82
3	42	2	1	1	1	1	61	77.7	71.1	72.1	0.0	0.0	3	5	4.5	9/21/82
3	43	2	1	1	1	1	64	84.3	75.4	77.8	0.0	0.0	3	5	4.5	9/21/82
3	44	0	0	0	1	2	53	81.7	73.9	75.2	0.0	0.0	3	5	4.5	9/21/82
3	45	2	1	1	1	5	53	93.4	86.2	88.4	0.0	0.0	3	5	4.5	9/21/82
3	46	2	1	1	1	1	54	80.6	73.1	74.6	0.0	0.0	3	5	4.5	9/21/82
3	47	2	0	0	1	1	43	83.5	77.6	80.0	0.0	0.0	3	5	4.5	9/21/82
3	48	2	1	1	1	5	46	-1.0	76.0	-1.0	0.0	0.0	3	5	4.5	9/21/82
3	49	2	1	1	1	5	47	90.7	84.9	84.2	0.0	0.0	3	5	4.5	9/21/82
3	50	2	1	1	1	1	66	82.4	75.0	76.6	0.0	0.0	3	5	4.5	9/21/82
3	51	2	1	1	1	0	50	-1.0	71.0	-1.0	0.0	0.0	3	5	4.5	9/21/82
3	52	2	1	1	1	3	44	-1.0	76.0	-1.0	0.0	0.0	3	5	4.5	9/21/82
3	53	2	1	1	1	1	51	80.3	72.9	74.4	0.0	0.0	3	5	4.5	9/21/82
3	54	2	1	1	1	5	43	88.4	80.9	82.7	0.0	0.0	3	5	4.5	9/21/82
3	55	2	1	1	1	1	62	77.8	70.9	71.9	0.0	0.0	3	5	4.5	9/21/82
3	56	2	1	1	1	1	57	76.4	69.0	70.5	0.0	0.0	3	5	4.5	9/21/82
3	57	2	1	1	1	1	64	81.5	75.0	75.8	0.0	0.0	3	5	4.5	9/21/82
3	58	2	1	1	1	1	55	78.5	70.5	72.4	0.0	0.0	3	5	4.5	9/21/82
3	59	2	1	1	1	5	42	86.5	79.3	80.4	0.0	0.0	3	5	4.5	9/21/82
3	60	2	1	1	1	5	42	88.6	82.4	82.8	0.0	0.0	3	5	4.5	9/21/82
3	61	2	1	1	1	5	44	87.9	80.7	81.8	0.0	0.0	3	10	4.4	9/21/82
3	62	2	1	1	1	0	52	80.5	73.8	75.2	0.0	0.0	3	10	4.4	9/21/82
3	63	2	1	1	1	1	65	81.2	73.4	75.3	0.0	0.0	3	10	4.4	9/21/82
3	64	2	1	1	1	0	54	78.6	71.4	72.5	0.0	0.0	3	10	4.4	9/21/82
3	65	2	1	1	1	0	58	80.0	73.4	74.0	0.0	0.0	3	10	4.4	9/21/82
3	66	2	1	1	1	0	49	76.2	68.8	70.3	0.0	0.0	3	10	4.4	9/21/82
3	67	2	1	1	1	7	44	77.4	70.8	71.2	0.0	0.0	3	10	4.4	9/21/82
3	68	2	1	1	1	1	59	79.5	71.6	73.6	0.0	0.0	3	10	4.4	9/21/82
3	69	2	1	1	1	0	54	76.1	69.6	70.6	0.0	0.0	3	10	4.4	9/21/82
3	70	2	1	1	1	1	51	80.0	72.5	74.2	0.0	0.0	3	10	4.4	9/21/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH	MIC					WS	WA	WE	DATE	
SITE	E	T	(1)	(2)	(3)	(4)	(5)	IP	IN	IC		
ENT	R	H	5	5	10	5	10	NE	NG	NT		
	L	L	DBA		DBA			DE	DL	DO		
	V	N						D	E	R		
3	71	2 1 1 1	5 47	86.0	80.3	80.3	0.0	0.0	3	10	4.4	9/21/82
3	72	2 1 1 1	0 51	75.7	68.7	70.2	0.0	0.0	3	10	4.4	9/21/82
3	73	2 1 1 1	5 45	86.3	80.2	80.5	0.0	0.0	3	10	4.4	9/21/82
3	74	2 1 1 1	1 51	78.2	69.6	71.9	0.0	0.0	3	10	4.4	9/21/82
3	75	2 1 1 1	1 50	76.1	69.6	70.6	0.0	0.0	3	10	4.4	9/21/82
3	76	1 1 1 1	5 38	86.0	78.8	80.8	0.0	0.0	3	10	4.4	9/21/82
3	77	2 1 1 1	7 61	86.5	80.0	80.4	0.0	0.0	3	10	4.4	9/21/82
3	78	2 1 1 1	3 45	83.3	76.0	76.9	0.0	0.0	3	10	4.4	9/21/82
3	79	2 1 1 1	1 50	78.7	70.9	72.1	0.0	0.0	3	10	4.4	9/21/82
3	80	2 1 1 1	1 54	77.1	70.2	72.2	0.0	0.0	3	10	4.4	9/21/82
3	81	2 1 1 1	1 63	77.8	70.1	72.3	0.0	0.0	3	10	4.4	9/21/82
3	82	0 0 0 1	1 54	80.9	72.9	75.4	0.0	0.0	3	10	4.4	9/21/82
3	83	2 1 1 1	1 55	76.0	68.6	70.8	0.0	0.0	3	10	4.4	9/21/82
3	84	2 1 1 1	2 45	79.4	71.7	74.2	0.0	0.0	3	10	4.4	9/21/82
3	85	2 1 1 1	3 47	85.5	79.1	80.2	0.0	0.0	3	10	4.4	9/21/82
3	86	2 1 1 1	5 45	86.2	79.4	80.6	0.0	0.0	6	285	2.3	9/21/82
3	87	2 1 1 1	2 48	83.7	76.7	77.1	0.0	0.0	6	285	2.3	9/21/82
3	88	2 1 1 1	0 44	73.0	65.4	66.4	0.0	0.0	6	285	2.3	9/21/82
3	89	2 1 1 1	1 58	77.9	70.5	72.4	0.0	0.0	6	285	2.3	9/21/82
3	90	2 1 1 1	0 63	78.1	71.3	73.1	0.0	0.0	6	285	2.3	9/21/82
3	91	2 1 1 1	0 59	77.7	70.1	72.0	0.0	0.0	6	285	2.3	9/21/82
3	92	2 1 1 1	1 48	76.9	68.2	71.2	0.0	0.0	6	285	2.3	9/21/82
3	93	2 1 1 1	5 56	92.5	85.7	86.5	0.0	0.0	6	285	2.3	9/21/82
3	94	2 1 1 1	1 56	81.2	73.2	75.5	0.0	0.0	6	285	2.3	9/21/82
3	95	2 1 1 1	1 52	79.2	71.2	73.2	0.0	0.0	6	285	2.3	9/21/82
3	96	2 1 1 1	0 55	75.5	68.4	70.1	0.0	0.0	6	285	2.3	9/21/82
3	97	1 1 1 1	0 55	75.2	68.4	70.4	0.0	0.0	6	285	2.3	9/21/82
3	98	1 1 1 1	0 46	76.3	69.5	71.3	0.0	0.0	6	285	2.3	9/21/82
3	99	2 1 1 1	1 45	74.9	67.4	69.6	0.0	0.0	6	285	2.3	9/21/82
3	100	2 1 1 1	5 46	89.3	83.5	83.6	0.0	0.0	6	285	2.3	9/21/82
3	101	2 1 1 1	1 58	77.8	70.7	72.5	0.0	0.0	6	285	2.3	9/21/82
3	102	2 1 1 1	1 51	81.2	75.0	76.1	0.0	0.0	6	285	2.3	9/21/82
3	103	2 1 1 1	0 48	76.2	70.0	70.4	0.0	0.0	6	285	2.3	9/21/82
3	104	2 1 1 1	5 48	89.3	83.4	83.4	0.0	0.0	6	285	2.3	9/21/82
3	105	2 1 1 1	5 45	88.6	81.4	82.4	0.0	0.0	3	310	2.9	9/21/82
3	106	2 1 1 1	1 59	78.0	70.5	72.1	0.0	0.0	3	310	2.9	9/21/82
3	107	2 1 1 1	1 65	87.3	79.7	82.1	0.0	0.0	3	310	2.9	9/21/82
3	108	2 1 1 1	5 45	89.9	82.7	83.8	0.0	0.0	6	315	6.4	9/21/82
3	109	2 1 1 1	5 44	86.9	81.0	81.9	0.0	0.0	6	315	6.4	9/21/82
3	110	2 1 1 1	1 53	76.0	68.3	70.6	0.0	0.0	6	315	6.4	9/21/82
3	111	2 1 1 1	5 43	88.5	82.1	82.5	0.0	0.0	6	315	6.4	9/21/82
3	112	2 1 1 1	5 38	86.5	79.4	80.0	0.0	0.0	6	315	6.4	9/21/82
3	113	2 1 1 1	7 61	78.6	72.7	72.9	0.0	0.0	6	315	6.4	9/21/82
3	114	2 1 1 1	5 50	84.3	77.0	78.1	0.0	0.0	6	315	6.4	9/21/82
3	115	0 0 0 1	0 55	79.6	72.5	74.4	0.0	0.0	6	315	6.4	9/21/82
3	116	2 1 1 1	0 48	74.3	68.4	69.2	0.0	0.0	6	315	6.4	9/21/82
3	117	0 0 0 1	1 59	77.2	70.0	73.9	0.0	0.0	6	315	6.4	9/21/82
3	118	2 1 1 1	1 66	78.8	70.7	72.3	0.0	0.0	6	315	6.4	9/21/82
3	119	0 0 0 1	0 34	80.3	74.7	75.9	0.0	0.0	6	315	6.4	9/21/82
3	120	2 1 1 1	1 50	77.6	70.6	72.2	0.0	0.0	6	315	6.4	9/21/82
3	121	2 1 1 1	1 33	77.2	69.9	71.4	0.0	0.0	6	315	6.4	9/21/82
3	122	2 1 1 1	1 55	76.4	68.3	71.3	0.0	0.0	6	315	6.4	9/21/82
3	123	2 1 1 1	1 55	76.9	68.7	70.8	0.0	0.0	6	315	6.4	9/21/82
3	124	2 1 1 1	3 56	91.5	84.8	85.5	0.0	0.0	6	315	6.4	9/21/82
3	125	2 1 1 1	5 45	87.0	80.4	81.0	0.0	0.0	6	315	6.4	9/21/82
3	126	2 1 1 1	1 50	82.7	74.8	77.0	0.0	0.0	3	315	3.2	9/21/82
3	127	2 1 1 1	1 52	76.8	68.9	71.5	0.0	0.0	3	315	3.2	9/21/82
3	128	2 1 1 1	0 51	73.6	66.3	68.3	0.0	0.0	3	315	3.2	9/21/82
3	129	2 0 0 1	5 42	84.4	77.7	79.1	0.0	0.0	3	315	3.2	9/21/82
3	130	2 1 1 1	1 59	78.1	71.1	72.9	0.0	0.0	3	315	3.2	9/21/82
3	131	2 0 0 1	1 46	83.5	78.9	80.2	0.0	0.0	3	315	3.2	9/21/82
3	132	2 1 1 1	1 63	83.6	75.4	76.9	0.0	0.0	3	315	3.2	9/21/82
3	133	2 1 1 1	5 52	87.6	81.0	81.6	0.0	0.0	3	315	3.2	9/21/82
3	134	2 1 1 1	1 58	83.2	75.5	78.0	0.0	0.0	3	315	3.2	9/21/82
3	135	2 1 1 1	1 49	78.4	70.5	72.9	0.0	0.0	3	315	3.2	9/21/82
3	136	2 0 0 1	1 57	78.1	69.9	72.5	0.0	0.0	3	315	3.2	9/21/82
3	137	2 1 1 1	5 57	89.9	83.9	84.0	0.0	0.0	3	315	3.2	9/21/82
3	138	1 0 0 1	1 44	75.7	67.2	69.6	0.0	0.0	3	315	3.2	9/21/82
3	139	2 1 1 1	2 40	80.9	74.0	75.8	0.0	0.0	3	315	3.2	9/21/82
3	140	2 0 0 1	1 53	81.0	73.3	75.4	0.0	0.0	3	315	3.2	9/21/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	V	DATE	
	QUAL.							IP	IN	IC		
SITE	E	T	(1)	(2)	(3)	(4)	NE	NG	NT			
	N	R	5	5	10	5	DE	DL	DO			
	T	H	DBA					D	E	R		
	R	L										
	V	L										
	D	N										
	E	V										
	N	H										
	T	L										
3	141	2 1 1 1	1 45	77.2	68.6	71.5	0.0	0.0	3	315	3.2	9/21/82
3	142	2 1 1 1	0 58	81.3	73.1	76.0	0.0	0.0	3	315	3.2	9/21/82
3	143	2 1 1 1	2 48	84.4	76.2	77.9	0.0	0.0	3	315	3.2	9/21/82
3	144	2 1 1 1	1 61	79.2	71.6	72.7	0.0	0.0	3	315	3.2	9/21/82
3	145	2 1 1 1	0 58	77.3	70.7	72.0	0.0	0.0	3	315	3.2	9/21/82
3	146	2 1 1 1	1 63	81.6	73.7	75.6	0.0	0.0	3	315	3.2	9/21/82
3	147	2 1 1 1	5 46	86.4	79.6	81.2	0.0	0.0	3	315	3.2	9/21/82
3	148	2 1 1 1	1 60	77.2	69.6	71.7	0.0	0.0	3	315	3.2	9/21/82
3	149	2 1 1 1	1 63	79.6	72.7	74.3	0.0	0.0	3	10	4.4	9/21/82
3	150	2 0 0 1	1 64	88.2	82.5	82.7	0.0	0.0	3	10	4.4	9/21/82
3	151	2 1 1 1	1 56	84.0	75.1	78.1	0.0	0.0	3	10	4.4	9/21/82
3	152	2 1 1 1	1 61	88.3	78.1	82.9	0.0	0.0	3	10	4.4	9/21/82
3	153	2 1 1 1	5 55	88.1	82.0	82.5	0.0	0.0	3	10	4.4	9/21/82
3	154	2 1 1 1	1 62	80.2	73.4	74.8	0.0	0.0	3	10	4.4	9/21/82
3	155	2 1 1 1	1 51	78.4	70.9	73.2	0.0	0.0	3	10	4.4	9/21/82
3	156	2 1 1 1	1 58	78.1	70.2	72.4	0.0	0.0	3	10	4.4	9/21/82
3	157	2 1 1 1	1 54	79.0	72.2	73.8	0.0	0.0	3	10	4.4	9/21/82
3	158	2 1 1 1	0 62	78.5	71.6	73.6	0.0	0.0	3	10	4.4	9/21/82
3	159	2 0 0 1	1 58	80.2	72.4	74.3	0.0	0.0	3	10	4.4	9/21/82
3	160	2 1 1 1	1 52	91.5	83.2	85.6	0.0	0.0	3	10	4.4	9/21/82
3	161	2 1 1 1	0 61	81.0	72.8	74.4	0.0	0.0	3	10	4.4	9/21/82
3	162	2 1 1 1	5 50	84.2	78.8	79.1	0.0	0.0	3	10	4.4	9/21/82
3	163	2 1 1 1	4 45	86.7	79.5	80.7	0.0	0.0	3	10	4.4	9/21/82
3	164	2 1 1 1	0 43	73.3	65.2	67.1	0.0	0.0	3	10	4.4	9/21/82
3	165	2 1 1 1	1 62	83.0	75.9	77.6	0.0	0.0	3	10	4.4	9/21/82
3	166	2 1 1 1	0 42	72.3	66.1	66.9	0.0	0.0	3	10	4.4	9/21/82
3	167	2 1 1 1	1 58	78.1	70.7	72.3	0.0	0.0	3	10	4.4	9/21/82
3	168	2 1 1 1	1 54	79.8	71.8	73.9	0.0	0.0	3	10	4.4	9/21/82
3	169	2 1 1 1	1 61	79.1	72.2	73.3	0.0	0.0	3	10	4.4	9/21/82
3	170	2 1 1 1	5 46	87.8	81.8	82.8	0.0	0.0	3	10	4.4	9/21/82
3	171	2 1 1 1	0 42	71.0	63.3	65.3	0.0	0.0	3	10	4.4	9/21/82
3	172	2 1 1 1	1 47	74.1	67.3	69.1	0.0	0.0	3	10	4.4	9/21/82
3	173	2 1 1 1	0 53	77.1	70.8	71.5	0.0	0.0	3	10	4.4	9/21/82
3	174	2 1 1 1	1 53	77.4	69.0	71.1	0.0	0.0	3	10	4.4	9/21/82
3	175	2 1 1 1	0 55	74.1	67.1	68.7	0.0	0.0	3	10	4.4	9/21/82
3	176	2 0 0 1	1 56	77.3	71.6	73.4	0.0	0.0	3	10	4.4	9/21/82
3	177	2 1 1 1	1 46	74.7	66.9	68.5	0.0	0.0	3	10	4.4	9/21/82
3	178	2 1 1 1	5 50	86.4	79.0	81.0	0.0	0.0	3	10	4.4	9/21/82
3	179	2 1 1 1	5 43	87.3	80.6	81.6	0.0	0.0	3	10	4.4	9/21/82
3	180	2 1 1 1	5 45	90.4	83.5	84.4	0.0	0.0	3	10	4.4	9/21/82
3	181	0 0 0 1	1 55	-1.0	-1.0	-1.0	0.0	0.0	3	10	4.4	9/21/82
3	182	2 1 1 1	5 43	88.1	81.9	82.5	0.0	0.0	3	10	4.4	9/21/82
3	183	2 1 1 1	0 59	75.7	68.3	70.4	0.0	0.0	3	10	4.4	9/21/82
3	184	2 1 1 1	1 54	74.9	66.6	68.9	0.0	0.0	3	10	4.4	9/21/82
3	185	2 1 1 1	1 53	77.9	70.2	71.7	0.0	0.0	3	10	4.4	9/21/82
3	186	2 1 1 1	1 53	80.4	73.1	75.6	0.0	0.0	3	10	4.4	9/21/82
3	187	2 1 1 1	1 51	75.7	68.6	70.2	0.0	0.0	3	10	4.4	9/21/82
3	188	2 1 1 1	5 55	-1.0	91.7	-1.0	0.0	0.0	3	10	4.4	9/21/82
3	189	2 1 1 1	1 56	77.6	70.6	72.3	0.0	0.0	3	10	4.4	9/21/82
3	190	2 1 1 1	2 49	81.4	74.4	75.7	0.0	0.0	3	10	4.4	9/21/82
3	191	2 1 1 1	1 55	78.1	70.8	73.4	0.0	0.0	3	10	4.4	9/21/82
3	192	2 1 1 1	1 56	80.7	74.0	74.7	0.0	0.0	3	10	4.4	9/21/82
3	193	2 0 0 1	1 77	87.3	81.3	81.8	0.0	0.0	3	10	4.4	9/21/82
3	194	2 1 1 1	1 52	77.3	69.1	70.8	0.0	0.0	3	10	4.4	9/21/82
3	195	1 1 1 1	1 46	74.8	68.5	69.1	0.0	0.0	3	10	4.4	9/21/82
3	196	2 1 1 1	1 58	79.1	71.0	72.8	0.0	0.0	3	10	4.4	9/21/82
3	197	2 1 1 1	1 52	83.3	76.8	77.0	0.0	0.0	3	10	4.4	9/21/82
3	198	2 1 1 1	5 45	86.7	80.2	81.3	0.0	0.0	3	10	4.4	9/21/82
3	199	2 1 1 1	0 50	75.3	68.1	69.5	0.0	0.0	3	10	4.4	9/21/82
3	200	2 1 1 1	5 44	86.5	80.0	81.0	0.0	0.0	3	10	4.4	9/21/82
3	201	2 1 1 1	5 44	84.4	77.6	78.3	0.0	0.0	3	330	3.9	9/22/82
3	202	1 1 1 1	1 59	80.2	72.6	74.2	0.0	0.0	3	330	3.9	9/22/82
3	203	2 1 1 1	0 64	80.8	73.0	74.1	0.0	0.0	3	330	3.9	9/22/82
3	204	1 1 1 1	0 48	77.6	70.7	71.6	0.0	0.0	3	330	3.9	9/22/82
3	205	2 1 1 1	1 45	75.3	67.8	69.1	0.0	0.0	3	330	3.9	9/22/82
3	206	2 1 1 1	2 51	87.5	79.5	80.8	0.0	0.0	3	330	3.9	9/22/82
3	207	2 1 1 1	0 56	77.3	69.8	71.9	0.0	0.0	0	0	0.0	9/22/82
3	208	2 1 1 1	1 55	79.9	73.0	74.6	0.0	0.0	0	0	0.0	9/22/82
3	209	2 1 1 1	1 53	79.8	72.1	74.1	0.0	0.0	0	330	0.0	9/22/82
3	210	2 1 1 1	1 56	78.7	71.6	72.9	0.0	0.0	0	330	0.0	9/22/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	* EVENT * * QUAL. *	* VEH * * T S * * Y P * * E D *	* MIC * (1) (2) (3) (4) (5) 5 5 10 5 10	* WS * * IP * * NE * * DE *	* WA * * IN * * NG * * DL *	* V * * WE * * IC * * NT * * DO * * R *	DATE					
3	211	2 1 1 1	1 59	79.5	72.4	73.9	0.0	0.0	0	330	0.0	9/22/82
3	212	2 1 1 1	1 64	80.5	73.4	75.1	0.0	0.0	0	0	0.0	9/22/82
3	213	2 1 1 1	0 60	80.0	72.7	73.9	0.0	0.0	0	0	0.0	9/22/82
3	214	2 1 1 1	0 46	73.1	65.9	67.6	0.0	0.0	0	0	0.0	9/22/82
3	215	2 1 1 1	1 50	80.3	72.1	74.3	0.0	0.0	0	0	0.0	9/22/82
3	216	2 1 1 1	1 54	77.0	68.9	70.5	0.0	0.0	0	0	0.0	9/22/82
3	217	2 1 1 1	0 56	76.6	69.2	70.5	0.0	0.0	0	0	0.0	9/22/82
3	218	2 1 1 1	0 59	77.0	70.8	71.9	0.0	0.0	0	0	0.0	9/22/82
3	219	2 1 1 1	0 55	77.8	70.1	72.0	0.0	0.0	0	0	0.0	9/22/82
3	220	2 1 1 1	1 70	81.5	74.3	75.6	0.0	0.0	0	0	0.0	9/22/82
3	221	2 1 1 1	0 51	80.2	71.7	73.9	0.0	0.0	0	0	0.0	9/22/82
3	222	2 1 1 1	1 54	77.0	69.5	71.3	0.0	0.0	0	0	0.0	9/22/82
3	223	2 1 1 1	0 62	78.2	71.5	73.2	0.0	0.0	0	0	0.0	9/22/82
3	224	2 1 1 1	1 45	77.5	69.6	71.5	0.0	0.0	0	0	0.0	9/22/82
3	225	2 1 1 1	5 48	90.0	83.3	83.8	0.0	0.0	0	320	0.0	9/22/82
3	226	2 1 1 1	1 50	77.8	69.1	71.6	0.0	0.0	0	320	0.0	9/22/82
3	227	2 1 1 1	0 65	82.1	74.0	76.5	0.0	0.0	0	320	0.0	9/22/82
3	228	2 1 1 1	0 47	78.4	72.7	73.5	0.0	0.0	0	320	0.0	9/22/82
3	229	2 1 1 1	5 54	87.6	81.4	82.1	0.0	0.0	0	320	0.0	9/22/82
3	230	0 0 0 1	0 59	83.0	75.7	78.5	0.0	0.0	0	320	0.0	9/22/82
3	231	2 1 1 1	1 59	78.2	70.8	72.3	0.0	0.0	0	320	0.0	9/22/82
3	232	2 1 1 1	1 51	79.8	71.6	74.5	0.0	0.0	0	320	0.0	9/22/82
3	233	2 1 1 1	5 59	96.4	89.4	91.3	0.0	0.0	0	320	0.0	9/22/82
3	234	2 1 1 1	1 53	79.6	71.7	74.1	0.0	0.0	0	320	0.0	9/22/82
3	235	2 1 1 1	3 51	91.6	84.0	84.7	0.0	0.0	0	320	0.0	9/22/82
3	236	2 1 1 1	1 56	78.6	71.0	72.8	0.0	0.0	0	320	0.0	9/22/82
3	237	2 1 1 1	5 60	93.1	86.3	86.8	0.0	0.0	0	320	0.0	9/22/82
3	238	2 1 1 1	5 54	87.4	81.1	82.8	0.0	0.0	0	320	0.0	9/22/82
3	239	2 1 1 1	0 35	69.9	63.8	64.8	0.0	0.0	0	320	0.0	9/22/82
3	240	2 1 1 1	1 50	81.1	73.3	75.6	0.0	0.0	0	320	0.0	9/22/82
3	241	0 0 1 0	1 50	73.0	67.5	69.9	0.0	0.0	0	320	0.0	9/22/82
3	242	2 1 1 1	1 49	79.5	70.6	73.6	0.0	0.0	0	320	0.0	9/22/82
3	243	0 0 0 1	2 47	82.5	74.4	75.9	0.0	0.0	0	320	0.0	9/22/82
3	244	2 1 1 1	5 55	93.2	85.1	88.2	0.0	0.0	0	320	0.0	9/22/82
3	245	2 1 1 1	1 58	76.7	69.0	71.2	0.0	0.0	0	320	0.0	9/22/82
3	246	2 1 1 1	0 52	77.3	70.6	71.7	0.0	0.0	0	320	0.0	9/22/82
3	247	2 1 1 1	1 39	75.4	67.9	69.4	0.0	0.0	0	320	0.0	9/22/82
3	248	2 1 1 1	1 52	77.1	70.0	71.2	0.0	0.0	0	320	0.0	9/22/82
3	249	2 1 1 1	0 56	77.3	69.6	71.4	0.0	0.0	0	320	0.0	9/22/82
3	250	2 1 1 1	1 57	80.3	72.3	74.0	0.0	0.0	3	310	2.9	9/22/82
3	251	2 1 1 1	7 51	80.6	73.7	74.2	0.0	0.0	3	310	2.9	9/22/82
3	252	2 1 1 1	0 51	76.6	70.1	70.8	0.0	0.0	3	310	2.9	9/22/82
3	253	2 1 1 1	1 49	77.6	71.6	72.3	0.0	0.0	3	310	2.9	9/22/82
3	254	2 1 1 1	1 54	78.4	70.0	73.0	0.0	0.0	3	310	2.9	9/22/82
3	255	2 1 1 1	1 55	76.8	70.1	71.2	0.0	0.0	3	310	2.9	9/22/82
3	256	2 1 1 1	5 45	84.0	76.8	77.8	0.0	0.0	3	310	2.9	9/22/82
3	257	2 1 1 1	1 58	83.8	75.4	77.4	0.0	0.0	3	310	2.9	9/22/82
3	258	2 1 1 1	5 54	90.1	83.5	84.9	0.0	0.0	3	310	2.9	9/22/82
3	259	2 1 1 1	0 66	79.8	72.9	74.3	0.0	0.0	3	310	2.9	9/22/82
3	260	0 0 0 1	1 62	82.2	75.4	78.3	0.0	0.0	3	310	2.9	9/22/82
3	261	2 1 1 1	1 47	72.1	64.1	66.6	0.0	0.0	3	310	2.9	9/22/82
3	262	2 1 1 1	0 57	76.2	68.5	70.6	0.0	0.0	3	280	0.8	9/22/82
3	263	2 1 1 1	1 53	82.8	74.6	77.1	0.0	0.0	3	280	0.8	9/22/82
3	264	2 1 1 1	1 63	79.5	71.4	74.0	0.0	0.0	3	280	0.8	9/22/82
3	265	2 1 1 1	1 63	79.7	72.1	73.8	0.0	0.0	3	280	0.8	9/22/82
3	266	2 1 1 1	1 53	78.1	69.3	72.0	0.0	0.0	3	280	0.8	9/22/82
3	267	2 1 1 1	1 57	79.2	71.0	73.6	0.0	0.0	3	280	0.8	9/22/82
3	268	2 1 1 1	3 54	84.8	78.2	78.4	0.0	0.0	3	280	0.8	9/22/82
3	269	2 1 1 1	5 46	85.5	78.8	80.3	0.0	0.0	3	280	0.8	9/22/82
3	270	2 1 1 1	1 58	78.4	70.0	72.5	0.0	0.0	3	280	0.8	9/22/82
3	271	2 1 1 1	0 54	74.8	67.8	69.1	0.0	0.0	3	280	0.8	9/22/82
3	272	2 1 1 1	1 38	74.0	66.0	68.5	0.0	0.0	3	280	0.8	9/22/82
3	273	2 1 1 1	1 64	86.5	76.3	80.6	0.0	0.0	3	280	0.8	9/22/82
3	274	2 1 1 1	1 61	-1.0	70.0	-1.0	0.0	0.0	3	280	0.8	9/22/82
3	275	0 0 0 1	1 55	76.4	69.1	71.3	0.0	0.0	3	280	0.8	9/22/82
3	276	2 1 1 1	3 54	91.4	84.0	84.8	0.0	0.0	3	280	0.8	9/22/82
3	277	2 1 1 1	1 56	79.5	71.9	73.2	0.0	0.0	3	310	2.9	9/22/82
3	278	2 1 1 1	0 50	75.7	69.3	70.3	0.0	0.0	0	300	0.0	9/22/82
3	279	2 1 1 1	2 64	84.2	76.2	78.1	0.0	0.0	3	300	2.2	9/22/82
3	280	2 1 1 1	1 49	83.4	73.4	76.4	0.0	0.0	3	300	2.2	9/22/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	V	DATE					
SIT	QUAL.	TYPE	(1)	(2)	(3)	(4)	(5)	IP	IN	WE		
TE	GRHLV	PEED	5	5	10	5	10	NE	NG	IC		
					DBA			DE	DL	NT		
										DO		
										R		
3	281	2 1 1 1	1 54	81.6	73.1	74.9	0.0	0.0	3	300	2.2	9/22/82
3	282	2 1 1 1	5 53	85.9	77.9	79.6	0.0	0.0	3	300	2.2	9/22/82
3	283	2 1 1 1	5 41	86.2	79.0	80.6	0.0	0.0	3	300	2.2	9/22/82
3	284	2 1 1 1	5 43	89.4	82.7	83.4	0.0	0.0	3	280	0.8	9/22/82
3	285	2 1 1 1	1 63	-1.0	71.0	-1.0	0.0	0.0	3	280	0.8	9/22/82
3	286	2 1 1 1	2 52	81.6	73.3	75.5	0.0	0.0	3	280	0.8	9/22/82
3	287	2 1 1 1	2 45	81.5	73.7	75.4	0.0	0.0	3	280	0.8	9/22/82
3	288	2 1 1 1	0 43	71.2	63.8	65.8	0.0	0.0	3	280	0.8	9/22/82
3	289	0 0 0 1	5 45	90.4	84.1	85.3	0.0	0.0	3	280	0.8	9/22/82
3	290	2 1 1 1	1 44	78.0	69.9	71.7	0.0	0.0	3	280	0.8	9/22/82
3	291	2 1 1 1	1 53	78.5	70.3	72.6	0.0	0.0	3	280	0.8	9/22/82
3	292	2 1 1 1	0 46	73.0	65.3	67.3	0.0	0.0	3	280	0.8	9/22/82
3	293	2 1 1 1	5 49	89.6	82.6	83.5	0.0	0.0	3	280	0.8	9/22/82
3	294	2 1 1 1	1 55	76.4	68.3	70.7	0.0	0.0	3	280	0.8	9/22/82
3	295	2 1 1 1	0 59	76.2	69.7	71.3	0.0	0.0	3	280	0.8	9/22/82
3	296	2 1 1 1	1 63	81.7	74.2	76.8	0.0	0.0	3	280	0.8	9/22/82
3	297	1 1 1 1	5 52	85.2	79.0	79.2	0.0	0.0	3	280	0.8	9/22/82
3	298	2 1 1 1	1 55	78.3	71.5	73.4	0.0	0.0	3	280	0.8	9/22/82
3	299	2 1 1 1	1 49	76.6	69.1	70.6	0.0	0.0	3	280	0.8	9/22/82
3	300	2 1 1 1	0 54	75.7	68.4	69.7	0.0	0.0	3	280	0.8	9/22/82
3	301	2 1 1 1	1 61	78.3	70.6	72.2	0.0	0.0	3	280	0.8	9/22/82
3	302	2 1 1 1	0 64	79.7	72.4	73.9	0.0	0.0	3	280	0.8	9/22/82
3	303	2 1 1 1	0 64	80.4	73.5	74.6	0.0	0.0	3	280	0.8	9/22/82
3	304	2 1 1 1	5 53	85.8	78.6	79.0	0.0	0.0	3	280	0.8	9/22/82
3	305	2 1 1 1	1 55	76.0	69.0	70.7	0.0	0.0	3	280	0.8	9/22/82
3	306	2 1 1 1	1 52	80.1	73.3	74.5	0.0	0.0	3	280	0.8	9/22/82
3	307	2 1 1 1	1 60	82.3	74.1	76.7	0.0	0.0	3	280	0.8	9/22/82
3	308	0 0 0 1	0 41	93.5	87.3	87.4	0.0	0.0	3	280	0.8	9/22/82
3	309	2 1 1 1	0 59	78.8	71.8	72.6	0.0	0.0	3	280	0.8	9/22/82
3	310	2 1 1 1	5 51	87.5	81.1	82.0	0.0	0.0	3	300	2.2	9/22/82
3	311	2 1 1 1	1 44	74.4	67.4	69.2	0.0	0.0	3	300	2.2	9/22/82
3	312	2 1 1 1	1 49	79.2	72.3	73.1	0.0	0.0	3	300	2.2	9/22/82
3	313	2 1 1 1	0 63	78.1	71.6	72.6	0.0	0.0	3	300	2.2	9/22/82
3	314	2 1 1 1	1 54	80.8	73.3	75.0	0.0	0.0	3	300	2.2	9/22/82
3	315	2 1 1 1	1 54	76.0	68.1	70.5	0.0	0.0	3	300	2.2	9/22/82
3	316	2 1 1 1	5 48	89.7	83.4	83.5	0.0	0.0	3	300	2.2	9/22/82
3	317	2 1 1 1	2 49	83.3	75.0	76.6	0.0	0.0	3	300	2.2	9/22/82
3	318	2 1 1 1	3 51	86.9	80.5	81.7	0.0	0.0	3	300	2.2	9/22/82
3	319	2 1 1 1	1 49	77.6	69.1	72.1	0.0	0.0	3	300	2.2	9/22/82
3	320	2 1 1 1	2 60	84.9	76.9	79.2	0.0	0.0	3	300	2.2	9/22/82
3	321	2 1 1 1	1 60	80.9	72.6	74.2	0.0	0.0	3	300	2.2	9/22/82
3	322	2 1 1 1	1 48	78.8	71.2	73.6	0.0	0.0	3	300	2.2	9/22/82
3	323	2 1 1 1	1 64	80.3	72.5	74.6	0.0	0.0	3	300	2.2	9/22/82
3	324	2 1 1 1	7 54	78.0	72.1	72.3	0.0	0.0	3	300	2.2	9/22/82
3	325	2 1 1 1	0 59	82.2	76.7	77.0	0.0	0.0	3	300	2.2	9/22/82
3	326	2 1 1 1	0 63	77.7	70.8	72.0	0.0	0.0	3	300	2.2	9/22/82
3	327	2 1 1 1	1 67	81.7	73.8	76.5	0.0	0.0	3	300	2.2	9/22/82
3	328	2 1 1 1	1 52	78.9	70.4	72.9	0.0	0.0	3	300	2.2	9/22/82
3	329	2 1 1 1	5 52	89.0	82.3	82.9	0.0	0.0	3	300	2.2	9/22/82
3	330	2 1 1 1	1 58	88.2	79.2	82.5	0.0	0.0	3	300	2.2	9/22/82
3	331	2 1 1 1	0 56	77.2	70.4	71.2	0.0	0.0	3	300	2.2	9/22/82
3	332	2 1 1 1	1 44	82.7	75.2	77.0	0.0	0.0	3	0	4.5	9/22/82
3	333	2 1 1 1	0 55	79.7	72.0	73.3	0.0	0.0	3	0	4.5	9/22/82
3	334	2 1 1 1	1 44	76.8	69.2	70.7	0.0	0.0	3	0	4.5	9/22/82
3	335	2 1 1 1	5 52	90.1	83.4	83.8	0.0	0.0	3	0	4.5	9/22/82
3	336	2 1 1 1	3 48	89.9	82.3	83.7	0.0	0.0	3	0	4.5	9/22/82
3	337	0 0 0 1	0 55	79.3	72.9	75.6	0.0	0.0	3	0	4.5	9/22/82
3	338	2 1 1 1	1 59	79.5	73.1	74.0	0.0	0.0	3	0	4.5	9/22/82
3	339	2 1 1 1	1 53	78.1	71.1	72.2	0.0	0.0	3	0	4.5	9/22/82
3	340	2 1 1 1	0 50	78.1	71.2	71.8	0.0	0.0	3	0	4.5	9/22/82
3	341	2 1 1 1	2 50	80.9	75.8	77.6	0.0	0.0	3	0	4.5	9/22/82
3	342	2 1 1 1	7 62	-1.0	83.5	-1.0	0.0	0.0	3	0	4.5	9/22/82
3	343	2 1 1 1	0 56	77.7	70.8	72.1	0.0	0.0	3	300	2.2	9/22/82
3	344	2 1 1 1	0 53	76.3	69.0	70.4	0.0	0.0	3	300	2.2	9/22/82
3	345	2 1 1 1	5 52	86.2	79.9	81.0	0.0	0.0	3	300	2.2	9/22/82
3	346	2 1 1 1	3 47	89.8	82.5	83.3	0.0	0.0	3	300	2.2	9/22/82
3	347	2 1 1 1	1 61	84.7	76.2	78.5	0.0	0.0	3	300	2.2	9/22/82
3	348	2 1 1 1	5 44	89.6	84.3	84.4	0.0	0.0	3	300	2.2	9/22/82
3	349	2 1 1 1	3 55	91.5	84.3	85.1	0.0	0.0	3	300	2.2	9/22/82
3	350	2 1 1 1	1 51	77.7	70.0	71.9	0.0	0.0	3	300	2.2	9/22/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	* EVENT * * QUAL.	* VEH * * T * * S * * P * * E * * D *	* MIC * (1) 5	* MIC * (2) 5	* MIC * (3) 10	* MIC * (4) 5	* MIC * (5) 10	* WS * * IP * * NE * * DE * * D *	* WA * * IN * * NG * * DL * * E *	* V * * IC * * NT * * DO * * R *	DATE	
3	351	2 0 0 1	0 44	73.2	65.9	68.3	0.0	0.0	3	0	4.5	9/22/82
3	352	2 1 1 1	1 55	78.7	71.4	72.6	0.0	0.0	3	0	4.5	9/22/82
3	353	0 0 0 1	0 52	78.7	71.3	72.6	0.0	0.0	3	0	4.5	9/22/82
3	354	2 1 1 1	1 47	77.1	68.7	70.2	0.0	0.0	3	0	4.5	9/22/82
3	355	2 1 1 1	5 45	84.2	78.1	78.8	0.0	0.0	3	0	4.5	9/22/82
3	356	2 1 1 1	1 62	78.9	71.6	73.3	0.0	0.0	3	0	4.5	9/22/82
3	357	0 0 0 1	0 63	81.6	74.3	76.4	0.0	0.0	0	0	0.0	9/22/82
3	358	2 1 1 1	1 69	77.1	69.7	71.9	0.0	0.0	0	0	0.0	9/22/82
3	359	2 1 1 1	3 52	88.8	82.9	83.3	0.0	0.0	0	0	0.0	9/22/82
3	360	2 1 1 1	0 60	79.5	72.0	73.4	0.0	0.0	3	330	3.9	9/22/82
3	361	2 1 1 1	1 54	81.1	75.4	76.0	0.0	0.0	3	330	3.9	9/22/82
3	362	2 1 1 1	5 52	85.2	80.5	80.4	0.0	0.0	3	330	3.9	9/22/82
3	363	2 1 1 1	0 44	76.8	70.1	71.4	0.0	0.0	3	330	3.9	9/22/82
3	364	2 1 1 1	0 57	79.7	72.9	74.4	0.0	0.0	0	0	0.0	9/22/82
3	365	2 1 1 1	0 58	78.8	72.0	73.2	0.0	0.0	0	0	0.0	9/22/82
3	366	2 1 1 1	4 39	86.3	79.5	80.4	0.0	0.0	0	0	0.0	9/22/82
3	367	2 1 1 1	2 46	79.9	73.0	74.4	0.0	0.0	0	0	0.0	9/22/82
3	368	2 1 1 1	0 58	78.1	70.2	72.0	0.0	0.0	0	0	0.0	9/22/82
3	369	2 1 1 1	0 58	76.8	69.4	70.8	0.0	0.0	0	0	0.0	9/22/82
3	370	2 1 1 1	5 58	87.5	81.1	82.3	0.0	0.0	0	0	0.0	9/22/82
3	371	2 1 1 1	0 58	76.5	70.3	71.5	0.0	0.0	0	0	0.0	9/22/82
3	372	2 1 1 1	1 47	73.8	65.8	67.8	0.0	0.0	0	0	0.0	9/22/82
3	373	2 1 1 1	1 64	78.8	70.7	73.1	0.0	0.0	0	0	0.0	9/22/82
3	374	2 1 1 1	0 57	76.8	69.7	70.7	0.0	0.0	0	85	0.0	9/23/82
3	375	2 1 1 1	1 67	82.9	74.8	76.1	0.0	0.0	0	85	0.0	9/23/82
3	376	2 1 1 1	1 62	80.4	73.4	74.6	0.0	0.0	0	85	0.0	9/23/82
3	377	2 1 1 1	5 43	89.4	83.0	83.3	0.0	0.0	0	85	0.0	9/23/82
3	378	2 1 1 1	5 43	87.7	79.8	81.0	0.0	0.0	0	85	0.0	9/23/82
3	379	0 0 0 1	1 59	80.1	74.3	75.7	0.0	0.0	0	85	0.0	9/23/82
3	380	2 1 1 1	5 43	92.2	85.2	85.3	0.0	0.0	0	85	0.0	9/23/82
3	381	2 1 1 1	5 45	90.4	83.3	84.0	0.0	0.0	0	85	0.0	9/23/82
3	382	2 1 1 1	1 58	79.3	72.3	73.8	0.0	0.0	0	85	0.0	9/23/82
3	383	2 1 1 1	5 45	88.0	81.4	82.7	0.0	0.0	0	85	0.0	9/23/82
3	384	2 1 1 1	1 41	77.2	69.9	71.2	0.0	0.0	0	85	0.0	9/23/82
3	385	0 0 0 1	5 45	89.8	83.1	84.0	0.0	0.0	0	85	0.0	9/23/82
3	386	2 1 1 1	7 60	83.1	76.5	77.4	0.0	0.0	0	85	0.0	9/23/82
3	387	2 1 1 1	5 52	85.6	78.7	79.6	0.0	0.0	0	85	0.0	9/23/82
3	388	2 1 1 1	0 42	73.5	66.4	67.8	0.0	0.0	0	85	0.0	9/23/82
3	389	2 1 1 1	1 55	76.4	69.4	70.6	0.0	0.0	0	85	0.0	9/23/82
3	390	2 1 1 1	4 49	89.4	81.1	82.6	0.0	0.0	0	85	0.0	9/23/82
3	391	2 1 1 1	2 56	83.4	75.1	76.5	0.0	0.0	0	85	0.0	9/23/82
3	392	2 1 1 1	0 55	82.2	73.6	75.3	0.0	0.0	0	85	0.0	9/23/82
3	393	2 1 1 1	1 55	78.2	71.0	72.5	0.0	0.0	0	85	0.0	9/23/82
3	394	2 1 1 1	1 59	88.8	79.8	83.4	0.0	0.0	0	85	0.0	9/23/82
3	395	2 1 1 1	1 61	78.7	71.3	72.5	0.0	0.0	0	85	0.0	9/23/82
3	396	2 1 1 1	7 53	84.8	78.8	79.2	0.0	0.0	0	85	0.0	9/23/82
3	397	2 1 1 1	1 64	81.8	74.5	75.3	0.0	0.0	0	85	0.0	9/23/82
3	398	2 1 1 1	1 51	78.6	70.8	72.7	0.0	0.0	0	85	0.0	9/23/82
3	399	0 0 0 1	0 53	80.5	74.1	75.6	0.0	0.0	0	85	0.0	9/23/82
3	400	0 0 0 1	0 58	79.9	73.6	74.8	0.0	0.0	0	85	0.0	9/23/82
3	401	2 1 1 1	2 58	86.6	79.5	80.6	0.0	0.0	0	85	0.0	9/23/82
3	402	2 1 1 1	5 43	90.4	83.1	83.6	0.0	0.0	0	85	0.0	9/23/82
3	403	2 1 1 1	5 43	86.4	80.0	81.2	0.0	0.0	0	85	0.0	9/23/82
3	404	2 1 1 1	1 52	83.0	74.8	77.3	0.0	0.0	0	85	0.0	9/23/82
3	405	2 1 1 1	1 66	80.1	72.3	73.8	0.0	0.0	0	85	0.0	9/23/82
3	406	2 1 1 1	1 59	76.8	69.3	70.8	0.0	0.0	0	85	0.0	9/23/82
3	407	2 1 1 1	1 61	82.9	75.1	77.3	0.0	0.0	0	350	0.0	9/23/82
3	408	2 1 1 1	1 54	76.8	69.1	70.5	0.0	0.0	0	350	0.0	9/23/82
3	409	2 1 1 1	1 56	77.2	69.3	70.8	0.0	0.0	0	350	0.0	9/23/82
3	410	2 1 1 1	1 66	79.7	71.6	73.4	0.0	0.0	0	350	0.0	9/23/82
3	411	2 1 1 1	0 55	76.8	69.9	70.9	0.0	0.0	0	350	0.0	9/23/82
3	412	2 1 1 1	1 56	78.8	70.9	72.7	0.0	0.0	0	0	0.0	9/23/82
3	413	2 1 1 1	5 50	91.7	84.7	85.7	0.0	0.0	0	0	0.0	9/23/82
3	414	2 1 1 1	1 57	79.6	70.9	73.2	0.0	0.0	0	0	0.0	9/23/82
3	415	2 1 1 1	1 53	86.8	75.3	79.8	0.0	0.0	0	0	0.0	9/23/82
3	416	2 1 1 1	1 66	82.2	74.8	76.2	0.0	0.0	0	0	0.0	9/23/82
3	417	2 1 1 1	1 50	76.8	69.9	71.2	0.0	0.0	0	0	0.0	9/23/82
3	418	2 1 1 1	0 54	76.0	68.7	69.9	0.0	0.0	0	0	0.0	9/23/82
3	419	2 1 1 1	5 41	86.9	79.3	81.0	0.0	0.0	0	0	0.0	9/23/82
3	420	2 1 1 1	5 45	89.8	82.9	83.8	0.0	0.0	0	300	0.0	9/23/82



\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	V	DATE					
SIT	QUAL.	T S	(1)	(2)	(3)	(4)	(5)	IP	IN	IC	DO	R
E	LE/N	P E	5	5	10	5	10	NE	NG	NT	DL	E
	RHLV	E D	DBA					DE	DL	DO	DL	E
3	491	2 1 1 1	5 44	89.2	82.6	82.9	0.0	0.0	3	355	4.5	9/23/82
3	492	2 1 1 1	5 44	85.7	78.5	79.7	0.0	0.0	3	355	4.5	9/23/82
3	493	2 1 1 1	1 73	81.8	74.0	75.8	0.0	0.0	3	355	4.5	9/23/82
3	494	2 1 1 1	5 44	89.8	82.0	83.3	0.0	0.0	3	355	4.5	9/23/82
3	495	2 1 1 1	5 42	88.6	81.2	82.3	0.0	0.0	3	355	4.5	9/23/82
3	496	2 1 1 1	2 40	83.1	75.7	77.0	0.0	0.0	3	355	4.5	9/23/82
3	497	2 1 1 1	1 54	77.7	69.5	71.5	0.0	0.0	3	355	4.5	9/23/82
3	498	2 1 1 1	0 61	78.8	72.6	73.3	0.0	0.0	3	355	4.5	9/23/82
3	499	2 1 1 1	1 55	79.9	72.8	74.2	0.0	0.0	3	355	4.5	9/23/82
3	500	2 1 1 1	0 53	77.4	70.5	71.7	0.0	0.0	3	355	4.5	9/23/82
3	501	2 1 1 1	1 56	78.8	70.4	72.0	0.0	0.0	3	355	4.5	9/23/82
3	502	2 1 1 1	1 53	76.8	69.1	71.5	0.0	0.0	3	355	4.5	9/23/82
3	503	2 1 1 1	5 47	83.9	76.6	78.0	0.0	0.0	3	355	4.5	9/23/82
3	504	2 1 1 1	5 50	95.9	88.6	90.2	0.0	0.0	3	355	4.5	9/23/82
3	505	2 1 1 1	5 50	86.9	79.5	80.9	0.0	0.0	3	355	4.5	9/23/82
3	506	2 1 1 1	0 61	79.2	72.6	73.9	0.0	0.0	3	355	4.5	9/23/82
3	507	2 1 1 1	1 52	76.4	68.6	70.4	0.0	0.0	3	355	4.5	9/23/82
3	508	2 1 1 1	1 68	84.3	76.1	78.1	0.0	0.0	3	355	4.5	9/23/82
3	509	2 1 1 1	1 40	80.3	71.4	74.0	0.0	0.0	3	355	4.5	9/23/82
3	510	2 1 1 1	1 60	78.5	71.0	72.6	0.0	0.0	3	355	4.5	9/23/82
3	511	2 1 1 1	0 58	78.5	71.8	72.8	0.0	0.0	3	355	4.5	9/23/82
3	512	2 1 1 1	5 44	93.0	85.5	86.0	0.0	0.0	3	355	4.5	9/23/82
3	513	2 1 1 1	0 65	81.4	73.5	74.8	0.0	0.0	3	355	4.5	9/23/82
3	514	2 1 1 1	5 46	86.7	79.6	81.3	0.0	0.0	3	355	4.5	9/23/82
3	515	2 1 1 1	1 60	80.5	72.8	74.5	0.0	0.0	3	355	4.5	9/23/82
3	516	2 1 1 1	1 50	81.7	73.2	76.3	0.0	0.0	3	355	4.5	9/23/82
3	517	2 1 1 1	1 61	80.2	72.9	73.9	0.0	0.0	3	355	4.5	9/23/82
3	518	2 1 1 1	1 47	80.3	72.4	73.5	0.0	0.0	3	355	4.5	9/23/82
3	519	2 1 1 1	1 43	72.9	65.6	66.8	0.0	0.0	3	355	4.5	9/23/82
3	520	2 1 1 1	1 56	77.6	70.5	71.8	0.0	0.0	3	355	4.5	9/23/82
3	521	2 1 1 1	3 49	92.0	84.3	85.3	0.0	0.0	3	355	4.5	9/23/82
3	522	2 1 1 1	1 54	80.3	73.4	74.3	0.0	0.0	3	355	4.5	9/23/82
3	523	2 1 1 1	0 48	73.4	65.9	67.5	0.0	0.0	3	355	4.5	9/23/82
3	524	2 1 1 1	0 54	77.1	69.5	71.0	0.0	0.0	3	355	4.5	9/23/82
3	525	1 1 1 1	0 50	76.7	69.3	71.0	0.0	0.0	3	355	4.5	9/23/82
3	526	1 1 1 1	0 51	75.9	69.0	70.2	0.0	0.0	3	355	4.5	9/23/82
3	527	2 1 1 1	7 60	86.6	80.4	80.8	0.0	0.0	3	355	4.5	9/23/82
3	528	2 1 1 1	5 43	89.1	82.4	82.8	0.0	0.0	3	355	4.5	9/23/82
3	529	2 1 1 1	1 49	77.7	69.6	72.3	0.0	0.0	3	355	4.5	9/23/82
3	530	2 1 1 1	0 55	78.3	72.0	72.5	0.0	0.0	3	355	4.5	9/23/82
3	531	2 1 1 1	0 64	79.1	72.2	73.5	0.0	0.0	3	355	4.5	9/23/82
3	532	2 1 1 1	1 59	78.6	71.1	72.7	0.0	0.0	3	355	4.5	9/23/82
3	533	2 1 1 1	5 44	90.3	82.9	84.1	0.0	0.0	3	355	4.5	9/23/82
3	534	2 1 1 1	5 44	89.1	82.4	83.2	0.0	0.0	3	355	4.5	9/23/82
3	535	2 1 1 1	1 55	78.3	70.4	72.1	0.0	0.0	3	350	4.4	9/23/82
3	536	1 1 1 1	0 47	73.4	66.0	67.5	0.0	0.0	3	350	4.4	9/23/82
3	537	2 1 1 1	1 61	82.2	74.1	75.5	0.0	0.0	3	350	4.4	9/23/82
3	538	0 0 1 1	1 53	79.3	72.0	73.6	0.0	0.0	3	350	4.4	9/23/82
3	539	2 1 1 1	5 49	91.2	84.1	84.8	0.0	0.0	3	350	4.4	9/23/82
3	540	2 1 1 1	2 53	85.0	77.1	78.5	0.0	0.0	3	350	4.4	9/23/82
3	541	2 1 1 1	0 50	75.9	68.5	69.2	0.0	0.0	3	350	4.4	9/23/82
3	542	2 1 1 1	1 66	78.6	71.0	73.1	0.0	0.0	3	350	4.4	9/23/82
3	543	2 1 1 1	0 60	76.9	70.6	71.8	0.0	0.0	3	350	4.4	9/23/82
3	544	2 1 1 1	5 39	83.2	76.0	76.8	0.0	0.0	3	350	4.4	9/23/82
3	545	2 1 1 1	5 49	89.9	83.0	83.4	0.0	0.0	3	350	4.4	9/23/82
3	546	2 1 1 1	1 59	80.6	72.1	74.2	0.0	0.0	3	350	4.4	9/23/82
3	547	2 1 1 1	1 66	80.5	71.9	73.8	0.0	0.0	3	350	4.4	9/23/82
3	548	2 1 1 1	0 50	77.8	70.0	72.0	0.0	0.0	3	350	4.4	9/23/82
3	549	2 1 1 1	5 57	87.1	79.6	80.7	0.0	0.0	3	350	4.4	9/23/82
3	550	2 1 1 1	0 46	74.5	67.5	69.3	0.0	0.0	3	350	4.4	9/23/82
3	551	2 1 1 1	1 43	76.5	68.6	69.7	0.0	0.0	3	350	4.4	9/23/82
3	552	2 1 1 1	3 50	87.0	79.0	80.3	0.0	0.0	3	350	4.4	9/23/82
3	553	2 1 1 1	1 46	75.2	68.2	68.5	0.0	0.0	3	350	4.4	9/23/82
3	554	2 1 1 1	2 50	82.0	74.3	76.1	0.0	0.0	3	350	4.4	9/23/82
3	555	2 1 1 1	0 50	76.4	69.2	70.6	0.0	0.0	3	350	4.4	9/23/82
3	556	2 1 1 1	1 53	78.1	69.3	71.3	0.0	0.0	3	350	4.4	9/23/82
3	557	2 1 1 1	5 45	86.5	79.6	80.5	0.0	0.0	3	350	4.4	9/23/82
3	558	0 0 0 1	0 51	76.0	68.9	71.6	0.0	0.0	3	350	4.4	9/23/82
3	559	2 1 1 1	3 55	92.2	85.1	84.9	0.0	0.0	3	350	4.4	9/23/82
3	560	2 1 1 1	1 61	85.7	76.7	79.2	0.0	0.0	3	350	4.4	9/23/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	V		
	QUAL.							IP	IN	WE		
SITE	G V D E	T S	(1)	(2)	(3)	(4)	(5)	NE	NG	IC		
	R H L V	P E E	5	5	10	5	10	DE	DL	NT	DATE	
		D	DBA					D	E	DO	R	
3	561	2 1 1 1	0 51	77.0	68.8	70.6	0.0	0.0	3	350	4.4	9/23/82
3	562	2 1 1 1	5 39	92.0	84.1	86.0	0.0	0.0	3	350	4.4	9/23/82
3	563	2 1 1 1	1 60	78.7	70.6	72.0	0.0	0.0	3	350	4.4	9/23/82
3	564	1 1 1 1	1 57	78.1	70.8	72.3	0.0	0.0	3	350	4.4	9/23/82
3	565	2 1 1 1	0 48	73.5	66.0	67.8	0.0	0.0	3	350	4.4	9/23/82
3	566	2 1 1 1	1 41	75.0	66.9	68.1	0.0	0.0	3	350	4.4	9/23/82
3	567	1 1 1 1	1 59	79.8	72.2	73.9	0.0	0.0	3	350	4.4	9/23/82
3	568	2 1 1 1	3 51	88.9	82.1	82.7	0.0	0.0	3	350	4.4	9/23/82
3	569	2 1 1 1	3 43	90.5	81.9	84.0	0.0	0.0	3	350	4.4	9/23/82
3	570	0 0 0 1	5 41	85.1	79.1	80.9	0.0	0.0	3	350	4.4	9/23/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH	MIC	WS	WA	V	DATE					
SITE	EVEN	TYPE	DBA	IP	ING	WEIC						
T	NRHLV	PEE	(1) 5	NE	DL	NTDO						
		D	(2) 5	DE	E	R						
			(3) 10									
			(4) 5									
			(5) 10									
5	1	2 1 1 1	1 48	73.9	66.6	68.0	62.0	64.3	0	320	0.0	10/27/82
5	2	2 1 1 1	1 50	77.6	70.5	71.6	65.0	67.7	0	320	0.0	10/27/82
5	3	2 1 1 1	1 57	75.4	68.1	69.9	62.5	65.1	0	320	0.0	10/27/82
5	4	2 1 1 1	1 42	69.4	65.2	66.7	61.3	64.6	0	320	0.0	10/27/82
5	5	2 1 1 1	1 33	66.5	59.9	61.8	56.1	58.3	0	320	0.0	10/27/82
5	6	2 1 1 1	2 33	79.9	73.2	73.7	69.4	70.4	0	320	0.0	10/27/82
5	7	2 1 1 1	0 46	69.9	63.0	63.6	58.0	60.6	0	320	0.0	10/27/82
5	8	2 1 1 1	2 43	79.3	72.1	73.1	67.8	69.2	0	320	0.0	10/27/82
5	9	2 1 1 1	0 43	70.2	63.2	64.1	57.6	61.0	0	320	0.0	10/27/82
5	10	2 1 1 1	1 42	75.3	68.2	69.2	64.3	65.6	0	290	0.0	10/27/82
5	11	2 1 1 1	1 45	78.0	70.2	72.1	65.6	68.1	0	290	0.0	10/27/82
5	12	2 1 1 1	1 36	70.5	63.1	64.8	58.1	61.2	0	290	0.0	10/27/82
5	13	2 1 1 1	1 44	73.1	65.1	66.6	59.7	63.0	0	290	0.0	10/27/82
5	14	2 1 1 1	1 39	71.6	64.4	65.7	58.8	61.8	0	230	0.0	10/27/82
5	15	2 1 1 1	0 58	81.7	75.1	75.3	70.1	72.1	0	230	0.0	10/27/82
5	16	2 1 1 1	1 50	76.1	68.9	70.4	63.1	66.5	0	230	0.0	10/27/82
5	17	1 1 1 1	1 46	73.4	66.9	68.3	66.2	68.3	0	230	0.0	10/27/82
5	18	2 1 1 1	0 43	73.2	66.5	67.5	61.9	63.5	0	230	0.0	10/27/82
5	19	2 1 1 1	1 47	73.9	67.4	68.7	62.4	65.4	0	230	0.0	10/27/82
5	20	2 1 1 1	1 46	77.2	69.6	71.2	65.0	67.7	0	230	0.0	10/27/82
5	21	2 1 1 1	1 39	74.2	66.4	67.7	61.7	64.1	0	230	0.0	10/27/82
5	22	2 1 1 1	1 42	73.6	66.2	67.6	61.5	63.9	0	280	0.0	10/27/82
5	23	2 1 1 1	1 41	70.7	64.2	65.4	58.8	62.3	0	280	0.0	10/27/82
5	24	2 1 1 1	0 36	70.2	63.6	63.8	58.7	60.6	0	280	0.0	10/27/82
5	25	2 1 1 1	1 47	75.2	68.6	69.7	62.8	66.0	0	280	0.0	10/27/82
5	26	2 1 1 1	1 39	71.4	64.6	65.6	59.0	62.1	0	280	0.0	10/27/82
5	27	2 1 1 1	1 47	74.5	67.3	68.6	61.9	65.0	0	170	0.0	10/27/82
5	28	2 1 1 1	2 33	78.1	70.8	71.3	67.2	68.1	0	170	0.0	10/27/82
5	29	2 1 1 1	0 45	74.0	66.8	68.3	61.6	64.8	0	170	0.0	10/27/82
5	30	2 1 1 1	3 31	85.8	78.9	79.4	76.6	76.9	0	170	0.0	10/27/82
5	31	2 1 1 1	0 46	72.8	65.8	66.9	62.0	64.3	0	170	0.0	10/27/82
5	32	2 1 1 1	0 44	71.8	64.6	65.9	58.5	62.1	0	170	0.0	10/27/82
5	33	2 1 1 1	0 36	70.9	63.9	64.9	58.8	61.4	0	170	0.0	10/27/82
5	34	2 1 1 1	3 37	87.7	80.5	81.3	77.1	77.1	0	200	0.0	10/27/82
5	35	2 1 1 1	0 46	71.5	65.0	66.2	59.5	62.0	0	200	0.0	10/27/82
5	36	2 1 1 1	0 62	78.5	71.1	72.8	65.8	68.8	0	200	0.0	10/27/82
5	37	2 1 1 1	0 47	76.4	69.3	70.7	63.7	67.1	0	200	0.0	10/27/82
5	38	2 1 1 1	0 43	71.6	64.4	65.8	59.9	62.2	0	200	0.0	10/27/82
5	39	2 1 1 1	1 48	75.5	68.3	69.5	63.6	66.0	0	200	0.0	10/27/82
5	40	2 1 1 1	1 46	72.3	65.4	66.8	59.1	62.8	0	200	0.0	10/27/82
5	41	2 1 1 1	1 43	71.1	64.4	64.7	58.7	60.9	0	200	0.0	10/27/82
5	42	2 1 1 1	1 43	75.0	68.9	71.0	63.6	67.7	0	200	0.0	10/27/82
5	43	2 1 1 1	1 32	72.4	64.1	65.6	58.1	61.8	0	200	0.0	10/27/82
5	44	2 1 1 1	1 31	71.8	64.1	65.1	60.8	62.2	0	200	0.0	10/27/82
5	45	2 1 1 1	1 44	74.4	66.9	68.5	61.5	64.9	0	200	0.0	10/27/82
5	46	1 1 1 1	0 50	74.4	67.1	68.3	61.9	64.9	0	200	0.0	10/27/82
5	47	2 1 1 1	0 49	74.7	68.5	69.0	63.8	65.9	0	200	0.0	10/27/82
5	48	2 1 1 1	0 35	71.5	63.5	65.4	58.9	62.4	0	200	0.0	10/27/82
5	49	2 1 1 1	0 53	78.5	70.9	72.3	65.4	68.2	0	200	0.0	10/27/82
5	50	2 1 1 1	1 41	72.0	65.3	66.3	60.4	62.5	3	270	0.0	10/27/82
5	51	2 1 1 1	1 42	72.6	65.1	66.6	60.2	63.6	3	270	0.0	10/27/82
5	52	2 1 1 1	0 42	71.9	65.3	66.2	60.8	63.0	3	270	0.0	10/27/82
5	53	2 1 1 1	1 46	72.4	64.9	66.8	60.3	63.3	3	270	0.0	10/27/82
5	54	2 1 1 1	2 44	83.8	76.6	78.2	71.2	73.7	3	270	0.0	10/27/82
5	55	1 1 1 1	1 31	70.0	62.9	64.2	59.7	62.1	3	270	0.0	10/27/82
5	56	2 1 1 1	0 43	72.2	66.0	66.9	60.7	63.3	3	270	0.0	10/27/82
5	57	1 1 1 1	2 43	81.2	73.8	74.8	70.6	70.9	3	270	0.0	10/27/82
5	58	2 1 1 1	0 46	71.0	64.2	65.1	60.4	61.4	3	270	0.0	10/27/82
5	59	2 1 1 1	0 51	77.1	69.2	71.9	63.4	67.1	3	270	0.0	10/27/82
5	60	2 1 1 1	1 45	76.5	69.2	70.5	63.9	66.5	3	270	0.0	10/27/82
5	61	2 1 1 1	0 42	72.0	64.7	65.4	60.6	62.6	3	270	0.0	10/27/82
5	62	2 1 1 1	1 49	74.2	66.8	68.1	61.4	64.6	3	270	0.0	10/27/82
5	63	2 1 1 1	0 43	71.0	63.6	65.4	61.3	63.6	6	270	0.0	10/27/82
5	64	2 1 1 1	0 42	83.3	76.1	76.9	71.5	72.8	6	270	0.0	10/27/82
5	65	2 1 1 1	0 47	75.3	67.8	69.1	63.7	65.6	6	270	0.0	10/27/82
5	66	2 1 1 1	1 45	74.8	67.4	68.3	63.4	64.7	6	270	0.0	10/27/82
5	67	2 1 1 1	1 46	74.1	66.5	68.0	61.2	64.5	6	270	0.0	10/27/82
5	68	2 1 1 1	0 40	70.0	62.6	63.7	58.2	60.8	6	270	0.0	10/27/82
5	69	1 1 1 1	0 49	75.3	68.6	69.5	63.4	65.8	3	270	0.0	10/27/82
5	70	2 1 1 1	1 46	72.9	65.5	66.2	61.7	62.7	3	270	0.0	10/27/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH TYPE	MIC	WS IP NE DE	WA IN NG DL E	WE IC NT DO R	DATE
SITE	VEH TYPE	VEH TYPE	(1) (2) (3) (4) (5)	DBA	DBA	DBA	DBA
5 71	2 1 1 1	0 42	72.8 65.4 66.3 61.8 63.5	3	270	0.0	10/27/82
5 72	2 1 1 1	1 50	76.4 69.3 70.5 63.9 66.3	3	340	4.2	10/27/82
5 73	2 1 1 1	1 44	76.6 70.5 71.6 65.8 68.0	3	340	4.2	10/27/82
5 74	2 1 1 1	0 45	70.7 64.1 64.8 60.6 61.9	3	340	4.2	10/27/82
5 75	2 1 1 1	0 45	70.0 62.9 64.2 58.0 60.9	3	340	4.2	10/27/82
5 76	2 1 1 1	1 43	77.9 70.8 71.5 66.2 67.9	3	340	4.2	10/27/82
5 77	2 1 1 1	1 44	71.5 64.4 65.6 59.2 62.2	3	340	4.2	10/27/82
5 78	2 1 1 1	0 44	72.6 65.6 66.8 61.0 63.5	3	340	4.2	10/27/82
5 79	2 1 1 1	0 45	73.5 65.7 66.9 60.1 63.3	3	340	4.2	10/27/82
5 80	2 1 1 1	1 44	72.3 64.9 66.3 58.6 62.5	3	180	-4.5	10/27/82
5 81	2 1 1 1	1 43	73.3 67.0 68.1 62.0 64.8	6	180	-9.0	10/27/82
5 82	2 1 1 1	1 43	72.4 65.2 66.9 59.2 62.2	6	180	-9.0	10/27/82
5 83	2 1 1 1	1 45	72.5 64.7 66.7 59.5 62.3	6	180	-9.0	10/27/82
5 84	2 1 1 1	1 45	75.2 67.4 69.2 62.2 65.5	6	180	-9.0	10/27/82
5 85	2 1 1 1	3 29	87.2 80.9 80.7 76.7 77.3	6	180	-9.0	10/27/82
5 86	2 1 1 1	1 52	77.2 69.7 72.1 63.6 68.4	6	180	-9.0	10/27/82
5 87	2 1 1 1	1 42	72.2 65.7 67.1 58.7 63.2	6	180	-9.0	10/27/82
5 88	2 1 1 1	3 35	85.1 78.3 79.4 74.6 75.3	6	180	-9.0	10/27/82
5 89	2 1 1 1	1 41	73.3 66.1 68.2 62.2 65.5	6	180	-9.0	10/27/82
5 90	2 1 1 1	3 36	87.9 81.3 81.3 78.8 78.1	6	180	-9.0	10/27/82
5 91	2 1 1 1	0 46	81.8 74.3 75.1 68.4 71.4	6	180	-9.0	10/27/82
5 92	2 1 1 1	0 41	72.8 65.3 67.4 60.5 63.7	6	180	-9.0	10/27/82
5 93	2 1 1 1	1 44	75.3 68.8 69.0 64.4 64.8	6	180	-9.0	10/27/82
5 94	2 1 1 1	0 43	71.1 63.2 65.1 58.7 61.9	6	180	-9.0	10/27/82
5 95	2 1 1 1	0 41	73.9 67.3 68.4 61.9 65.0	6	180	-9.0	10/27/82
5 96	2 1 1 1	2 34	76.8 69.7 70.6 65.0 67.2	6	180	-9.0	10/27/82
5 97	2 1 1 1	1 37	73.5 66.0 68.0 61.1 64.1	6	180	-9.0	10/27/82
5 98	2 1 1 1	3 25	83.6 77.8 78.0 74.1 74.4	6	180	-9.0	10/27/82
5 99	2 1 1 1	0 42	71.0 64.2 65.9 59.8 63.1	6	180	-9.0	10/27/82
5 100	2 1 1 1	2 38	80.5 73.5 75.1 67.7 71.4	6	180	-9.0	10/27/82
5 101	2 1 1 1	1 44	76.0 67.5 70.3 61.8 66.4	6	180	-9.0	10/27/82
5 102	2 1 1 1	0 42	72.0 64.8 66.3 59.1 62.8	6	180	-9.0	10/27/82
5 103	2 1 1 1	3 31	97.0 91.0 90.9 88.0 87.3	6	180	-9.0	10/27/82
5 104	2 1 1 1	0 47	73.8 66.7 68.4 61.7 65.0	6	180	-9.0	10/27/82
5 105	2 1 1 1	1 41	70.8 64.5 65.7 59.5 61.6	6	180	-9.0	10/27/82
5 106	0 0 1 1	1 41	73.4 66.6 68.9 61.0 66.9	6	180	-9.0	10/27/82
5 107	2 1 1 1	1 55	75.0 67.8 70.5 62.7 66.7	6	180	-9.0	10/27/82
5 108	2 1 1 1	2 42	82.1 75.6 76.7 71.6 73.4	6	180	-9.0	10/27/82
5 109	2 1 1 1	0 34	71.5 64.2 66.0 58.2 62.8	6	180	-9.0	10/27/82
5 110	2 1 1 1	1 34	71.7 64.0 65.8 59.2 61.7	6	180	-9.0	10/27/82
5 111	2 1 1 1	0 51	76.5 68.9 71.0 63.1 66.9	6	180	-9.0	10/27/82
5 112	2 1 1 1	0 42	73.0 65.5 67.8 60.1 63.6	6	180	-9.0	10/27/82
5 113	2 1 1 1	0 56	75.2 68.1 71.1 61.9 66.4	6	180	-9.0	10/27/82
5 114	2 1 1 1	1 45	71.6 64.6 65.6 58.2 62.3	6	180	-9.0	10/27/82
5 115	2 1 1 1	1 46	73.9 65.9 68.2 59.5 63.7	6	180	-9.0	10/27/82
5 116	2 1 1 1	1 47	67.4 62.5 65.4 57.1 61.8	6	180	-9.0	10/27/82
5 117	2 1 1 1	2 40	81.6 75.1 75.3 70.3 70.7	6	180	-9.0	10/27/82
5 118	2 0 1 1	0 42	72.6 65.9 67.3 59.3 63.3	6	180	-9.0	10/27/82
5 119	2 1 1 1	1 34	73.0 65.9 66.9 60.4 63.9	6	180	-9.0	10/27/82
5 120	2 0 1 1	1 40	73.0 65.7 67.5 62.0 63.9	6	180	-9.0	10/27/82
5 121	2 1 1 1	2 45	76.2 69.6 71.3 64.8 66.7	6	180	-9.0	10/27/82
5 122	2 1 1 1	0 43	73.2 65.4 67.9 59.9 64.0	6	180	-9.0	10/27/82
5 123	2 1 1 1	1 47	73.3 64.8 67.9 59.4 63.1	6	180	-9.0	10/27/82
5 124	2 1 1 1	0 43	74.8 67.2 69.0 62.7 66.0	6	180	-9.0	10/27/82
5 125	2 1 1 1	1 41	71.8 64.2 65.8 60.2 64.0	6	180	-9.0	10/27/82
5 126	2 1 1 1	3 28	87.0 79.9 80.4 76.7 76.1	6	180	-9.0	10/27/82
5 127	2 1 1 1	0 42	68.9 61.5 63.5 55.3 59.3	6	180	-9.0	10/27/82
5 128	2 1 1 1	3 28	87.4 80.9 81.1 77.1 77.4	6	180	-9.0	10/27/82
5 129	2 1 1 1	1 42	72.4 65.6 66.8 60.5 63.1	6	180	-9.0	10/27/82
5 130	2 1 1 1	1 44	73.1 65.4 67.7 59.6 62.7	6	180	-9.0	10/27/82
5 131	2 0 1 1	1 44	73.8 65.4 68.6 60.9 65.8	6	180	-9.0	10/27/82
5 132	2 1 1 1	1 44	73.7 67.1 68.4 62.6 65.1	6	180	-9.0	10/27/82
5 133	2 1 1 1	0 41	72.5 65.4 67.2 59.5 63.5	6	180	-9.0	10/27/82
5 134	2 0 1 1	1 46	72.8 64.8 68.4 61.4 65.2	6	180	-9.0	10/27/82
5 135	2 1 1 1	2 37	84.3 78.1 78.6 74.8 74.7	6	180	-9.0	10/27/82
5 136	2 1 1 1	0 42	70.0 63.9 65.0 58.4 61.9	6	180	-9.0	10/27/82
5 137	2 1 1 1	0 47	76.9 69.8 71.5 62.9 67.7	6	180	-9.0	10/27/82
5 138	2 1 1 1	0 48	74.5 66.6 69.5 62.5 65.7	6	180	-9.0	10/27/82
5 139	2 1 1 1	2 43	79.7 72.9 73.9 69.1 69.9	6	180	-9.0	10/27/82
5 140	0 0 1 1	0 45	73.9 67.4 69.1 63.7 65.3	6	180	-9.0	10/27/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH TYPE	MIC (1)	MIC (2)	MIC (3)	MIC (4)	MIC (5)	WS	WA	V	DATE	
SITE	EVENT	GRHLV	PEE5	PEE5	DBA 10	DBA 5	DBA 10	IP	IN	WE		
								NE	NG	IC		
								DE	DL	NT		
								D	E	DO		
										R		
5	141	2 1 1 1	1 47	73.7	67.4	69.0	61.6	65.7	6	180	-9.0	10/27/82
5	142	0 0 1 1	0 43	74.3	68.4	72.1	63.2	68.0	6	180	-9.0	10/27/82
5	143	2 1 1 1	1 39	70.6	64.2	65.7	61.0	63.2	6	180	-9.0	10/27/82
5	144	0 0 1 1	1 37	72.7	65.7	70.3	62.9	66.4	6	180	-9.0	10/27/82
5	145	2 1 1 1	1 53	80.0	73.1	74.9	68.3	70.8	6	180	-9.0	10/27/82
5	146	0 0 1 1	1 43	72.2	64.0	66.1	58.7	62.2	6	180	-9.0	10/27/82
5	147	2 1 1 1	1 48	71.9	65.2	66.0	60.4	63.2	6	180	-9.0	10/27/82
5	148	2 1 1 1	0 43	74.2	67.8	69.7	66.2	67.4	6	180	-9.0	10/27/82
5	149	2 1 1 1	0 48	73.1	65.6	67.6	60.2	63.8	6	180	-9.0	10/27/82
5	150	2 1 1 1	1 44	73.5	65.9	67.8	62.0	64.9	6	180	-9.0	10/27/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	WE	V					
SITE	QUAL.	TYPE	(1)	(2)	(3)	(4)	(5)	IP	IN	IC	DATE	
EVENT	G V D E	N	(1)	(2)	(3)	(4)	(5)	NE	NG	NT		
TYPE	R H L V	P E	5	5	10	5	10	DE	DL	DO		
TYPE	R H L V	P E	5	5	10	5	10	DE	DL	DO	DATE	
6	1	1 1 1 1	1 35	70.5	63.7	65.0	0.0	0.0	0	250	0.0	10/28/82
6	2	1 1 1 1	0 29	68.8	61.9	63.9	0.0	0.0	0	250	0.0	10/28/82
6	3	1 1 1 1	0 35	67.3	60.9	61.8	0.0	0.0	0	250	0.0	10/28/82
6	4	1 1 1 1	0 38	69.6	62.6	64.5	0.0	0.0	0	250	0.0	10/28/82
6	5	1 1 1 1	1 35	69.0	61.7	64.0	0.0	0.0	0	250	0.0	10/28/82
6	6	1 1 1 1	1 42	71.8	64.6	65.8	0.0	0.0	0	250	0.0	10/28/82
6	7	2 1 1 1	1 28	76.5	68.6	69.4	0.0	0.0	0	250	0.0	10/28/82
6	8	0 0 0 1	1 16	54.9	55.4	55.8	0.0	0.0	3	270	0.0	10/28/82
6	9	0 0 1 1	1 35	69.6	63.1	64.5	0.0	0.0	3	270	0.0	10/28/82
6	10	2 1 1 1	5 20	77.6	70.6	70.9	0.0	0.0	3	270	0.0	10/28/82
6	11	1 1 1 1	1 36	71.4	64.4	65.6	0.0	0.0	3	270	0.0	10/28/82
6	12	0 0 1 1	0 36	68.0	61.6	63.0	0.0	0.0	3	270	0.0	10/28/82
6	13	2 1 1 1	0 37	68.2	61.7	62.8	0.0	0.0	6	280	1.6	10/28/82
6	14	2 1 1 1	1 36	68.8	62.9	64.3	0.0	0.0	6	280	1.6	10/28/82
6	15	0 1 1 1	0 26	62.3	56.1	57.7	0.0	0.0	6	280	1.6	10/28/82
6	16	2 1 1 1	1 33	67.8	60.7	62.1	0.0	0.0	6	280	1.6	10/28/82
6	17	0 1 1 1	1 36	69.3	61.6	63.3	0.0	0.0	6	280	1.6	10/28/82
6	18	2 1 1 1	0 41	70.6	63.9	65.3	0.0	0.0	6	280	1.6	10/28/82
6	19	2 1 1 1	1 42	73.2	65.8	67.4	0.0	0.0	6	280	1.6	10/28/82
6	20	2 1 1 1	1 42	72.4	64.9	66.6	0.0	0.0	6	280	1.6	10/28/82
6	21	1 1 1 1	1 26	64.0	56.8	58.3	0.0	0.0	6	280	1.6	10/28/82
6	22	1 1 0 1	1 37	69.0	63.0	63.8	0.0	0.0	6	280	1.6	10/28/82
6	23	2 1 1 1	2 29	77.7	70.3	71.2	0.0	0.0	6	280	1.6	10/28/82
6	24	2 1 1 1	1 31	73.5	67.9	67.5	0.0	0.0	6	280	1.6	10/28/82
6	25	0 1 1 1	0 39	72.5	65.7	67.1	0.0	0.0	6	280	1.6	10/28/82
6	26	0 1 1 1	1 33	68.9	62.5	63.7	0.0	0.0	6	280	1.6	10/28/82
6	27	1 1 1 1	0 31	67.8	61.4	62.3	0.0	0.0	6	280	1.6	10/28/82
6	28	0 1 1 1	1 30	71.2	64.9	65.8	0.0	0.0	6	280	1.6	10/28/82
6	29	1 1 1 1	1 30	69.2	61.8	63.4	0.0	0.0	6	280	1.6	10/28/82
6	30	0 1 1 1	1 32	67.2	60.7	61.2	0.0	0.0	6	270	0.0	10/28/82
6	31	1 1 1 1	0 30	70.3	65.2	66.2	0.0	0.0	6	270	0.0	10/28/82
6	32	1 1 1 1	0 28	69.6	62.8	63.6	0.0	0.0	6	270	0.0	10/28/82
6	33	1 1 1 1	1 32	69.4	61.7	63.1	0.0	0.0	6	270	0.0	10/28/82
6	34	2 1 1 1	1 35	70.1	62.3	63.5	0.0	0.0	6	270	0.0	10/28/82
6	35	1 1 1 1	1 44	72.4	65.0	67.2	0.0	0.0	6	270	0.0	10/28/82
6	36	1 1 1 1	1 40	69.7	62.7	63.9	0.0	0.0	6	270	0.0	10/28/82
6	37	2 1 1 1	1 40	76.3	69.0	67.0	0.0	0.0	6	270	0.0	10/28/82
6	38	2 1 1 1	0 30	69.1	62.8	63.1	0.0	0.0	6	270	0.0	10/28/82
6	39	2 1 1 1	2 28	75.4	68.4	69.5	0.0	0.0	6	270	0.0	10/28/82
6	40	1 1 1 1	1 36	68.4	61.0	62.8	0.0	0.0	6	270	0.0	10/28/82
6	41	1 1 1 1	1 35	66.9	60.6	61.7	0.0	0.0	6	270	0.0	10/28/82
6	42	1 1 1 1	0 37	66.6	62.6	65.3	0.0	0.0	6	270	0.0	10/28/82
6	43	0 1 1 1	1 32	70.4	62.6	64.8	0.0	0.0	6	270	0.0	10/28/82
6	44	0 0 1 1	1 21	64.3	60.5	61.6	0.0	0.0	6	270	0.0	10/28/82
6	45	1 1 1 1	1 30	67.2	59.7	61.1	0.0	0.0	6	270	0.0	10/28/82
6	46	1 1 1 1	1 26	68.3	61.4	62.6	0.0	0.0	3	270	0.0	10/28/82
6	47	0 1 1 1	0 29	68.8	61.6	63.5	0.0	0.0	3	270	0.0	10/28/82
6	48	1 1 1 1	0 32	67.0	60.7	61.7	0.0	0.0	3	270	0.0	10/28/82
6	49	2 1 1 1	1 42	75.2	68.4	69.1	0.0	0.0	3	270	0.0	10/28/82
6	50	1 1 1 1	1 44	72.6	65.0	66.7	0.0	0.0	3	270	0.0	10/28/82
6	51	0 1 1 1	1 35	68.5	61.4	63.2	0.0	0.0	3	270	0.0	10/28/82
6	52	1 1 1 1	1 35	68.0	62.1	63.0	0.0	0.0	3	270	0.0	10/28/82
6	53	0 0 1 1	1 38	71.4	65.5	67.7	0.0	0.0	3	270	0.0	10/28/82
6	54	2 1 1 1	0 30	74.3	67.4	68.3	0.0	0.0	3	270	0.0	10/28/82
6	55	1 1 1 1	0 33	67.0	60.2	61.4	0.0	0.0	3	270	0.0	10/28/82
6	56	1 1 1 1	1 37	69.5	62.9	64.1	0.0	0.0	3	270	0.0	10/28/82
6	57	2 1 1 1	0 36	68.3	63.4	63.9	0.0	0.0	3	270	0.0	10/28/82
6	58	1 1 1 1	1 32	70.8	64.1	64.6	0.0	0.0	3	270	0.0	10/28/82
6	59	1 1 1 1	1 29	69.8	63.2	64.2	0.0	0.0	3	270	0.0	10/28/82
6	60	0 1 1 1	1 38	69.3	63.1	64.2	0.0	0.0	3	270	0.0	10/28/82
6	61	0 1 1 1	1 28	65.8	59.5	60.7	0.0	0.0	3	270	0.0	10/28/82
6	62	1 1 1 1	1 30	67.7	60.3	61.4	0.0	0.0	3	270	0.0	10/28/82
6	63	1 1 1 1	1 41	72.0	65.3	66.8	0.0	0.0	3	270	0.0	10/28/82
6	64	1 1 1 1	1 38	70.9	63.1	64.7	0.0	0.0	3	270	0.0	10/28/82
6	65	1 1 1 1	0 33	67.1	61.1	62.0	0.0	0.0	3	270	0.0	10/28/82
6	66	0 1 1 1	1 31	70.2	63.2	64.6	0.0	0.0	3	270	0.0	10/28/82
6	67	2 1 1 1	2 26	70.1	62.7	63.6	0.0	0.0	3	270	0.0	10/28/82
6	68	1 1 1 1	1 41	73.2	65.7	67.2	0.0	0.0	3	270	0.0	10/28/82
6	69	1 1 1 1	0 33	67.6	60.7	61.8	0.0	0.0	3	270	0.0	10/28/82
6	70	1 1 1 1	1 37	70.3	62.8	64.9	0.0	0.0	3	270	0.0	10/28/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH TYPE	MIC	WS IP NE DE	WA IN NG DL	V WE IC NT DO	DATE					
SITE	EVENT	VEH TYPE	(1) (2) (3) (4) (5)	DBA	DBA	DBA	DATE					
6	71	0 0 1 1	0 30	66.8	61.6	63.2	0.0	0.0	3	270	0.0	10/28/82
6	72	1 1 1 1	1 29	68.0	61.6	62.1	0.0	0.0	6	250	-3.1	10/28/82
6	73	1 1 1 1	1 37	71.1	63.3	64.8	0.0	0.0	6	250	-3.1	10/28/82
6	74	2 1 1 1	0 42	72.5	64.8	66.8	0.0	0.0	6	250	-3.1	10/28/82
6	75	1 1 1 1	0 31	68.4	61.6	62.5	0.0	0.0	6	250	-3.1	10/28/82
6	76	0 1 1 1	1 27	63.6	56.3	58.0	0.0	0.0	6	250	-3.1	10/28/82
6	77	1 1 1 1	1 42	71.8	64.6	66.4	0.0	0.0	6	250	-3.1	10/28/82
6	78	2 1 1 1	0 40	70.2	62.7	64.7	0.0	0.0	6	250	-3.1	10/28/82
6	79	2 1 1 1	2 28	77.5	70.2	71.5	0.0	0.0	6	250	-3.1	10/28/82
6	80	2 1 1 1	1 33	70.0	63.2	63.9	0.0	0.0	6	250	-3.1	10/28/82
6	81	1 1 1 1	2 22	70.2	63.3	64.3	0.0	0.0	6	250	-3.1	10/28/82
6	82	0 1 1 1	1 36	68.1	61.4	63.2	0.0	0.0	6	250	-3.1	10/28/82
6	83	0 1 1 1	0 34	66.2	59.5	61.3	0.0	0.0	6	250	-3.1	10/28/82
6	84	2 1 1 1	0 39	73.8	67.5	69.0	0.0	0.0	6	250	-3.1	10/28/82
6	85	1 1 1 1	1 33	68.8	61.7	63.0	0.0	0.0	6	250	-3.1	10/28/82
6	86	1 1 1 1	0 34	68.8	61.1	63.2	0.0	0.0	6	250	-3.1	10/28/82
6	87	0 1 1 1	0 40	68.0	61.6	63.4	0.0	0.0	6	270	0.0	10/28/82
6	88	0 1 1 1	0 34	66.7	60.4	60.9	0.0	0.0	6	270	0.0	10/28/82
6	89	1 1 1 1	1 34	68.6	62.0	65.2	0.0	0.0	6	270	0.0	10/28/82
6	90	0 0 1 1	0 33	65.5	59.0	61.3	0.0	0.0	6	270	0.0	10/28/82
6	91	1 1 1 1	1 35	72.4	65.2	66.5	0.0	0.0	6	270	0.0	10/28/82
6	92	1 1 1 1	1 29	67.9	65.9	67.0	0.0	0.0	6	270	0.0	10/28/82
6	93	0 1 1 1	1 23	65.5	58.5	59.5	0.0	0.0	6	270	0.0	10/28/82
6	94	1 1 1 1	0 39	70.4	63.6	65.2	0.0	0.0	6	270	0.0	10/28/82
6	95	1 1 1 1	1 21	62.4	55.3	56.9	0.0	0.0	6	270	0.0	10/28/82
6	96	1 1 1 1	1 38	70.4	63.0	64.7	0.0	0.0	6	270	0.0	10/28/82
6	97	1 1 1 1	0 34	66.4	59.9	60.4	0.0	0.0	6	270	0.0	10/28/82
6	98	1 1 1 1	1 42	72.0	64.6	66.1	0.0	0.0	6	270	0.0	10/28/82
6	99	1 1 1 1	0 31	65.8	59.3	60.6	0.0	0.0	6	270	0.0	10/28/82
6	100	1 1 1 1	1 37	70.6	63.2	64.5	0.0	0.0	6	270	0.0	10/28/82
6	101	1 1 1 1	1 34	67.6	62.1	62.8	0.0	0.0	6	270	0.0	10/28/82
6	102	0 1 1 1	1 37	69.7	62.2	63.7	0.0	0.0	6	270	0.0	10/28/82
6	103	1 1 1 1	0 34	67.4	61.7	62.6	0.0	0.0	6	270	0.0	10/28/82
6	104	0 1 1 1	1 27	64.5	57.3	59.2	0.0	0.0	6	270	0.0	10/28/82
6	105	1 1 1 1	0 39	72.1	65.2	65.9	0.0	0.0	6	270	0.0	10/28/82
6	106	1 1 1 1	0 44	70.6	63.7	65.7	0.0	0.0	6	270	0.0	10/28/82
6	107	1 1 1 1	0 40	71.9	65.1	65.6	0.0	0.0	6	270	0.0	10/28/82
6	108	1 1 1 1	0 34	68.7	64.0	65.8	0.0	0.0	6	270	0.0	10/28/82
6	109	1 1 1 1	1 36	69.1	61.5	63.0	0.0	0.0	6	270	0.0	10/28/82
6	110	1 1 1 1	0 33	66.9	60.4	62.6	0.0	0.0	6	270	0.0	10/28/82
6	111	0 0 1 1	1 31	67.6	61.9	64.0	0.0	0.0	6	270	0.0	10/28/82
6	112	2 1 1 1	2 28	81.0	73.7	74.9	0.0	0.0	6	270	0.0	10/28/82
6	113	0 1 1 1	1 30	66.3	59.3	60.5	0.0	0.0	6	270	0.0	10/28/82
6	114	0 1 1 1	0 35	66.2	60.2	61.0	0.0	0.0	6	270	0.0	10/28/82
6	115	1 1 1 1	1 28	66.3	59.3	60.4	0.0	0.0	6	270	0.0	10/28/82
6	116	1 1 1 1	1 32	67.5	60.2	61.5	0.0	0.0	6	270	0.0	10/28/82
6	117	1 1 1 1	0 24	70.8	64.4	64.7	0.0	0.0	6	270	0.0	10/28/82
6	118	2 1 1 1	2 34	77.9	71.5	72.8	0.0	0.0	6	270	0.0	10/28/82
6	119	2 1 1 1	2 33	78.8	72.4	73.1	0.0	0.0	6	270	0.0	10/28/82
6	120	2 1 1 1	2 35	78.7	72.1	73.9	0.0	0.0	6	270	0.0	10/28/82
6	121	1 1 1 1	1 35	70.2	63.0	64.4	0.0	0.0	6	260	-1.6	10/28/82
6	122	1 1 1 1	0 24	61.1	54.9	56.0	0.0	0.0	6	270	0.0	10/28/82
6	123	1 1 1 1	0 34	72.7	65.7	66.8	0.0	0.0	6	270	0.0	10/28/82
6	124	1 1 1 1	1 39	70.8	63.6	65.4	0.0	0.0	6	270	0.0	10/28/82
6	125	1 1 1 1	1 36	69.9	62.4	64.0	0.0	0.0	6	270	0.0	10/28/82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	WE	DATE	
	QUAL.		(1)	(2)	(3)	(4)	(5)	IN	IC			
SITE	G V D E	T S	(1)	(2)	(3)	(4)	(5)	NG	NT			
	R H L V	P E	5	5	10	5	10	DL	DO			
		E D	DBA					D	E	R		
7	1	2 1 1 1	5 61	89.4	81.8	83.8	72.0	75.8	3	50	2.9	1/10/83
7	2	2 1 1 1	5 57	87.3	79.9	81.8	69.0	72.9	3	50	2.9	1/10/83
7	3	1 1 1 1	5 57	86.9	80.2	82.2	71.3	74.2	3	50	2.9	1/10/83
7	4	0 1 1 1	2 58	87.0	78.8	81.6	71.9	75.3	3	50	2.9	1/10/83
7	5	2 1 1 1	5 63	86.7	79.4	82.5	70.0	73.7	3	50	2.9	1/10/83
7	6	2 1 1 1	5 61	90.3	82.4	84.5	73.3	76.2	3	50	2.9	1/10/83
7	7	2 1 1 1	5 61	90.6	83.5	85.7	72.9	76.7	3	50	2.9	1/10/83
7	8	1 1 1 1	3 52	86.7	79.8	81.2	69.5	73.3	3	90	0.0	1/10/83
7	9	2 1 1 1	5 58	91.4	84.9	86.3	78.4	78.7	3	90	0.0	1/10/83
7	10	2 1 1 1	5 54	88.7	81.4	84.0	73.3	75.2	3	90	0.0	1/10/83
7	11	2 1 1 1	5 65	90.2	83.0	84.2	73.0	76.3	3	90	0.0	1/10/83
7	12	1 1 1 1	2 55	86.9	79.0	81.2	68.1	73.2	3	90	0.0	1/10/83
7	13	2 1 1 1	5 45	87.1	79.9	81.5	71.6	73.8	3	90	0.0	1/10/83
7	14	2 1 1 1	5 54	92.5	84.5	86.4	74.2	77.7	0	50	0.0	1/10/83
7	15	1 1 1 1	2 54	84.2	77.3	78.9	67.2	71.0	0	50	0.0	1/10/83
7	16	2 1 1 1	2 53	86.2	78.4	80.9	67.8	71.9	3	100	-0.8	1/10/83
7	17	2 1 1 1	5 55	92.9	84.5	86.6	73.2	77.0	3	100	-0.8	1/10/83
7	18	2 1 1 1	5 60	88.8	82.3	84.1	75.1	78.1	3	100	-0.8	1/10/83
7	19	2 1 1 1	2 52	88.0	79.3	82.3	69.0	73.0	3	100	-0.8	1/10/83
7	20	1 1 1 1	5 57	88.2	81.3	83.2	71.9	75.5	3	100	-0.8	1/10/83
7	21	2 1 1 1	5 56	90.7	82.1	85.1	72.9	76.3	3	100	-0.8	1/10/83
7	22	2 1 1 1	2 57	90.3	82.2	84.5	70.9	75.0	0	0	0.0	1/10/83
7	23	2 1 1 1	5 60	89.2	83.5	84.1	74.1	77.0	0	0	0.0	1/10/83
7	24	2 1 1 1	1 53	88.5	81.8	83.3	72.1	75.3	0	0	0.0	1/10/83
7	25	0 1 1 1	1 58	82.0	74.5	77.0	63.8	69.7	0	0	0.0	1/10/83
7	26	2 1 1 1	0 59	78.3	72.3	74.1	61.8	66.1	0	0	0.0	1/10/83
7	27	1 1 1 1	5 56	89.9	82.6	84.5	73.3	77.0	0	0	0.0	1/10/83
7	28	2 1 1 1	0 59	78.8	72.8	73.8	62.5	66.9	0	0	0.0	1/10/83
7	29	1 1 1 1	2 57	85.0	78.0	80.0	67.8	72.4	0	0	0.0	1/10/83
7	30	1 1 1 1	3 60	90.6	83.1	84.1	75.6	77.5	0	0	0.0	1/10/83
7	31	0 1 1 1	2 47	83.5	76.7	78.5	68.3	71.6	0	110	0.0	1/10/83
7	32	2 1 1 1	5 53	89.5	82.6	84.2	72.7	76.3	0	110	0.0	1/10/83
7	33	1 1 1 1	2 61	84.0	76.8	78.7	65.6	70.3	3	110	-1.5	1/10/83
7	34	1 1 1 1	1 56	80.4	72.9	75.5	63.5	68.3	3	110	-1.5	1/10/83
7	35	2 1 1 1	2 61	86.4	78.2	80.6	67.4	72.1	3	110	-1.5	1/10/83
7	36	2 1 1 1	5 59	91.2	84.4	85.2	77.1	78.4	3	110	-1.5	1/10/83
7	37	2 1 1 1	5 57	85.8	79.3	81.0	68.7	72.7	3	110	-1.5	1/10/83
7	38	1 1 1 1	2 53	82.5	74.5	77.1	65.0	69.1	3	110	-1.5	1/10/83
7	39	1 1 1 1	3 53	87.8	80.5	82.6	71.8	74.8	3	110	-1.5	1/10/83
7	40	2 1 1 1	3 56	89.6	80.8	83.4	70.8	74.0	3	110	-1.5	1/10/83
7	41	2 1 1 1	5 55	87.8	80.3	82.0	71.3	74.3	3	110	-1.5	1/10/83
7	42	2 1 1 1	1 64	82.5	75.4	76.7	63.1	67.9	0	0	0.0	1/10/83
7	43	2 1 1 1	5 54	88.5	81.1	83.1	72.1	75.0	0	0	0.0	1/10/83
7	44	2 1 1 1	5 53	86.1	79.2	81.1	68.9	72.5	0	0	0.0	1/10/83
7	45	2 1 1 1	1 63	80.1	74.4	75.7	66.2	69.4	0	0	0.0	1/10/83
7	46	2 1 1 1	2 56	87.8	79.4	81.9	69.5	73.0	0	0	0.0	1/10/83
7	47	2 1 1 1	5 64	89.4	83.0	84.9	74.3	76.7	0	0	0.0	1/10/83
7	48	2 1 1 1	1 53	81.9	74.8	76.9	64.9	68.9	3	90	0.0	1/10/83
7	49	2 1 1 1	2 63	85.9	79.3	80.1	69.8	73.6	3	90	0.0	1/10/83
7	50	2 1 1 1	5 56	86.3	79.3	81.1	68.8	72.7	3	90	0.0	1/10/83
7	51	2 1 1 1	3 55	86.4	79.0	80.6	69.7	72.3	3	90	0.0	1/10/83
7	52	2 1 1 1	5 57	94.3	87.1	88.1	79.4	80.9	3	90	0.0	1/10/83
7	53	2 1 1 1	5 53	86.4	78.5	81.0	67.7	71.3	3	90	0.0	1/10/83
7	54	0 1 1 1	5 46	96.2	89.9	90.9	82.4	83.8	3	90	0.0	1/10/83
7	55	2 1 1 1	5 49	94.9	88.5	89.5	82.8	82.2	3	90	0.0	1/10/83
7	56	2 1 1 1	1 62	79.8	72.6	74.4	62.3	66.2	3	90	0.0	1/10/83
7	57	1 1 1 1	0 50	78.8	74.0	75.2	63.4	68.6	3	90	0.0	1/10/83
7	58	2 1 1 1	5 54	88.5	81.1	83.4	71.8	74.5	3	90	0.0	1/10/83
7	59	1 1 1 1	1 60	80.2	74.4	75.5	69.6	71.1	3	90	0.0	1/10/83
7	60	2 1 1 1	1 61	82.4	75.5	77.8	64.6	69.0	3	90	0.0	1/10/83
7	61	2 1 1 1	2 59	85.3	78.0	79.6	67.3	71.5	3	90	0.0	1/10/83
7	62	2 1 1 1	0 63	80.6	74.5	76.8	62.7	67.6	3	90	0.0	1/10/83
7	63	2 1 1 1	5 56	92.9	85.7	87.6	77.5	78.9	3	90	0.0	1/10/83
7	64	2 1 1 1	5 57	91.8	83.8	85.7	74.5	77.3	3	90	0.0	1/10/83
7	65	2 1 1 1	2 53	84.4	77.6	79.9	67.9	71.7	3	90	0.0	1/10/83
7	66	2 1 1 1	2 66	86.6	79.6	81.4	70.1	73.3	3	90	0.0	1/10/83
7	67	2 1 1 1	3 52	87.2	79.5	81.5	69.5	72.6	3	90	0.0	1/10/83
7	68	2 1 1 1	5 54	90.1	82.9	84.7	75.2	77.1	3	90	0.0	1/10/83
7	69	2 1 1 1	5 56	89.5	82.4	84.3	72.9	76.2	3	90	0.0	1/10/83
7	70	2 1 1 1	5 58	94.5	86.4	89.5	73.5	79.5	3	90	0.0	1/10/83

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	* EVENT * * QUAL.	* VEH * * T * * S * * P * * E * * D *	* MIC * (1) (2) (3) (4) (5)	* WS * * IP * * NE * * DE *	* WA * * IN * * NG * * DL *	* V * * WE * * IC * * NT * * DO * * R *	* DATE *					
S I T E	E V E N T	G V D E N L H L V	(1) 5	(2) 5	(3) 10	(4) 5	(5) 10	DBA	WS IP NE DE	WA IN NG DL	V WE IC NT DO R	DATE
7	71	1 1 1 1	1 49	81.2	73.5	76.2	65.5	68.9	3	100	-8	1/10/83
7	72	2 1 1 1	5 46	90.9	84.6	85.4	76.4	78.5	3	100	-8	1/10/83
7	73	2 1 1 1	0 58	78.3	71.9	74.0	60.6	65.8	3	100	-8	1/10/83
7	74	2 1 1 1	5 45	88.2	80.7	82.7	71.9	74.1	3	100	-8	1/10/83
7	75	2 1 1 1	2 62	90.2	83.5	84.9	74.8	78.5	3	100	-8	1/10/83
7	76	2 1 1 1	1 61	83.5	76.9	78.5	67.3	70.9	3	100	-8	1/10/83
7	77	2 1 1 1	5 62	90.8	83.6	85.7	73.6	77.2	3	100	-8	1/10/83
7	78	2 1 1 1	5 50	89.4	81.8	83.5	73.2	75.1	3	100	-8	1/10/83
7	79	2 1 1 1	5 56	90.5	83.0	85.3	71.5	75.4	3	100	-8	1/10/83
7	80	1 1 1 1	3 44	86.7	79.2	81.5	69.9	73.8	3	100	-8	1/10/83
7	81	2 1 1 1	0 56	77.3	71.4	72.6	61.5	65.6	3	100	-8	1/10/83
7	82	2 1 1 1	5 55	87.5	81.4	82.9	72.0	75.2	3	100	-8	1/10/83
7	83	2 1 1 1	5 60	87.9	81.3	83.3	72.8	75.9	3	100	-8	1/10/83
7	84	2 1 1 1	1 55	79.6	72.6	74.1	62.4	66.2	3	100	-8	1/10/83
7	85	2 1 1 1	5 53	88.3	81.9	84.0	73.0	76.4	3	100	-8	1/10/83
7	86	2 1 1 1	5 59	90.0	82.6	84.0	72.4	75.6	3	100	-8	1/10/83
7	87	2 1 1 1	2 50	82.3	75.5	78.0	64.5	68.7	3	90	0.0	1/10/83
7	88	2 1 1 1	5 60	90.5	82.4	84.1	73.5	76.0	3	90	0.0	1/10/83
7	89	2 1 1 1	5 54	90.8	83.7	85.2	75.3	77.3	3	90	0.0	1/10/83
7	90	2 1 1 1	5 55	88.7	81.5	82.8	72.9	75.7	3	90	0.0	1/10/83
7	91	2 1 1 1	5 62	92.1	84.4	86.5	76.7	78.6	3	90	0.0	1/10/83
7	92	0 1 1 1	2 52	87.1	79.7	81.0	71.2	73.6	3	90	0.0	1/10/83
7	93	1 1 1 1	2 58	87.5	79.5	82.1	70.3	73.3	0	90	0.0	1/10/83
7	94	2 1 1 1	4 59	89.3	83.0	85.0	74.2	78.0	0	90	0.0	1/10/83
7	95	2 1 1 1	1 61	80.3	73.6	75.1	65.9	69.0	0	90	0.0	1/10/83
7	96	2 1 1 1	0 57	78.7	72.0	74.1	60.5	65.3	0	90	0.0	1/10/83
7	97	2 1 1 1	5 60	89.2	82.2	84.3	74.2	77.2	0	90	0.0	1/10/83
7	98	2 1 1 1	3 62	89.3	82.5	84.4	73.6	76.9	0	90	0.0	1/10/83
7	99	2 1 1 1	5 57	88.9	81.5	83.4	72.8	75.6	0	90	0.0	1/10/83
7	100	2 1 1 1	1 55	79.3	72.6	74.7	62.3	66.5	0	90	0.0	1/10/83
7	101	2 1 1 1	5 61	89.0	81.5	83.8	72.1	75.7	0	90	0.0	1/10/83
7	102	2 1 1 1	0 57	77.1	70.7	72.1	61.1	64.8	0	90	0.0	1/10/83
7	103	2 1 1 1	5 56	88.4	81.4	82.9	72.6	75.0	0	90	0.0	1/10/83
7	104	1 1 1 1	2 57	83.1	77.7	80.1	68.4	73.1	0	90	0.0	1/10/83
7	105	2 1 1 1	5 52	86.5	79.9	81.8	69.6	73.2	0	90	0.0	1/10/83
7	106	2 1 1 1	5 54	89.1	82.4	84.1	73.0	76.4	0	90	0.0	1/10/83
7	107	1 1 1 1	0 59	78.7	71.9	73.7	60.8	65.0	0	90	0.0	1/10/83
7	108	1 1 1 1	1 58	78.3	72.6	73.8	64.9	67.6	0	90	0.0	1/10/83
7	109	2 1 1 1	3 54	83.3	75.1	77.5	66.3	69.2	0	90	0.0	1/10/83
7	110	2 1 1 1	5 47	88.2	81.0	82.8	73.1	74.8	0	90	0.0	1/10/83
7	111	2 1 1 1	1 54	79.1	72.0	73.7	58.8	65.9	0	90	0.0	1/10/83
7	112	2 1 1 1	5 46	89.2	81.2	83.0	72.1	74.4	0	90	0.0	1/10/83
7	113	2 1 1 1	5 60	89.9	82.4	84.8	72.9	75.5	0	90	0.0	1/10/83
7	114	2 1 1 1	2 60	88.1	81.3	82.8	72.1	75.7	0	90	0.0	1/10/83
7	115	2 1 1 1	3 59	89.0	81.5	83.1	72.0	74.9	0	90	0.0	1/10/83
7	116	2 1 1 1	2 60	87.7	79.9	81.7	70.2	73.3	0	90	0.0	1/10/83
7	117	2 1 1 1	5 61	90.1	82.6	85.4	72.9	76.4	0	90	0.0	1/10/83
7	118	2 1 1 1	5 58	88.4	81.4	83.5	71.8	75.0	0	90	0.0	1/10/83
7	119	1 1 1 1	1 60	-1.0	75.0	-1.0	-1.0	-1.0	0	90	0.0	1/ 0/ 3
7	120	2 1 1 1	1 71	86.7	78.7	81.1	66.5	71.5	3	90	0.0	1/10/83
7	121	1 1 1 1	2 59	84.2	77.0	79.1	67.0	71.8	3	90	0.0	1/10/83
7	122	2 1 1 1	5 57	87.7	80.6	82.3	70.7	74.8	3	90	0.0	1/10/83
7	123	2 1 1 1	2 49	86.4	78.0	80.2	69.8	72.9	3	90	0.0	1/10/83
7	124	1 1 1 1	2 56	84.2	77.9	80.3	67.2	72.8	3	90	0.0	1/10/83
7	125	1 1 1 1	5 60	87.2	79.4	81.9	68.9	72.9	3	90	0.0	1/10/83
7	126	2 1 1 1	5 56	90.1	82.1	84.7	72.5	75.5	3	90	0.0	1/10/83
7	127	2 1 1 1	3 48	87.3	79.7	81.3	72.5	74.3	3	90	0.0	1/10/83
7	128	2 1 1 1	2 53	85.5	77.6	79.7	67.0	71.2	3	90	0.0	1/10/83
7	129	2 1 1 1	3 59	87.6	79.6	82.0	69.4	73.9	3	90	0.0	1/10/83
7	130	2 1 1 1	4 54	87.8	79.9	81.4	71.0	73.7	3	90	0.0	1/10/83
7	131	0 1 1 1	0 50	77.6	71.5	73.3	63.3	67.3	3	90	0.0	1/10/83
7	132	1 1 1 1	5 55	87.1	80.1	82.0	69.9	74.0	3	90	0.0	1/10/83
7	133	2 1 1 1	1 55	78.4	72.4	74.0	60.7	65.6	3	90	0.0	1/10/83
7	134	2 1 1 1	0 50	75.3	68.1	70.6	56.3	61.8	3	90	0.0	1/10/83
7	135	2 1 1 1	5 55	89.3	80.7	82.8	70.7	74.0	3	90	0.0	1/10/83
7	136	2 1 1 1	2 51	85.3	76.9	78.5	68.9	71.0	3	90	0.0	1/10/83
7	137	2 1 1 1	5 61	90.1	83.0	85.4	73.9	77.3	3	90	0.0	1/10/83
7	138	2 1 1 1	5 58	91.9	83.9	86.4	73.2	76.9	3	90	0.0	1/10/83
7	139	2 1 1 1	2 57	90.0	82.0	84.6	68.9	74.6	3	90	0.0	1/10/83
7	140	1 1 1 1	0 47	78.2	70.8	73.2	-1.0	-1.0	3	90	0.0	1/10/83

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

SITE	LOC.	EVENT QUAL.			VEH		MIC					WS IP NE DE	WA IN NG DL E	VE IC NT DO R	DATE	
		G	V	D	E	T	S	(1)	(2)	(3)	(4)					(5)
		L	H	N	V	P	E	5	5	10	5	10				
7	141	2	1	1	1	3	57	94.3	85.9	88.3	77.0	80.1	3	90	0.0	1/10/83
7	142	2	1	1	1	5	59	87.2	80.3	82.0	71.5	74.9	3	90	0.0	1/10/83
7	143	2	1	1	1	5	53	85.7	78.3	80.4	71.1	72.9	3	90	0.0	1/10/83
7	144	2	1	1	1	2	62	85.9	78.4	80.4	68.6	72.7	3	90	0.0	1/10/83
7	145	2	1	1	1	5	51	88.0	79.4	82.2	69.0	73.0	3	90	0.0	1/10/83
7	146	2	1	1	1	5	61	91.5	84.2	86.8	73.1	77.3	3	90	0.0	1/10/83
7	147	2	1	1	1	5	64	90.6	82.9	85.5	73.5	77.0	3	90	0.0	1/10/83
7	148	2	1	1	1	5	59	90.2	82.0	84.6	71.2	75.4	3	90	0.0	1/10/83
7	149	2	1	1	1	5	57	89.8	81.9	83.8	72.2	75.3	3	120	-2.2	1/10/83
7	150	1	1	1	1	2	60	87.2	79.9	81.7	70.8	74.6	3	120	-2.2	1/10/83
7	151	2	1	1	1	5	59	86.9	79.7	81.6	71.1	74.0	3	120	-2.2	1/10/83
7	152	2	1	1	1	3	53	89.1	81.9	82.5	72.8	76.6	3	120	-2.2	1/10/83
7	153	0	1	1	1	1	50	79.0	71.3	73.0	62.8	66.4	3	120	-2.2	1/10/83
7	154	2	1	1	1	5	55	90.2	81.8	84.7	72.2	75.3	6	110	-3.1	1/10/83
7	155	2	1	1	1	5	56	89.4	82.2	84.1	73.3	75.7	6	110	-3.1	1/10/83
7	156	2	1	1	1	5	56	87.3	79.8	82.2	71.1	73.8	6	110	-3.1	1/10/83
7	157	2	1	1	1	1	66	81.1	74.5	76.0	63.2	67.5	6	110	-3.1	1/10/83
7	158	2	1	1	1	2	56	85.4	77.4	80.1	68.3	72.4	6	110	-3.1	1/10/83
7	159	1	1	1	1	1	52	81.3	73.3	76.1	65.0	67.5	6	110	-3.1	1/10/83
7	160	2	1	1	1	3	55	91.4	85.7	85.2	77.3	79.4	6	110	-3.1	1/10/83
7	161	2	1	1	1	2	51	84.3	77.5	79.3	70.2	71.7	6	110	-3.1	1/10/83
7	162	2	1	1	1	2	61	87.5	79.3	81.3	69.3	73.3	6	110	-3.1	1/10/83
7	163	2	1	1	1	2	53	87.3	80.1	81.5	72.5	74.7	6	110	-3.1	1/10/83
7	164	1	1	1	1	0	48	77.3	70.4	71.9	62.3	64.5	6	110	-3.1	1/10/83
7	165	2	1	1	1	5	52	87.7	80.9	82.9	72.1	75.8	6	90	0.0	1/10/83
7	166	2	1	1	1	5	57	90.6	82.6	85.5	71.5	75.6	6	110	-3.1	1/10/83
7	167	2	1	1	1	2	52	84.7	76.9	79.1	67.8	70.6	6	110	-3.1	1/10/83
7	168	1	1	1	1	3	46	86.8	79.9	81.4	71.4	74.5	6	110	-3.1	1/10/83
7	169	2	1	1	1	3	41	88.9	80.0	82.9	71.9	75.2	6	110	-3.1	1/10/83
7	170	2	1	1	1	5	53	96.5	90.2	90.8	83.1	84.7	6	110	-3.1	1/10/83
7	171	1	1	1	1	3	53	85.9	78.4	80.5	70.4	72.8	6	110	-3.1	1/10/83
7	172	0	1	1	1	2	50	88.6	83.8	86.2	74.6	78.0	6	110	-3.1	1/10/83
7	173	2	1	1	1	5	56	91.5	84.2	85.8	75.4	78.7	6	110	-3.1	1/10/83
7	174	2	1	1	1	5	52	88.7	81.4	83.1	72.4	75.2	6	110	-3.1	1/10/83
7	175	2	1	1	1	5	60	93.4	86.2	87.9	77.5	79.6	6	110	-3.1	1/10/83
7	176	2	1	1	1	1	68	83.7	76.3	78.7	64.7	68.8	6	110	-3.1	1/10/83
7	177	2	1	1	1	1	63	86.6	77.8	81.3	65.1	70.4	6	110	-3.1	1/10/83
7	178	2	1	1	1	5	53	87.3	79.2	81.5	69.3	72.7	6	110	-3.1	1/10/83
7	179	2	1	1	1	2	58	83.7	76.0	79.4	64.4	68.9	6	110	-3.1	1/10/83
7	180	0	1	1	1	5	50	86.1	79.6	81.6	72.3	74.8	6	110	-3.1	1/10/83
7	181	1	1	1	1	5	59	87.7	81.5	83.3	72.4	76.5	6	110	-3.1	1/10/83
7	182	2	1	1	1	5	52	87.5	80.1	82.1	71.9	75.2	6	110	-3.1	1/10/83
7	183	1	1	1	1	5	55	87.8	80.3	82.3	71.7	74.1	6	110	-3.1	1/10/83
7	184	0	1	1	1	4	55	88.1	80.5	82.9	70.8	74.9	6	110	-3.1	1/10/83
7	185	2	1	1	1	1	54	80.4	72.4	75.3	62.7	66.2	6	110	-3.1	1/10/83
7	186	1	1	1	1	2	53	82.9	75.8	78.9	64.5	69.1	6	110	-3.1	1/10/83
7	187	2	1	1	1	2	59	86.5	78.4	81.0	69.0	72.6	6	110	-3.1	1/10/83
7	188	1	1	1	1	1	54	78.3	71.9	73.6	64.8	67.4	6	110	-3.1	1/10/83
7	189	2	1	1	1	2	53	89.8	81.0	84.7	69.0	74.2	6	110	-3.1	1/10/83
7	190	2	1	1	1	4	52	88.4	81.2	83.0	70.6	74.9	6	110	-3.1	1/10/83
7	191	1	1	1	1	2	46	80.5	72.8	75.9	64.4	66.7	6	110	-3.1	1/10/83
7	192	0	1	1	1	1	50	78.7	73.4	75.9	63.4	68.9	6	110	-3.1	1/10/83
7	193	2	1	1	1	5	46	89.1	81.0	83.7	71.9	75.2	6	110	-3.1	1/10/83
7	194	2	1	1	1	2	59	87.2	78.1	82.1	67.0	71.5	6	110	-3.1	1/10/83
7	195	2	1	1	1	1	59	81.1	73.0	76.0	59.6	65.7	6	150	-7.8	1/10/83
7	196	2	1	1	1	3	54	87.7	79.4	81.5	70.8	74.5	0	270	0.0	1/10/83
7	197	0	1	1	1	5	60	97.1	90.6	91.0	87.4	84.5	0	270	0.0	1/10/83
7	198	2	1	1	1	5	58	87.8	80.4	82.1	71.2	74.4	0	270	0.0	1/10/83
7	199	2	1	1	1	2	55	86.3	79.5	80.7	70.5	73.1	0	270	0.0	1/10/83
7	200	2	1	1	1	5	55	93.6	85.7	88.3	76.4	78.9	6	270	0.0	1/10/83
7	201	2	1	1	1	5	51	86.5	79.3	81.8	70.0	73.2	6	270	0.0	1/10/83
7	202	2	1	1	1	5	56	92.5	86.7	87.9	76.9	78.8	6	270	0.0	1/10/83
7	203	2	1	1	1	3	51	84.9	76.8	79.4	66.9	70.6	6	270	0.0	1/10/83
7	204	2	1	1	1	3	58	86.2	78.9	82.3	68.8	73.6	6	270	0.0	1/10/83
7	205	2	1	1	1	4	62	90.6	84.5	84.8	76.7	78.0	6	240	-4.5	1/10/83
7	206	2	1	1	1	1	53	80.2	73.7	75.6	64.8	68.6	6	240	-4.5	1/10/83
7	207	2	1	1	1	2	54	86.2	78.7	80.4	68.2	72.6	6	240	-4.5	1/10/83
7	208	2	1	1	1	4	62	92.2	85.3	86.6	76.2	78.3	6	240	-4.5	1/10/83
7	209	2	1	1	1	2	62	83.7	76.7	78.4	66.3	69.9	6	240	-4.5	1/10/83
7	210	2	1	1	1	5	59	86.1	80.0	81.3	74.0	75.9	6	240	-4.5	1/10/83

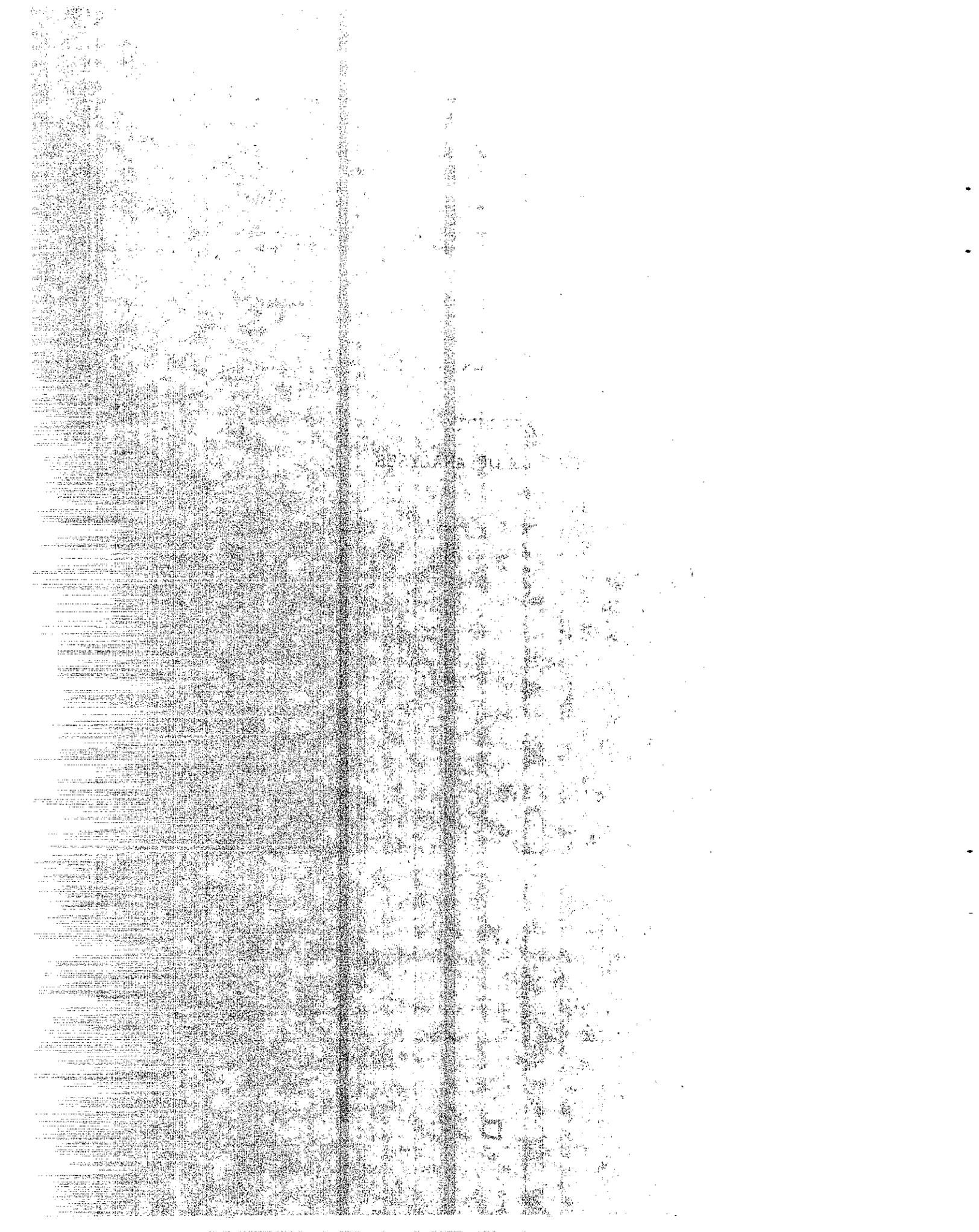
\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH TYPE	SPEED	(1)	(2)	(3)	(4)	(5)	WS IP	WA IN	V WE	DATE
SITE	EVENT	GVDRH	DELN	5	5	10	5	10	NE DE	NG DL	IC NT	DO R
*****												
*****												
*****												
7	211	0 1 1 1	2 50	84.2	78.2	80.4	70.3	73.4	6	240	-4.5	1/10/83
7	212	2 1 1 1	5 51	86.5	79.5	81.1	69.2	73.3	6	240	-4.5	1/10/83
7	213	0 1 1 1	5 58	87.9	81.7	83.5	73.0	75.6	6	240	-4.5	1/10/83
7	214	2 1 1 1	5 53	88.5	82.0	83.9	74.1	76.4	6	270	0.0	1/10/83

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH TYPE	MIC	WS	WA	V	DATE
SITE	EVENT	VEH TYPE	MIC	WS	WA	V	DATE
			(1) (2) (3) (4) (5)	IP	IN	IC	
			5 5 10 5 10	NE	NG	NT	
			DBA	DE	DL	DO	
				D	E	R	
9	1	2 1 1 1	0 55 79.1 76.0 75.3 0.0 0.0	6	180	-9.0	1/11/83
9	2	2 1 1 1	2 55 -1.0 84.0 -1.0 0.0 0.0	6	180	-9.0	1/11/83
9	3	2 1 1 1	0 59 80.5 75.0 75.4 0.0 0.0	6	180	-9.0	1/11/83
9	4	2 1 1 1	0 55 78.1 73.0 73.6 0.0 0.0	6	180	-9.0	1/11/83
9	5	2 1 1 1	5 45 89.2 84.6 84.5 0.0 0.0	6	180	-9.0	1/11/83
9	6	2 1 1 1	2 58 -1.0 83.0 -1.0 0.0 0.0	6	180	-9.0	1/11/83
9	7	2 1 1 1	1 56 -1.0 75.5 -1.0 0.0 0.0	6	180	-9.0	1/11/83
9	8	2 1 1 1	5 53 86.5 80.7 81.2 0.0 0.0	6	180	-9.0	1/11/83
9	9	2 1 1 1	5 52 86.6 81.0 81.2 0.0 0.0	6	180	-9.0	1/11/83
9	10	1 1 1 1	0 53 77.7 72.8 72.6 0.0 0.0	6	180	-9.0	1/11/83
9	11	2 1 1 1	5 49 91.4 86.8 86.2 0.0 0.0	6	180	-9.0	1/11/83
9	12	2 1 1 1	1 61 80.3 75.6 76.1 0.0 0.0	6	180	-9.0	1/11/83
9	13	2 1 1 1	0 57 79.1 74.5 73.6 0.0 0.0	6	180	-9.0	1/11/83
9	14	2 1 1 1	1 51 77.4 72.5 72.0 0.0 0.0	6	180	-9.0	1/11/83
9	15	2 1 1 1	0 58 80.2 75.4 74.7 0.0 0.0	6	180	-9.0	1/11/83
9	16	2 1 1 1	1 61 80.7 74.4 74.4 0.0 0.0	6	180	-9.0	1/11/83
9	17	2 1 1 1	0 53 77.5 71.9 71.6 0.0 0.0	6	180	-9.0	1/11/83
9	18	2 1 1 1	1 57 81.4 76.1 75.6 0.0 0.0	6	180	-9.0	1/11/83
9	19	2 1 1 1	2 56 84.9 79.1 79.6 0.0 0.0	6	180	-9.0	1/11/83
9	20	2 1 1 1	5 55 95.8 89.8 90.2 0.0 0.0	6	180	-9.0	1/11/83
9	21	2 1 1 1	2 52 82.8 77.8 77.4 0.0 0.0	6	180	-9.0	1/11/83
9	22	2 1 1 1	1 52 84.8 79.0 78.6 0.0 0.0	6	180	-9.0	1/11/83
9	23	2 1 1 1	5 59 88.7 83.7 83.5 0.0 0.0	6	180	-9.0	1/11/83
9	24	2 1 1 1	5 55 88.7 83.9 83.6 0.0 0.0	6	180	-9.0	1/11/83
9	25	2 1 1 1	5 43 83.4 78.1 78.6 0.0 0.0	6	180	-9.0	1/11/83
9	26	2 1 1 1	5 61 92.9 89.1 87.3 0.0 0.0	6	180	-9.0	1/11/83
9	27	2 1 1 1	0 55 77.3 72.2 71.9 0.0 0.0	6	180	-9.0	1/11/83
9	28	2 0 1 1	1 49 82.4 76.9 77.8 0.0 0.0	6	170	-8.9	1/11/83
9	29	2 1 1 1	5 55 87.1 82.4 82.2 0.0 0.0	6	170	-8.9	1/11/83
9	30	2 1 1 1	1 57 80.9 75.5 75.9 0.0 0.0	6	170	-8.9	1/11/83
9	31	2 1 1 1	2 55 89.2 84.0 83.7 0.0 0.0	6	170	-8.9	1/11/83
9	32	2 1 1 1	5 46 88.6 82.8 82.8 0.0 0.0	6	170	-8.9	1/11/83
9	33	2 1 1 1	0 48 74.8 70.4 70.2 0.0 0.0	6	170	-8.9	1/11/83
9	34	2 1 1 1	5 65 91.8 86.2 86.2 0.0 0.0	6	170	-8.9	1/11/83
9	35	2 1 1 1	2 60 87.4 83.3 82.1 0.0 0.0	6	170	-8.9	1/11/83
9	36	2 1 1 1	0 53 77.6 72.6 72.8 0.0 0.0	6	170	-8.9	1/11/83
9	37	2 1 1 1	5 54 90.0 84.4 84.8 0.0 0.0	6	170	-8.9	1/11/83
9	38	2 1 1 1	1 44 77.2 72.9 72.1 0.0 0.0	6	170	-8.9	1/11/83
9	39	2 1 1 1	5 57 88.6 83.3 83.1 0.0 0.0	6	170	-8.9	1/11/83
9	40	2 1 1 1	5 50 87.0 81.5 81.6 0.0 0.0	6	170	-8.9	1/11/83
9	41	2 1 1 1	5 52 90.7 85.4 85.7 0.0 0.0	6	170	-8.9	1/11/83
9	42	2 1 1 1	2 55 83.7 79.2 78.5 0.0 0.0	6	170	-8.9	1/11/83
9	43	2 1 1 1	5 57 90.7 86.5 85.5 0.0 0.0	6	170	-8.9	1/11/83
9	44	2 1 1 1	0 57 82.0 75.6 75.8 0.0 0.0	6	170	-8.9	1/11/83
9	45	2 1 1 1	5 53 85.4 79.5 80.5 0.0 0.0	6	170	-8.9	1/11/83
9	46	2 1 1 1	5 49 87.0 83.2 82.5 0.0 0.0	6	170	-8.9	1/11/83
9	47	2 1 1 1	1 54 80.8 74.7 75.7 0.0 0.0	6	170	-8.9	1/11/83
9	48	2 1 1 1	0 64 81.5 76.8 77.4 0.0 0.0	6	170	-8.9	1/11/83
9	49	2 1 1 1	5 51 87.2 83.3 82.5 0.0 0.0	6	170	-8.9	1/11/83
9	50	2 1 1 1	2 49 84.7 80.6 79.9 0.0 0.0	6	170	-8.9	1/11/83
9	51	2 1 1 1	1 60 81.6 76.0 76.6 0.0 0.0	6	170	-8.9	1/11/83
9	52	2 1 1 1	1 54 80.3 74.6 75.5 0.0 0.0	6	170	-8.9	1/11/83
9	53	2 1 1 1	0 56 78.2 72.6 72.6 0.0 0.0	6	170	-8.9	1/11/83
9	54	2 1 1 1	5 52 86.4 80.8 81.0 0.0 0.0	6	170	-8.9	1/11/83
9	55	2 1 1 1	5 57 90.5 84.6 84.7 0.0 0.0	6	170	-8.9	1/11/83
9	56	1 1 1 1	5 62 93.0 87.4 88.0 0.0 0.0	6	170	-8.9	1/11/83
9	57	1 1 1 1	0 46 77.1 72.2 72.8 0.0 0.0	6	170	-8.9	1/11/83
9	58	1 1 1 1	1 52 79.4 74.9 74.5 0.0 0.0	6	170	-8.9	1/11/83
9	59	1 1 1 1	5 54 89.1 83.1 83.6 0.0 0.0	6	170	-8.9	1/11/83
9	60	1 1 1 1	1 52 80.4 74.1 74.4 0.0 0.0	6	170	-8.9	1/11/83
9	61	1 1 1 1	2 43 85.2 80.7 79.9 0.0 0.0	6	170	-8.9	1/11/83
9	62	1 1 1 1	0 61 79.6 75.6 74.2 0.0 0.0	6	170	-8.9	1/11/83
9	63	2 1 1 1	5 53 89.1 83.8 83.8 0.0 0.0	6	170	-8.9	1/11/83
9	64	1 1 1 1	5 52 92.5 86.7 86.7 0.0 0.0	6	170	-8.9	1/11/83
9	65	1 1 1 1	0 60 80.5 75.3 76.2 0.0 0.0	6	170	-8.9	1/11/83
9	66	1 1 1 1	0 56 76.9 71.9 72.6 0.0 0.0	6	170	-8.9	1/11/83
9	67	0 1 1 1	0 60 77.6 72.8 72.7 0.0 0.0	6	170	-8.9	1/11/83
9	68	1 1 1 1	1 60 81.9 77.4 77.4 0.0 0.0	6	170	-8.9	1/11/83
9	69	2 1 1 1	1 62 82.7 76.9 77.4 0.0 0.0	6	170	-8.9	1/11/83
9	70	2 1 1 1	0 51 77.2 72.5 72.0 0.0 0.0	6	170	-8.9	1/11/83





\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	V	QUAL.					DATE				
							G	V	D	E	N		P	E	(1)	(2)
SITE	EVENT	VEH	MIC	WS	WA	V	QUAL.					DATE				
							R	H	L	V	E		D	5	5	10
10	1	1	1	1	1	1	52	78.4	70.2	72.5	0.0	0.0	3	290	1.5	1/12/83
10	2	2	1	1	1	1	57	79.9	73.4	74.7	0.0	0.0	3	290	1.5	1/12/83
10	3	2	1	1	1	2	56	82.5	76.3	76.6	0.0	0.0	3	290	1.5	1/12/83
10	4	0	0	1	1	1	62	80.1	74.1	75.8	0.0	0.0	3	290	1.5	1/12/83
10	5	2	1	1	1	1	61	78.6	71.8	73.4	0.0	0.0	3	290	1.5	1/12/83
10	6	1	1	1	1	3	61	86.0	80.7	81.6	0.0	0.0	3	290	1.5	1/12/83
10	7	0	1	1	1	1	51	75.6	69.6	71.2	0.0	0.0	3	290	1.5	1/12/83
10	8	1	1	1	1	0	61	78.1	72.7	73.6	0.0	0.0	3	290	1.5	1/12/83
10	9	2	1	1	1	3	51	90.4	85.1	85.0	0.0	0.0	3	290	1.5	1/12/83
10	10	1	1	1	1	3	59	84.6	79.8	80.0	0.0	0.0	3	290	1.5	1/12/83
10	11	2	1	1	1	1	54	79.7	72.8	74.3	0.0	0.0	3	290	1.5	1/12/83
10	12	2	1	1	1	0	65	-1.0	73.5	-1.0	0.0	0.0	3	290	1.5	1/12/83
10	13	2	1	1	1	3	52	88.0	81.6	82.4	0.0	0.0	3	290	1.5	1/12/83
10	14	2	1	1	1	4	50	91.0	85.1	86.3	0.0	0.0	3	290	1.5	1/12/83
10	15	2	1	1	1	0	56	76.3	71.3	72.3	0.0	0.0	3	290	1.5	1/12/83
10	16	1	1	1	1	0	46	74.7	68.4	69.4	0.0	0.0	3	290	1.5	1/12/83
10	17	1	1	1	1	0	55	76.5	70.4	72.2	0.0	0.0	3	290	1.5	1/12/83
10	18	0	0	1	1	1	57	79.1	74.1	75.3	0.0	0.0	3	290	1.5	1/12/83
10	19	0	1	1	1	1	56	80.1	73.1	74.9	0.0	0.0	3	290	1.5	1/12/83
10	20	2	1	1	1	5	57	90.8	83.9	85.6	0.0	0.0	3	290	1.5	1/12/83
10	21	1	1	1	1	0	53	76.1	69.8	71.6	0.0	0.0	3	290	1.5	1/12/83
10	22	1	1	1	1	2	52	83.7	76.6	78.2	0.0	0.0	3	290	1.5	1/12/83
10	23	1	1	1	1	1	55	78.3	71.4	73.2	0.0	0.0	3	290	1.5	1/12/83
10	24	1	1	1	1	1	64	84.0	77.8	78.5	0.0	0.0	3	290	1.5	1/12/83
10	25	0	0	1	1	0	54	73.6	69.2	70.0	0.0	0.0	3	290	1.5	1/12/83
10	26	0	0	1	1	0	60	82.3	77.5	79.7	0.0	0.0	3	290	1.5	1/12/83
10	27	0	1	1	1	1	63	80.2	74.5	75.7	0.0	0.0	0	0	0.0	1/12/83
10	28	0	1	1	1	0	62	82.6	77.0	78.2	0.0	0.0	0	0	0.0	1/12/83
10	29	0	0	1	1	0	50	76.2	72.8	73.0	0.0	0.0	0	0	0.0	1/12/83
10	30	2	1	1	1	3	45	88.9	82.6	83.4	0.0	0.0	0	0	0.0	1/12/83
10	31	1	1	1	1	0	50	75.0	68.9	70.3	0.0	0.0	0	0	0.0	1/12/83
10	32	1	1	1	1	1	53	76.6	69.5	71.1	0.0	0.0	0	0	0.0	1/12/83
10	33	1	1	1	1	1	53	79.0	72.1	74.0	0.0	0.0	0	0	0.0	1/12/83
10	34	2	1	1	1	5	60	89.2	83.1	83.7	0.0	0.0	0	0	0.0	1/12/83
10	35	1	1	1	1	0	47	78.8	73.6	73.6	0.0	0.0	0	0	0.0	1/12/83
10	36	2	1	1	1	2	50	84.2	77.7	78.8	0.0	0.0	0	0	0.0	1/12/83
10	37	0	1	1	1	1	57	80.7	73.0	75.0	0.0	0.0	0	0	0.0	1/12/83
10	38	0	0	1	1	0	58	78.2	73.9	74.6	0.0	0.0	0	0	0.0	1/12/83
10	39	0	0	1	1	0	56	77.2	73.6	74.1	0.0	0.0	0	0	0.0	1/12/83
10	40	2	1	1	1	3	54	92.4	85.6	87.2	0.0	0.0	0	0	0.0	1/12/83
10	41	1	1	1	1	0	42	73.8	69.5	70.2	0.0	0.0	0	0	0.0	1/12/83
10	42	2	1	1	1	5	60	-1.0	83.0	-1.0	0.0	0.0	0	0	0.0	1/12/83
10	43	2	1	1	1	5	45	87.2	80.5	81.9	0.0	0.0	0	0	0.0	1/12/83
10	44	2	1	1	1	3	57	88.3	82.0	82.8	0.0	0.0	3	290	1.5	1/12/83
10	45	2	1	1	1	0	54	76.6	70.2	71.4	0.0	0.0	3	290	1.5	1/12/83
10	46	1	1	1	1	1	60	81.7	74.3	76.4	0.0	0.0	3	290	1.5	1/12/83
10	47	2	1	1	1	1	55	80.1	73.6	74.7	0.0	0.0	3	290	1.5	1/12/83
10	48	0	0	1	1	1	60	78.6	72.9	74.2	0.0	0.0	3	290	1.5	1/12/83
10	49	2	1	1	1	5	43	91.4	85.0	86.4	0.0	0.0	3	290	1.5	1/12/83
10	50	1	1	1	1	2	52	83.7	78.1	78.5	0.0	0.0	3	290	1.5	1/12/83
10	51	1	1	1	1	1	54	79.4	72.9	74.3	0.0	0.0	3	290	1.5	1/12/83
10	52	0	0	1	1	1	57	77.7	71.8	72.9	0.0	0.0	0	0	0.0	1/12/83
10	53	1	1	1	1	2	52	85.0	79.6	80.6	0.0	0.0	0	0	0.0	1/12/83
10	54	2	1	1	1	2	50	-1.0	82.5	-1.0	0.0	0.0	0	0	0.0	1/12/83
10	55	0	0	0	1	0	46	79.4	73.3	75.2	0.0	0.0	0	0	0.0	1/12/83
10	56	1	1	1	1	0	54	76.3	71.0	72.3	0.0	0.0	0	0	0.0	1/12/83
10	57	1	1	1	1	0	55	77.0	70.7	71.6	0.0	0.0	0	0	0.0	1/12/83
10	58	1	1	1	1	1	51	76.1	70.8	71.5	0.0	0.0	0	0	0.0	1/12/83
10	59	1	1	1	1	2	54	81.3	73.8	75.2	0.0	0.0	0	0	0.0	1/12/83
10	60	1	1	1	1	0	56	75.2	69.7	70.7	0.0	0.0	0	0	0.0	1/12/83
10	61	1	1	1	1	1	58	78.4	70.9	73.0	0.0	0.0	0	0	0.0	1/12/83
10	62	1	1	1	1	0	64	78.6	72.2	74.2	0.0	0.0	0	0	0.0	1/12/83
10	63	2	1	1	1	2	62	88.3	82.1	82.5	0.0	0.0	0	0	0.0	1/12/83
10	64	0	1	1	1	0	58	80.5	74.5	75.6	0.0	0.0	0	0	0.0	1/12/83
10	65	1	1	1	1	1	61	81.6	73.9	76.3	0.0	0.0	0	0	0.0	1/12/83
10	66	1	1	1	1	0	57	78.1	71.3	73.2	0.0	0.0	0	0	0.0	1/12/83
10	67	0	0	1	1	0	48	77.4	70.8	72.2	0.0	0.0	0	0	0.0	1/12/83
10	68	1	1	1	1	2	58	84.5	79.2	78.5	0.0	0.0	0	0	0.0	1/12/83
10	69	2	1	1	1	2	58	92.2	86.0	86.4	0.0	0.0	0	0	0.0	1/12/83
10	70	2	1	1	1	5	50	85.1	78.7	79.8	0.0	0.0	0	0	0.0	1/12/83

***** DATA SUMMARY *****														
LOC.	* EVENT * * QUAL.	* VEH * * T S * * P E * * D	MIC					* WS * * IP * * NE * * DE * * D	* WA * * IN * * NG * * DL * * E	* V * * WE * * IC * * NT * * DO * * R *	DATE			
S I T E	E V E N T	G V D E /	R H L V	(1) 5	(2) 5	(3) 10	(4) 5	(5) 10	DBA					
10	71	2 1 1 1	5 59	88.0	82.1	82.4	0.0	0.0	0	0	0.0	1/12/83		
10	72	0 1 1 1	0 46	77.6	74.6	74.9	0.0	0.0	0	0	0.0	1/12/83		
10	73	1 1 1 1	1 61	80.1	73.1	74.7	0.0	0.0	0	0	0.0	1/12/83		
10	74	1 1 1 1	1 57	81.3	74.2	75.4	0.0	0.0	0	0	0.0	1/12/83		
10	75	0 1 1 1	0 51	77.6	72.9	73.6	0.0	0.0	0	0	0.0	1/12/83		
10	76	1 1 1 1	1 57	76.7	71.0	72.3	0.0	0.0	0	0	0.0	1/12/83		
10	77	1 1 1 1	3 61	85.1	78.3	79.5	0.0	0.0	0	0	0.0	1/12/83		
10	78	0 1 1 1	0 56	80.0	74.4	75.3	0.0	0.0	0	0	0.0	1/12/83		
10	79	1 1 1 1	2 53	84.6	78.8	79.8	0.0	0.0	0	0	0.0	1/12/83		
10	80	1 1 1 1	2 56	85.3	78.9	79.9	0.0	0.0	0	0	0.0	1/12/83		
10	81	0 1 1 1	2 55	82.4	76.8	77.1	0.0	0.0	0	0	0.0	1/12/83		
10	82	0 1 1 1	1 62	80.0	73.3	74.4	0.0	0.0	0	0	0.0	1/12/83		
10	83	2 1 1 1	2 50	83.8	77.8	78.8	0.0	0.0	0	0	0.0	1/12/83		
10	84	1 1 1 1	2 60	87.1	80.1	81.2	0.0	0.0	0	0	0.0	1/12/83		
10	85	2 1 1 1	5 54	86.2	80.4	81.3	0.0	0.0	0	0	0.0	1/12/83		
10	86	1 1 1 1	3 42	84.3	77.6	77.8	0.0	0.0	0	0	0.0	1/12/83		
10	87	0 1 1 1	0 52	77.7	72.5	72.8	0.0	0.0	0	0	0.0	1/12/83		
10	88	1 1 1 1	0 64	82.4	75.6	77.4	0.0	0.0	0	0	0.0	1/12/83		
10	89	0 1 1 1	0 59	79.2	73.2	74.7	0.0	0.0	0	0	0.0	1/12/83		
10	90	1 1 1 1	2 55	86.3	78.6	81.4	0.0	0.0	0	0	0.0	1/12/83		
10	91	2 1 1 1	5 54	88.8	82.6	83.1	0.0	0.0	0	0	0.0	1/12/83		
10	92	1 1 1 1	1 48	76.2	70.9	72.3	0.0	0.0	0	0	0.0	1/12/83		
10	93	0 0 1 1	1 55	78.7	74.6	75.7	0.0	0.0	0	0	0.0	1/12/83		
10	94	1 1 1 1	0 57	77.3	72.1	72.9	0.0	0.0	0	0	0.0	1/12/83		
10	95	1 1 1 1	0 57	75.6	69.8	71.3	0.0	0.0	0	0	0.0	1/12/83		
10	96	2 1 1 1	2 52	89.1	82.4	83.3	0.0	0.0	0	0	0.0	1/12/83		
10	97	1 1 1 1	2 45	81.7	76.5	77.3	0.0	0.0	0	0	0.0	1/12/83		
10	98	0 1 1 1	0 54	75.4	69.7	71.0	0.0	0.0	0	0	0.0	1/12/83		
10	99	1 1 1 1	0 54	78.3	72.0	72.9	0.0	0.0	0	0	0.0	1/12/83		
10	100	0 1 1 1	1 59	80.6	73.2	75.2	0.0	0.0	0	0	0.0	1/12/83		





\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH	MIC	WS	WA	V	DATE				
SITE	EVENT	TYPE	(1)	(2)	(3)	(4)	(5)	IP	IN	WE	DATE
	GL	VE	(1)	(2)	(3)	(4)	(5)	NE	NG	IC	DATE
	LR	HL	5	5	10	5	10	DE	DL	NT	DATE
		V	DBA					D	E	DO	DATE
										R	DATE
11 141	1 1 1 1	0 64	81.1	75.3	76.2	70.3	70.9	6	270	0.0	2/ 8/83
11 142	1 1 1 1	1 61	78.0	72.6	74.0	68.2	68.3	6	270	0.0	2/ 8/83
11 143	2 1 1 1	1 59	76.4	70.7	71.4	66.6	68.4	6	270	0.0	2/ 8/83
11 144	2 1 1 1	1 55	77.9	72.3	73.3	67.5	68.9	6	270	0.0	2/ 8/83
11 145	2 1 1 1	0 57	77.7	73.4	73.2	67.3	68.9	6	270	0.0	2/ 8/83
11 146	0 0 1 1	0 52	76.3	72.5	73.4	67.9	70.4	6	270	0.0	2/ 8/83
11 147	0 0 1 1	1 55	79.8	75.7	75.9	72.1	72.1	6	270	0.0	2/ 8/83
11 148	0 0 1 1	1 56	76.3	71.8	72.4	66.9	67.6	6	270	0.0	2/ 8/83
11 149	0 1 1 1	0 53	77.8	72.9	73.8	68.2	70.5	6	270	0.0	2/ 8/83
11 150	2 1 1 1	5 52	84.0	79.3	79.3	74.9	74.4	6	270	0.0	2/ 8/83
11 151	2 1 1 1	1 55	76.6	72.2	72.1	66.9	68.1	6	270	0.0	2/ 8/83
11 152	2 1 1 1	1 53	78.9	73.4	74.3	68.5	69.7	6	270	0.0	2/ 8/83
11 153	2 1 1 1	5 54	85.0	79.9	79.8	76.0	75.2	6	270	0.0	2/ 8/83
11 154	2 1 1 1	5 58	87.5	84.0	83.5	79.1	77.7	6	270	0.0	2/ 8/83
11 155	2 1 1 1	2 69	85.9	81.6	81.1	77.8	76.5	6	270	0.0	2/ 8/83
11 156	0 1 1 1	2 60	82.9	77.9	77.5	74.2	73.4	6	270	0.0	2/ 8/83
11 157	2 1 1 1	2 60	85.1	80.0	79.9	76.2	74.4	6	270	0.0	2/ 8/83
11 158	2 1 1 1	5 63	88.9	84.0	84.1	78.7	78.6	6	270	0.0	2/ 8/83
11 159	2 1 1 1	5 61	88.2	84.1	83.9	79.3	79.0	6	270	0.0	2/ 8/83
11 160	2 1 1 1	3 59	85.5	80.2	80.7	76.0	74.7	6	270	0.0	2/ 8/83
11 161	2 1 1 1	5 71	89.1	85.1	84.5	81.0	79.6	6	270	0.0	2/ 8/83
11 162	2 1 1 1	3 64	91.2	85.5	84.7	81.2	79.6	6	270	0.0	2/ 8/83
11 163	2 1 1 1	5 60	84.6	80.1	79.7	75.2	75.1	6	270	0.0	2/ 8/83
11 164	0 1 1 1	1 61	77.7	72.9	73.2	67.7	68.5	6	270	0.0	2/ 8/83
11 165	2 1 1 1	5 59	89.3	84.0	84.9	79.7	78.5	6	270	0.0	2/ 8/83
11 166	2 1 1 1	2 53	82.4	77.9	77.0	72.3	73.1	6	270	0.0	2/ 8/83
11 167	2 1 1 1	2 59	91.2	87.0	87.5	78.1	79.3	6	270	0.0	2/ 8/83
11 168	2 1 1 1	1 60	79.0	74.3	75.4	70.6	71.4	6	270	0.0	2/ 8/83
11 169	2 1 1 1	5 56	85.2	80.3	81.0	77.2	75.3	6	270	0.0	2/ 8/83
11 170	2 1 1 1	5 61	88.5	84.1	84.1	80.1	79.0	6	270	0.0	2/ 8/83
11 171	2 1 1 1	5 57	86.6	82.1	81.9	78.8	77.6	6	270	0.0	2/ 8/83
11 172	2 1 1 1	0 56	77.5	73.4	72.6	67.8	68.9	6	270	0.0	2/ 8/83
11 173	2 1 1 1	3 66	87.7	82.6	82.8	78.2	77.5	6	270	0.0	2/ 8/83
11 174	2 1 1 1	3 62	86.0	82.1	81.6	77.3	77.7	6	270	0.0	2/ 8/83
11 175	2 1 1 1	2 58	82.2	77.1	77.6	73.8	73.6	6	270	0.0	2/ 8/83
11 176	2 1 1 1	5 56	85.1	80.3	79.9	75.5	75.1	6	270	0.0	2/ 8/83
11 177	2 1 1 1	0 62	79.7	74.4	74.5	69.0	69.6	6	270	0.0	2/ 8/83
11 178	2 1 1 1	1 62	78.2	73.4	74.5	69.4	68.6	6	270	0.0	2/ 8/83
11 179	2 1 1 1	1 62	84.9	79.9	80.3	74.3	74.9	6	270	0.0	2/ 8/83
11 180	0 1 1 1	0 61	76.0	70.9	71.5	66.2	66.6	6	270	0.0	2/ 8/83
11 181	2 1 1 1	5 59	86.4	82.1	81.6	77.8	76.7	6	270	0.0	2/ 8/83
11 182	2 1 1 1	3 56	90.5	85.2	85.9	79.4	79.7	6	270	0.0	2/ 8/83
11 183	2 1 1 1	0 59	78.7	73.6	73.8	69.3	70.0	6	270	0.0	2/ 8/83
11 184	2 1 1 1	5 61	86.9	81.9	82.3	78.0	77.0	6	270	0.0	2/ 8/83
11 185	2 1 1 1	5 59	84.7	79.7	80.2	75.8	75.5	6	270	0.0	2/ 8/83
11 186	2 1 1 1	5 64	88.5	84.0	83.4	79.3	78.2	6	270	0.0	2/ 8/83
11 187	2 1 1 1	5 62	90.7	84.7	85.2	81.7	81.7	6	270	0.0	2/ 8/83
11 188	2 1 1 1	2 62	89.3	85.3	84.6	81.3	80.2	6	270	0.0	2/ 8/83
11 189	2 1 1 1	3 56	84.7	79.1	80.1	74.8	74.8	6	270	0.0	2/ 8/83
11 190	2 1 1 1	1 71	80.3	75.0	76.1	70.0	70.0	6	270	0.0	2/ 8/83
11 191	1 1 1 1	1 57	78.1	72.4	73.7	68.6	68.8	6	270	0.0	2/ 8/83
11 192	2 1 1 1	0 56	80.8	75.0	76.1	70.6	70.3	6	270	0.0	2/ 8/83
11 193	0 1 1 1	1 63	79.6	73.7	75.2	69.0	68.7	6	270	0.0	2/ 8/83
11 194	0 1 1 1	0 63	77.8	73.7	73.3	68.2	69.9	6	270	0.0	2/ 8/83
11 195	2 1 1 1	0 61	75.5	70.8	71.2	66.1	67.0	6	270	0.0	2/ 8/83
11 196	2 1 1 1	3 57	88.1	83.6	83.3	77.3	77.2	6	270	0.0	2/ 8/83
11 197	2 1 1 1	3 53	85.8	80.4	80.5	76.3	75.6	6	270	0.0	2/ 8/83
11 198	2 1 1 1	0 56	77.9	73.5	72.9	69.3	69.6	6	270	0.0	2/ 8/83
11 199	2 1 1 1	0 61	77.2	71.9	72.3	66.0	67.8	6	270	0.0	2/ 8/83
11 200	2 1 1 1	4 61	86.2	80.2	80.5	76.3	75.2	6	270	0.0	2/ 8/83

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	V	DATE					
	QUAL.						IP	IN	WE							
S	E	T	(1)	(2)	(3)	(4)	NE	NG	IC							
I	V	P	5	5	10	5	DE	DL	NT							
T	R	E	5	5	10	5	D	E	DO	DATE						
E	H	N	DBA						R							
	L	L														
	V	V														
	L	L														
	R	L														
	H	V														
	L	L														
	V	V														
	L	L														
	R	L														
	H	V														
12	1	2	1	1	1	1	60	81.1	75.3	75.0	68.9	70.6	0	90	0.0	2/ 9/83
12	2	2	1	1	1	3	56	84.1	78.5	78.9	71.5	73.1	0	90	0.0	2/ 9/83
12	3	2	1	1	1	1	63	75.6	70.8	70.4	64.5	67.3	0	90	0.0	2/ 9/83
12	4	2	1	1	1	0	61	73.7	68.1	68.4	61.8	64.7	0	90	0.0	2/ 9/83
12	5	2	1	1	1	5	59	91.3	87.1	86.4	80.8	82.1	0	90	0.0	2/ 9/83
12	6	1	1	1	1	0	50	73.0	67.5	67.5	61.2	63.3	0	90	0.0	2/ 9/83
12	7	2	1	1	1	2	46	82.3	76.8	76.6	70.2	71.6	0	90	0.0	2/ 9/83
12	8	2	1	1	1	5	56	86.7	81.9	81.4	74.8	76.4	0	90	0.0	2/ 9/83
12	9	2	1	1	1	5	60	88.2	83.9	83.2	78.3	79.0	0	90	0.0	2/ 9/83
12	10	2	1	1	1	3	54	85.8	80.7	79.8	72.9	74.1	0	90	0.0	2/ 9/83
12	11	2	1	1	1	0	46	71.9	66.3	66.1	60.4	61.0	0	90	0.0	2/ 9/83
12	12	2	1	1	1	5	69	90.0	85.3	84.9	77.9	79.8	0	90	0.0	2/ 9/83
12	13	2	1	1	1	1	58	86.7	82.0	81.6	75.2	76.9	0	90	0.0	2/ 9/83
12	14	2	1	1	1	1	56	74.7	68.7	68.9	62.5	64.4	0	90	0.0	2/ 9/83
12	15	2	1	1	1	5	57	84.0	79.4	79.0	72.7	74.6	0	90	0.0	2/ 9/83
12	16	2	1	1	1	5	51	85.7	81.2	80.6	74.2	75.4	0	300	0.0	2/ 9/83
12	17	2	1	1	1	1	59	76.2	70.7	70.7	64.8	66.7	0	300	0.0	2/ 9/83
12	18	2	1	1	1	5	52	84.2	79.4	78.7	72.9	73.7	0	300	0.0	2/ 9/83
12	19	2	1	1	1	5	53	86.8	83.3	81.7	75.6	76.8	0	300	0.0	2/ 9/83
12	20	2	1	1	1	1	56	79.7	74.5	74.0	69.0	70.4	0	300	0.0	2/ 9/83
12	21	2	1	1	1	5	58	91.7	88.1	86.3	81.2	81.8	0	300	0.0	2/ 9/83
12	22	2	1	1	1	1	60	75.5	70.4	70.2	64.1	66.9	0	300	0.0	2/ 9/83
12	23	2	1	1	1	5	52	89.5	85.1	84.0	78.9	80.4	0	300	0.0	2/ 9/83
12	24	2	1	1	1	0	60	73.6	67.5	68.1	61.8	63.5	0	300	0.0	2/ 9/83
12	25	2	1	1	1	5	62	87.9	82.8	82.3	75.6	76.8	0	300	0.0	2/ 9/83
12	26	2	1	1	1	2	55	84.6	81.2	79.2	74.4	74.9	0	300	0.0	2/ 9/83
12	27	2	1	1	1	1	61	75.8	71.3	70.9	65.1	66.3	0	300	0.0	2/ 9/83
12	28	2	1	1	1	1	54	76.7	71.3	71.3	64.6	67.2	0	300	0.0	2/ 9/83
12	29	2	1	1	1	5	53	85.6	81.8	80.9	75.9	76.6	0	300	0.0	2/ 9/83
12	30	2	1	1	1	2	59	86.3	81.3	80.7	74.3	75.8	0	270	0.0	2/ 9/83
12	31	2	1	1	1	1	60	73.3	67.8	67.1	61.1	63.3	0	270	0.0	2/ 9/83
12	32	2	1	1	1	0	56	75.2	69.9	69.6	63.4	65.4	0	270	0.0	2/ 9/83
12	33	2	1	1	1	3	59	86.3	81.0	80.6	74.2	75.9	0	270	0.0	2/ 9/83
12	34	2	1	1	1	0	64	77.2	71.7	71.5	65.2	67.1	0	270	0.0	2/ 9/83
12	35	2	1	1	1	1	61	73.9	68.8	68.8	63.2	64.8	0	270	0.0	2/ 9/83
12	36	2	1	1	1	1	58	73.6	68.2	68.0	61.7	63.5	0	270	0.0	2/ 9/83
12	37	2	1	1	1	5	53	87.9	82.3	83.0	76.6	76.4	0	270	0.0	2/ 9/83
12	38	2	1	1	1	0	60	77.9	72.7	72.6	66.3	67.8	0	270	0.0	2/ 9/83
12	39	0	1	1	1	2	46	82.5	77.3	77.1	71.4	73.4	0	270	0.0	2/ 9/83
12	40	2	1	1	1	2	55	79.1	74.3	73.3	66.8	69.0	0	300	0.0	2/ 9/83
12	41	2	1	1	1	1	64	79.1	74.6	73.8	67.2	69.0	0	300	0.0	2/ 9/83
12	42	2	1	1	1	0	58	75.8	70.7	70.4	64.7	65.5	0	300	0.0	2/ 9/83
12	43	2	1	1	1	1	57	77.0	71.1	70.8	64.2	66.8	0	300	0.0	2/ 9/83
12	44	2	1	1	1	1	65	76.0	70.7	70.3	64.0	66.6	0	300	0.0	2/ 9/83
12	45	2	1	1	1	5	45	86.3	80.9	81.0	74.8	75.6	0	300	0.0	2/ 9/83
12	46	2	1	1	1	0	55	77.8	72.3	71.8	66.1	67.8	0	300	0.0	2/ 9/83
12	47	2	1	1	1	1	61	76.6	71.1	70.9	64.9	66.5	0	300	0.0	2/ 9/83
12	48	2	1	1	1	0	58	74.6	69.4	69.1	63.1	64.5	0	300	0.0	2/ 9/83
12	49	2	1	1	1	5	49	84.7	80.2	80.0	73.6	74.3	0	300	0.0	2/ 9/83
12	50	2	1	1	1	2	52	78.0	73.1	72.4	66.6	68.7	0	300	0.0	2/ 9/83
12	51	2	1	1	1	0	59	72.6	67.2	67.3	61.5	63.0	0	300	0.0	2/ 9/83
12	52	2	1	1	1	5	54	86.6	82.3	81.9	75.9	77.7	0	300	0.0	2/ 9/83
12	53	2	1	1	1	0	54	76.1	70.2	70.6	63.6	65.3	0	300	0.0	2/ 9/83
12	54	2	1	1	1	5	54	88.6	84.2	83.2	77.5	78.4	0	300	0.0	2/ 9/83
12	55	2	1	1	1	1	52	74.5	69.2	68.9	62.0	64.5	0	300	0.0	2/ 9/83
12	56	2	1	1	1	1	57	73.4	68.4	68.1	61.4	64.0	0	300	0.0	2/ 9/83
12	57	2	1	1	1	5	54	83.1	78.2	77.8	70.9	73.6	0	300	0.0	2/ 9/83
12	58	2	1	1	1	5	57	88.4	84.0	83.2	77.3	79.7	0	300	0.0	2/ 9/83
12	59	2	1	1	1	5	59	88.8	84.2	84.2	76.0	78.7	0	120	0.0	2/ 9/83
12	60	1	1	1	1	3	46	83.2	78.4	77.8	71.9	72.8	0	120	0.0	2/ 9/83
12	61	2	1	1	1	3	51	84.9	80.0	79.2	72.9	74.2	0	120	0.0	2/ 9/83
12	62	2	1	1	1	1	56	74.3	69.5	69.5	63.7	64.9	0	120	0.0	2/ 9/83
12	63	1	1	1	1	1	64	76.0	71.4	71.1	66.5	67.5	0	120	0.0	2/ 9/83
12	64	2	1	1	1	2	54	80.2	74.6	74.3	67.5	69.5	3	330	3.9	2/ 9/83
12	65	2	1	1	1	0	47	72.1	66.8	66.9	61.0	62.9	3	330	3.9	2/ 9/83
12	66	2	1	1	1	1	55	79.1	73.7	73.3	67.8	68.5	3	330	3.9	2/ 9/83
12	67	2	1	1	1	5	54	88.3	83.5	82.7	76.1	77.8	3	330	3.9	2/ 9/83
12	68	2	1	1	1	3	52	83.6	78.8	78.2	72.6	73.5	3	330	3.9	2/ 9/83
12	69	2	1	1	1	1	53	78.1	72.3	72.0	66.0	68.4	3	330	3.9	2/ 9/83
12	70	2	1	1	1	1	52	74.6	69.3	69.0	62.6	64.8	3	330	3.9	2/ 9/83



\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	QUAL.	VEH	MIC	WS	WA	V									
SITE	EVENT	GRHLV	TYPE	(1)	(2)	(3)	(4)	(5)	IP	NE	NG	WE	IC	NT	DO	DATE
				5	5	10	5	10	DE	DL	DL	DL	DL	DL	DL	
				DBA					D	E	E	R	R	R	R	
12	141	2 1 1 1	5 56	92.4	86.9	87.5	79.6	81.1	6	270	0.0	2/	9/83			
12	142	2 1 1 1	1 58	73.4	67.5	67.8	61.6	63.5	6	270	0.0	2/	9/83			
12	143	2 1 1 1	0 64	75.2	69.4	69.4	62.6	64.9	6	270	0.0	2/	9/83			
12	144	2 1 1 1	1 66	77.9	72.3	72.0	66.0	67.4	6	270	0.0	2/	9/83			
12	145	2 1 1 1	2 55	77.9	73.7	74.3	68.4	70.5	6	270	0.0	2/	9/83			
12	146	1 1 1 1	1 58	73.9	68.5	69.1	62.9	64.1	6	290	3.1	2/	9/83			
12	147	2 1 1 1	3 53	82.3	76.9	76.3	69.5	72.5	6	290	3.1	2/	9/83			
12	148	2 1 1 1	5 47	84.0	78.4	78.6	70.9	72.5	6	290	3.1	2/	9/83			
12	149	2 1 1 1	5 58	89.9	83.9	83.7	76.9	78.5	6	290	3.1	2/	9/83			
12	150	2 1 1 1	1 63	91.8	85.5	85.5	79.3	80.0	6	290	3.1	2/	9/83			
12	151	2 1 1 1	4 56	85.9	81.5	80.6	75.7	77.6	6	290	3.1	2/	9/83			
12	152	2 1 1 1	1 61	75.6	70.1	70.1	64.3	64.8	6	290	3.1	2/	9/83			
12	153	2 1 1 1	3 48	87.9	83.2	82.4	77.2	77.1	6	290	3.1	2/	9/83			
12	154	2 1 1 1	5 58	84.3	78.8	78.8	72.3	74.0	6	290	3.1	2/	9/83			
12	155	2 1 1 1	1 56	75.5	69.5	69.9	62.2	64.7	6	290	3.1	2/	9/83			
12	156	2 1 1 1	3 56	82.2	77.1	77.0	69.4	72.2	6	290	3.1	2/	9/83			
12	157	2 1 1 1	1 59	74.7	69.4	69.4	62.7	65.5	6	290	3.1	2/	9/83			
12	158	0 0 1 1	2 57	83.0	79.6	79.0	73.7	76.0	6	290	3.1	2/	9/83			
12	159	2 1 1 1	1 65	77.7	71.6	71.9	65.0	67.6	6	290	3.1	2/	9/83			
12	160	2 1 1 1	4 48	96.5	91.1	90.7	83.9	84.8	6	290	3.1	2/	9/83			
12	161	2 1 1 1	1 44	76.7	72.0	71.7	66.9	68.0	6	290	3.1	2/	9/83			
12	162	2 1 1 1	3 51	88.6	83.2	82.1	75.4	77.5	6	290	3.1	2/	9/83			
12	163	2 1 1 1	0 70	87.5	71.8	82.1	75.3	77.3	6	290	3.1	2/	9/83			
12	164	2 1 1 1	1 55	73.3	67.4	67.7	61.7	62.8	6	290	3.1	2/	9/83			
12	165	2 1 1 1	0 65	72.9	67.0	67.3	61.2	63.3	6	290	3.1	2/	9/83			
12	166	2 1 1 1	1 55	72.7	66.3	67.4	60.3	62.8	6	290	3.1	2/	9/83			
12	167	2 1 1 1	5 54	94.8	88.8	89.9	82.7	83.0	6	290	3.1	2/	9/83			
12	168	2 1 1 1	3 49	84.4	79.5	79.1	72.2	74.4	6	290	3.1	2/	9/83			
12	169	2 1 1 1	3 59	91.1	85.8	85.3	79.1	80.7	6	290	3.1	2/	9/83			
12	170	2 1 1 1	1 61	74.4	68.9	69.4	62.9	64.4	6	290	3.1	2/	9/83			
12	171	1 1 1 1	1 64	78.0	72.4	72.8	65.1	67.4	6	290	3.1	2/	9/83			
12	172	2 1 1 1	0 63	73.0	66.9	67.7	61.1	62.1	6	290	3.1	2/	9/83			
12	173	2 1 1 1	5 51	85.3	80.1	79.9	73.5	74.8	6	290	3.1	2/	9/83			
12	174	2 1 1 1	5 56	88.0	82.3	81.8	75.0	75.9	6	290	3.1	2/	9/83			
12	175	1 1 1 1	1 51	72.7	67.7	67.6	62.2	63.1	6	290	3.1	2/	9/83			
12	176	2 1 1 1	3 59	90.5	85.0	84.2	77.9	79.5	6	290	3.1	2/	9/83			
12	177	2 1 1 1	3 55	89.6	85.3	84.4	78.7	79.9	6	290	3.1	2/	9/83			
12	178	2 1 1 1	5 61	83.9	78.8	78.4	72.4	73.3	6	290	3.1	2/	9/83			
12	179	0 0 1 1	4 58	84.6	79.2	79.7	75.2	76.0	6	290	3.1	2/	9/83			
12	180	2 1 1 1	1 66	-1.0	72.5	72.4	66.5	68.3	6	290	3.1	2/	9/83			
12	181	2 1 1 1	5 58	-1.0	87.2	87.5	79.6	81.2	6	290	3.1	2/	9/83			
12	182	2 1 1 1	1 63	-1.0	72.4	72.2	66.0	67.7	6	290	3.1	2/	9/83			
12	183	2 1 1 1	0 60	-1.0	69.0	68.9	62.9	65.4	6	290	3.1	2/	9/83			
12	184	2 1 1 1	1 55	-1.0	70.9	71.9	64.1	66.1	6	290	3.1	2/	9/83			
12	185	2 1 1 1	5 52	-1.0	80.2	79.3	-1.0	-1.0	6	290	3.1	2/	9/83			
12	186	2 1 1 1	5 53	-1.0	85.9	85.4	80.3	81.9	6	290	3.1	2/	9/83			
12	187	2 1 1 1	5 53	-1.0	76.4	76.1	69.5	72.0	6	290	3.1	2/	9/83			
12	188	2 1 1 1	5 64	-1.0	86.2	85.4	79.5	-1.0	6	290	3.1	2/	9/83			
12	189	0 0 1 1	5 61	-1.0	85.1	85.4	77.3	78.9	6	290	3.1	2/	9/83			
12	190	2 1 1 1	5 55	-1.0	83.8	83.0	77.1	78.7	6	290	3.1	2/	9/83			
12	191	2 1 1 1	5 55	-1.0	82.6	82.0	76.0	77.1	6	290	3.1	2/	9/83			
12	192	2 1 1 1	1 58	-1.0	69.9	70.1	63.6	65.8	6	290	3.1	2/	9/83			
12	193	2 1 1 1	1 60	-1.0	69.8	69.9	63.4	64.4	6	290	3.1	2/	9/83			
12	194	2 1 1 1	1 54	-1.0	69.6	69.7	63.5	63.9	6	290	3.1	2/	9/83			
12	195	2 1 1 1	0 55	-1.0	65.9	66.2	59.2	60.6	3	260	-8	2/	9/83			
12	196	2 1 1 1	5 55	-1.0	79.7	79.8	72.2	74.8	3	260	-8	2/	9/83			
12	197	2 1 1 1	0 57	-1.0	69.2	69.7	61.5	64.9	3	260	-8	2/	9/83			
12	198	1 1 1 1	0 35	-1.0	64.0	63.8	58.3	59.8	3	260	-8	2/	9/83			
12	199	2 1 1 1	5 52	-1.0	81.6	81.2	74.4	76.8	3	260	-8	2/	9/83			
12	200	2 1 1 1	1 59	-1.0	72.4	71.7	66.6	67.3	6	270	0.0	2/	9/83			









\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	WE	V	DATE														
									QUAL.	T	S	IP	IN	IC								
SITE	EVENT	G	V	D	E	N	P	E	(1)	(2)	(3)	(4)	(5)	NE	NG	NT	DO	R				
																			R	H	L	V
																		DBA	DBA	DBA	DBA	DBA
15	71	2	1	1	1	5	67	96.2	88.7	90.1	81.3	82.5	0	240	0.0	2/15/83						
15	72	2	1	1	1	2	58	85.3	78.0	78.9	70.5	72.3	0	240	0.0	2/15/83						
15	73	2	1	1	1	3	47	86.4	79.0	80.4	72.2	73.7	0	240	0.0	2/15/83						
15	74	2	1	1	1	1	63	77.9	71.5	73.7	64.3	68.0	0	240	0.0	2/15/83						
15	75	2	1	1	1	5	62	93.8	86.6	88.0	79.7	80.5	0	240	0.0	2/15/83						
15	76	2	1	1	1	5	55	88.7	81.6	83.2	75.1	76.5	0	240	0.0	2/15/83						
15	77	2	1	1	1	7	61	86.7	80.1	71.1	70.0	72.7	0	240	0.0	2/15/83						
15	78	2	1	1	1	5	59	88.1	81.0	82.4	74.7	75.8	0	240	0.0	2/15/83						
15	79	2	1	1	1	5	62	90.7	83.1	84.6	76.2	77.6	0	240	0.0	2/15/83						
15	80	2	1	1	1	2	62	88.9	80.6	82.9	73.9	75.7	0	240	0.0	2/15/83						
15	81	2	1	1	1	5	65	92.3	85.3	86.0	78.4	79.1	0	240	0.0	2/15/83						
15	82	2	1	1	1	5	65	95.5	88.0	89.7	80.3	82.1	0	240	0.0	2/15/83						
15	83	2	1	1	1	5	55	85.0	79.2	80.1	73.4	75.9	0	240	0.0	2/15/83						
15	84	2	1	1	1	5	60	89.5	82.7	83.8	75.6	77.0	0	240	0.0	2/15/83						
15	85	0	1	1	1	0	64	78.9	72.2	73.9	65.3	67.6	0	240	0.0	2/15/83						
15	86	2	1	1	1	5	60	88.8	81.2	82.6	73.8	75.4	0	240	0.0	2/15/83						
15	87	2	1	1	1	3	55	95.2	89.4	88.5	83.0	82.3	0	240	0.0	2/15/83						
15	88	2	1	1	1	5	58	93.5	88.4	87.4	83.1	82.6	0	240	0.0	2/15/83						
15	89	0	0	1	1	5	55	92.6	86.7	87.4	79.6	82.5	0	240	0.0	2/15/83						
15	90	0	0	1	1	4	60	87.3	81.0	82.4	75.2	76.3	0	240	0.0	2/15/83						
15	91	2	1	1	1	3	63	90.1	82.8	83.8	75.4	76.4	0	240	0.0	2/15/83						
15	92	2	1	1	1	5	60	93.0	87.1	87.1	80.5	81.2	0	240	0.0	2/15/83						
15	93	2	1	1	1	5	61	93.7	87.1	88.2	80.0	81.2	0	240	0.0	2/15/83						
15	94	2	1	1	1	5	58	86.0	79.4	80.5	72.3	74.3	0	240	0.0	2/15/83						
15	95	2	1	1	1	5	56	92.7	85.3	86.5	78.1	79.5	0	240	0.0	2/15/83						
15	96	2	1	1	1	5	61	93.9	85.8	87.2	78.5	79.3	0	240	0.0	2/15/83						
15	97	2	1	1	1	5	64	91.8	85.8	86.1	78.4	79.4	0	240	0.0	2/15/83						
15	98	1	1	1	1	0	59	78.7	72.1	73.0	64.5	67.2	0	240	0.0	2/15/83						
15	99	2	1	1	1	5	54	88.2	80.8	82.3	74.8	76.0	0	240	0.0	2/15/83						
15	100	1	1	1	1	2	59	82.2	76.3	77.2	69.5	71.7	0	240	0.0	2/15/83						
15	101	2	1	1	1	4	65	92.0	84.5	85.7	77.7	78.2	0	240	0.0	2/15/83						
15	102	2	1	1	1	7	60	88.0	80.7	81.3	73.2	75.1	0	240	0.0	2/15/83						
15	103	2	1	1	1	2	61	86.5	79.2	80.6	73.4	74.6	0	240	0.0	2/15/83						
15	104	2	1	1	1	4	58	89.5	81.8	83.1	74.3	75.8	0	240	0.0	2/15/83						
15	105	2	1	1	1	5	57	90.0	83.3	84.5	76.8	78.1	0	240	0.0	2/15/83						
15	106	2	1	1	1	2	59	87.1	79.0	80.8	72.0	74.2	0	0	0.0	2/15/83						
15	107	1	1	1	1	5	56	85.9	79.3	79.8	73.2	74.9	0	0	0.0	2/15/83						
15	108	2	1	1	1	2	57	85.7	79.7	80.1	74.5	75.4	0	0	0.0	2/15/83						
15	109	2	1	1	1	5	62	89.7	82.5	83.5	74.6	76.5	0	0	0.0	2/15/83						
15	110	2	1	1	1	5	51	86.5	79.6	80.6	73.3	74.8	0	0	0.0	2/15/83						
15	111	2	1	1	1	3	57	88.8	81.6	82.2	76.2	76.1	0	0	0.0	2/15/83						
15	112	2	1	1	1	3	61	89.1	82.2	82.8	75.0	76.4	0	0	0.0	2/15/83						
15	113	2	1	1	1	3	64	88.1	80.5	81.8	73.6	75.4	0	0	0.0	2/15/83						
15	114	2	1	1	1	5	60	91.4	84.4	86.6	77.7	79.6	0	0	0.0	2/15/83						
15	115	2	1	1	1	3	67	93.4	85.2	87.1	77.8	79.5	0	0	0.0	2/15/83						
15	116	0	1	1	1	2	51	87.3	79.1	80.9	73.4	75.5	0	0	0.0	2/15/83						
15	117	2	1	1	1	2	63	90.0	82.9	83.0	76.5	77.0	0	0	0.0	2/15/83						
15	118	2	1	1	1	5	62	94.5	87.2	88.1	80.0	81.4	0	0	0.0	2/15/83						
15	119	2	1	1	1	5	68	93.9	86.3	87.6	78.7	80.4	0	0	0.0	2/15/83						
15	120	2	1	1	1	5	54	89.9	83.1	83.9	76.4	76.9	0	0	0.0	2/15/83						
15	121	2	1	1	1	5	60	88.4	80.7	82.1	73.5	75.3	0	0	0.0	2/15/83						
15	122	2	1	1	1	3	60	91.8	83.8	84.7	77.5	77.6	0	0	0.0	2/15/83						
15	123	2	1	1	1	3	61	94.8	89.0	89.5	83.2	83.4	0	0	0.0	2/15/83						
15	124	2	1	1	1	2	50	85.4	79.4	79.2	71.0	73.6	0	0	0.0	2/15/83						
15	125	2	1	1	1	5	61	92.6	85.4	86.0	78.4	79.2	0	0	0.0	2/15/83						
15	126	2	1	1	1	5	57	88.1	80.9	82.1	73.3	74.9	0	0	0.0	2/15/83						
15	127	2	1	1	1	2	62	89.9	83.2	84.8	75.6	77.8	0	0	0.0	2/15/83						
15	128	2	1	1	1	3	64	93.4	87.3	87.5	80.2	80.8	0	0	0.0	2/15/83						
15	129	2	1	1	1	2	57	86.1	79.4	80.5	72.9	73.7	0	0	0.0	2/15/83						
15	130	2	1	1	1	2	56	85.0	78.4	78.8	71.9	72.8	0	0	0.0	2/15/83						
15	131	2	1	1	1	5	59	90.6	82.8	83.8	-1.0	-1.0	0	0	0.0	2/15/83						
15	132	2	1	1	1	4	58	86.8	79.9	80.8	72.6	74.1	0	0	0.0	2/15/83						
15	133	2	1	1	1	2	55	87.8	80.1	81.4	73.5	74.9	0	0	0.0	2/15/83						
15	134	2	1	1	1	5	55	87.8	79.9	81.6	73.2	74.1	0	0	0.0	2/15/83						
15	135	2	1	1	1	2	60	89.0	82.1	82.9	75.2	76.2	0	0	0.0	2/15/83						
15	136	2	1	1	1	5	59	88.9	81.8	82.9	74.4	76.1	0	0	0.0	2/15/83						
15	137	2	1	1	1	5	55	88.6	83.3	85.3	75.8	78.1	0	0	0.0	2/15/83						
15	138	2	1	1	1	4	63	90.1	82.8	84.5	76.1	77.4	0	0	0.0	2/15/83						
15	139	2	1	1	1	5	47	89.0	81.0	82.5	74.4	75.5	0	0	0.0	2/15/83						
15	140	2	1	1	1	5	61	92.9	85.9	87.0	78.1	79.9	0	0	0.0	2/15/83						

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	V	DATE	
	QUAL.		(1)	(2)	(3)	(4)	(5)	IN	WE			
SITE	EN	TYPE	5	5	10	5	10	NG	IC			
			DBA					DL	NT			
								E	DO			
									R			
15	141	0 0 1 1	2 54	82.6	75.6	76.5	70.6	71.6	0	0	0.0	2/15/83
15	142	0 1 1 1	2 59	87.0	79.1	80.5	73.0	74.5	0	0	0.0	2/15/83
15	143	2 1 1 1	5 50	92.8	85.5	86.2	78.7	79.4	0	0	0.0	2/15/83
15	144	2 1 1 1	5 61	93.1	86.0	87.1	78.5	80.0	0	0	0.0	2/15/83
15	145	0 1 1 1	2 39	86.1	79.2	80.1	72.3	74.2	0	0	0.0	2/15/83
15	146	2 1 1 1	2 64	89.3	81.4	83.1	74.1	75.4	0	0	0.0	2/15/83
15	147	2 1 1 1	2 55	85.9	79.0	79.0	72.3	73.1	0	0	0.0	2/15/83
15	148	2 1 1 1	5 62	91.4	84.2	85.2	77.8	78.6	0	0	0.0	2/15/83
15	149	1 1 1 1	3 52	84.8	78.8	79.3	73.1	74.4	0	0	0.0	2/15/83
15	150	2 1 1 1	2 62	91.3	84.7	84.8	76.2	78.2	0	0	0.0	2/15/83
15	151	2 1 1 1	2 65	89.6	82.6	83.5	75.3	77.5	3	30	3.9	2/15/83
15	152	2 1 1 1	3 57	89.5	82.3	83.2	75.6	76.4	3	30	3.9	2/15/83
15	153	2 1 1 1	5 62	90.4	82.5	-1.0	-1.0	-1.0	3	30	3.9	2/15/83
15	154	0 1 1 1	2 56	86.2	79.7	80.2	74.1	74.9	3	30	3.9	2/15/83
15	155	2 1 1 1	4 58	89.7	82.1	83.5	74.9	76.3	3	30	3.9	2/15/83
15	156	2 1 1 1	5 61	91.3	84.8	85.5	78.3	-1.0	3	30	3.9	2/15/83
15	157	2 1 1 1	4 60	89.7	82.6	83.6	75.9	76.5	3	30	3.9	2/15/83
15	158	2 1 1 1	2 59	86.5	79.8	80.3	73.0	71.1	3	30	3.9	2/15/83
15	159	2 1 1 1	2 57	87.4	80.9	81.2	74.7	76.2	3	30	3.9	2/15/83
15	160	2 1 1 1	5 56	86.6	79.5	-1.0	70.3	70.0	3	30	3.9	2/15/83
15	161	2 1 1 1	2 62	88.6	81.5	81.7	74.5	74.8	3	30	3.9	2/15/83
15	162	2 1 1 1	5 59	89.6	82.0	83.4	75.2	76.5	3	30	3.9	2/15/83
15	163	2 1 1 1	4 59	88.9	82.2	73.9	72.1	73.2	3	30	3.9	2/15/83
15	164	2 1 1 1	2 57	86.1	79.5	81.2	73.5	74.1	3	30	3.9	2/15/83
15	165	0 1 1 1	1 63	81.0	73.2	75.2	67.2	69.4	3	30	3.9	2/15/83
15	166	2 1 1 1	5 57	87.5	80.9	81.6	73.7	75.5	3	30	3.9	2/15/83
15	167	2 1 1 1	2 60	85.8	77.6	78.8	71.3	72.5	3	30	3.9	2/15/83
15	168	2 1 1 1	1 64	81.5	74.8	75.7	66.5	69.4	3	30	3.9	2/15/83
15	169	2 1 1 1	5 46	89.0	83.0	83.4	76.3	76.3	3	30	3.9	2/15/83
15	170	2 1 1 1	5 56	90.1	82.4	83.6	75.5	76.9	3	30	3.9	2/15/83
15	171	2 1 1 1	5 50	87.1	79.6	80.7	72.0	73.4	3	30	3.9	2/15/83
15	172	2 1 1 1	2 60	90.2	82.9	83.5	77.3	77.2	3	30	3.9	2/15/83
15	173	2 1 1 1	4 63	90.6	83.3	84.2	76.3	77.3	3	30	3.9	2/15/83
15	174	0 1 1 1	0 46	75.7	69.4	70.3	62.8	65.6	3	30	3.9	2/15/83
15	175	2 1 1 1	5 59	92.6	85.4	86.3	79.9	79.8	3	30	3.9	2/15/83
15	176	2 1 1 1	5 68	96.9	89.9	90.4	83.5	84.2	3	30	3.9	2/15/83
15	177	0 0 0 1	1 63	80.9	74.2	75.2	66.6	68.6	3	30	3.9	2/15/83
15	178	0 0 0 1	1 64	85.7	77.1	79.9	70.4	72.2	3	30	3.9	2/15/83
15	179	2 1 1 1	2 59	90.1	82.1	83.5	75.5	76.1	3	30	3.9	2/15/83
15	180	2 1 1 1	3 50	88.5	81.4	81.8	74.2	75.7	3	30	3.9	2/15/83
15	181	2 1 1 1	2 61	88.1	79.3	81.1	71.9	73.6	3	30	3.9	2/15/83
15	182	2 1 1 1	2 58	84.7	77.6	78.9	71.3	72.4	3	30	3.9	2/15/83
15	183	0 0 1 1	1 55	78.9	74.2	75.4	68.2	70.5	3	30	3.9	2/15/83
15	184	2 1 1 1	5 58	90.6	83.0	84.2	76.7	78.0	3	30	3.9	2/15/83
15	185	2 1 1 1	5 60	87.8	82.7	83.7	75.4	76.9	3	30	3.9	2/15/83
15	186	1 1 1 1	5 60	91.3	84.1	84.8	77.4	79.0	3	30	3.9	2/15/83
15	187	1 1 1 1	1 55	79.8	73.6	74.7	68.0	70.0	3	60	2.3	2/15/83
15	188	2 1 1 1	2 63	88.9	81.0	82.7	73.3	76.0	3	60	2.3	2/15/83
15	189	2 1 1 1	2 68	88.7	81.5	83.1	74.2	75.3	3	60	2.3	2/15/83
15	190	2 1 1 1	2 62	85.6	78.8	79.4	71.9	73.2	3	60	2.3	2/15/83
15	191	2 1 1 1	2 61	88.4	81.4	82.2	73.7	75.6	3	60	2.3	2/15/83
15	192	2 1 1 1	5 67	91.7	84.3	84.9	76.4	78.5	3	60	2.3	2/15/83
15	193	2 1 1 1	2 57	91.0	82.9	84.3	75.7	77.0	3	60	2.3	2/15/83
15	194	0 0 1 1	0 60	79.9	75.8	76.0	69.0	71.4	3	60	2.3	2/15/83
15	195	2 1 1 1	2 62	90.8	83.7	84.5	77.0	77.9	3	60	2.3	2/15/83
15	196	2 1 1 1	1 58	79.0	72.5	73.6	65.0	67.4	3	60	2.3	2/15/83
15	197	2 1 1 1	5 62	90.0	82.3	83.3	74.5	76.5	3	60	2.3	2/15/83
15	198	2 1 1 1	5 62	91.1	84.3	85.7	78.3	78.9	3	60	2.3	2/15/83
15	199	2 1 1 1	5 57	88.6	81.1	82.7	73.4	75.1	3	60	2.3	2/15/83
15	200	2 1 1 1	4 53	91.0	83.9	85.0	76.0	77.8	3	60	2.3	2/15/83
15	201	2 1 1 1	4 55	89.2	81.1	82.5	75.1	75.5	3	60	2.3	2/15/83
15	202	2 1 1 1	2 52	89.2	80.6	82.5	74.1	75.7	3	60	2.3	2/15/83
15	203	2 1 1 1	5 59	90.2	83.8	83.8	76.7	78.0	3	60	2.3	2/15/83
15	204	2 1 1 1	5 61	89.1	82.1	82.7	75.2	72.5	3	60	2.3	2/15/83
15	205	2 1 1 1	1 63	81.1	76.4	77.2	71.1	72.5	3	60	2.3	2/15/83
15	206	1 1 1 1	1 59	83.2	76.1	77.3	69.8	71.0	3	60	2.3	2/15/83
15	207	2 1 1 1	5 61	94.4	88.0	88.4	80.7	81.0	3	60	2.3	2/15/83
15	208	2 1 1 1	3 63	89.4	81.6	82.5	74.7	75.9	3	60	2.3	2/15/83
15	209	2 1 1 1	5 66	93.9	87.2	88.1	80.0	80.4	3	60	2.3	2/15/83
15	210	2 1 1 1	4 60	91.0	83.0	84.7	76.1	75.0	3	60	2.3	2/15/83



\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	V	DATE					
	QUAL.							IP	IN	WE						
S	E	T	(1)	(2)	(3)	(4)	(5)	NG	IC							
ITE	N	R	5	5	10	5	10	DL	NT							
	T	H	DBA					DE	DL	DO						
		L					D	E	R							
16	1	2	1	1	1	0	57	79.7	72.8	74.1	65.2	68.1	0	90	0.0	2/16/83
16	2	2	1	1	1	4	54	86.0	80.0	81.0	73.0	74.2	0	90	0.0	2/16/83
16	3	2	1	1	1	1	61	82.1	75.5	75.9	66.4	69.5	0	90	0.0	2/16/83
16	4	2	1	1	1	5	62	90.5	84.0	84.5	75.8	66.9	0	90	0.0	2/16/83
16	5	2	1	1	1	4	56	88.5	81.8	82.1	74.6	76.8	0	90	0.0	2/16/83
16	6	2	1	1	1	5	57	90.7	83.4	84.5	75.5	77.7	0	90	0.0	2/16/83
16	7	2	1	1	1	5	64	91.6	84.9	85.9	76.5	78.6	0	90	0.0	2/16/83
16	8	2	1	1	1	1	56	80.0	73.0	73.8	64.8	68.1	0	90	0.0	2/16/83
16	9	2	1	1	1	1	52	80.1	72.0	73.2	62.8	66.0	0	90	0.0	2/16/83
16	10	2	1	1	1	5	57	88.3	82.2	82.9	73.8	75.7	0	90	0.0	2/16/83
16	11	2	1	1	1	3	58	87.7	80.7	81.3	73.1	75.0	0	90	0.0	2/16/83
16	12	2	1	1	1	5	58	90.5	83.6	84.9	75.6	77.9	0	90	0.0	2/16/83
16	13	2	1	1	1	1	58	85.0	77.8	79.5	69.7	72.3	0	90	0.0	2/16/83
16	14	2	1	1	1	5	60	89.9	83.6	84.0	76.3	77.2	0	90	0.0	2/16/83
16	15	2	1	1	1	1	82	88.5	82.1	82.4	72.8	75.3	0	90	0.0	2/16/83
16	16	0	1	1	1	2	58	86.4	79.7	79.8	73.0	73.9	0	90	0.0	2/16/83
16	17	2	1	1	1	0	55	79.9	73.0	73.7	64.0	66.5	0	90	0.0	2/16/83
16	18	1	1	1	1	5	60	88.3	82.0	83.2	75.3	77.4	0	90	0.0	2/16/83
16	19	2	1	1	1	0	65	83.6	76.4	77.7	67.5	70.5	0	90	0.0	2/16/83
16	20	2	1	1	1	0	66	81.9	75.2	75.9	67.8	70.8	0	90	0.0	2/16/83
16	21	2	1	1	1	5	59	91.0	83.6	85.0	76.2	78.3	0	90	0.0	2/16/83
16	22	2	1	1	1	1	65	84.3	77.4	79.1	69.9	72.6	0	90	0.0	2/16/83
16	23	2	1	1	1	1	60	80.9	73.9	74.5	64.8	67.8	0	90	0.0	2/16/83
16	24	2	1	1	1	1	56	79.4	71.9	73.1	63.6	66.4	0	90	0.0	2/16/83
16	25	1	1	1	1	3	54	86.8	80.7	81.0	72.9	75.0	0	90	0.0	2/16/83
16	26	2	1	1	1	2	60	87.4	79.9	80.9	71.8	73.6	0	90	0.0	2/16/83
16	27	2	1	1	1	1	59	82.5	75.7	76.4	67.0	69.9	0	90	0.0	2/16/83
16	28	2	1	1	1	1	61	83.0	75.2	75.9	67.8	69.8	0	90	0.0	2/16/83
16	29	2	1	1	1	5	61	92.7	85.5	86.0	77.2	78.5	0	90	0.0	2/16/83
16	30	2	1	1	1	0	54	79.9	72.7	73.6	63.8	67.5	0	90	0.0	2/16/83
16	31	2	1	1	1	4	57	87.0	80.8	81.9	73.0	76.4	0	90	0.0	2/16/83
16	32	2	1	1	1	5	61	91.7	84.2	84.9	77.1	77.9	0	90	0.0	2/16/83
16	33	0	0	1	1	2	57	85.0	78.2	79.4	71.5	73.0	0	90	0.0	2/16/83
16	34	2	1	1	1	5	63	89.5	82.6	83.3	74.8	76.3	0	90	0.0	2/16/83
16	35	2	1	1	1	1	67	82.2	75.0	75.7	66.7	69.5	0	90	0.0	2/16/83
16	36	2	1	1	1	2	64	86.5	79.1	80.9	70.2	73.8	0	90	0.0	2/16/83
16	37	2	1	1	1	1	60	79.4	72.5	74.2	60.4	67.8	0	90	0.0	2/16/83
16	38	0	0	1	1	1	60	85.0	79.9	80.5	72.2	75.2	0	90	0.0	2/16/83
16	39	2	1	1	1	1	62	80.8	73.8	74.6	65.4	68.2	0	90	0.0	2/16/83
16	40	2	1	1	1	3	58	89.7	82.8	83.7	74.9	76.7	0	90	0.0	2/16/83
16	41	2	1	1	1	1	67	84.7	77.4	78.4	68.5	71.1	0	90	0.0	2/16/83
16	42	2	1	1	1	0	54	77.7	71.1	72.3	63.8	66.1	0	90	0.0	2/16/83
16	43	2	1	1	1	1	58	79.9	73.3	74.2	66.8	68.9	0	90	0.0	2/16/83
16	44	2	1	1	1	0	60	79.5	71.8	73.6	63.2	66.2	0	90	0.0	2/16/83
16	45	2	1	1	1	1	63	80.2	73.0	74.8	66.8	69.3	0	90	0.0	2/16/83
16	46	2	1	1	1	1	63	81.9	74.7	75.7	65.9	69.1	0	90	0.0	2/16/83
16	47	2	1	1	1	1	53	82.9	75.4	76.3	66.8	69.4	0	90	0.0	2/16/83
16	48	2	1	1	1	1	64	82.3	74.8	76.0	66.1	68.7	0	90	0.0	2/16/83
16	49	2	1	1	1	1	61	81.2	73.5	74.8	65.1	68.4	0	90	0.0	2/16/83
16	50	0	1	1	1	1	76	88.3	82.0	82.0	74.8	76.7	0	90	0.0	2/16/83
16	51	0	0	1	1	2	56	84.2	77.3	78.1	69.4	71.5	0	90	0.0	2/16/83
16	52	2	1	1	1	2	51	86.4	79.9	79.8	72.6	73.2	0	90	0.0	2/16/83
16	53	2	1	1	1	1	57	82.8	75.5	76.5	67.6	69.7	0	90	0.0	2/16/83
16	54	2	1	1	1	1	60	78.8	72.4	73.4	65.8	67.0	0	90	0.0	2/16/83
16	55	2	1	1	1	0	57	83.0	76.4	76.6	68.7	69.8	0	90	0.0	2/16/83
16	56	2	1	1	1	5	54	87.5	81.7	81.8	74.8	75.6	0	90	0.0	2/16/83
16	57	2	1	1	1	0	62	80.5	73.9	74.8	66.0	68.8	0	90	0.0	2/16/83
16	58	2	1	1	1	1	63	83.8	77.1	77.4	67.9	70.9	0	90	0.0	2/16/83
16	59	2	1	1	1	1	57	85.1	78.3	78.8	69.5	72.2	0	90	0.0	2/16/83
16	60	0	0	1	1	0	62	78.6	71.8	73.7	67.7	69.7	0	90	0.0	2/16/83
16	61	0	0	1	1	1	53	78.5	71.4	72.7	63.7	67.2	0	90	0.0	2/16/83
16	62	2	1	1	1	5	60	87.8	81.4	82.6	74.0	75.5	0	90	0.0	2/16/83
16	63	2	0	1	1	5	62	88.7	82.3	83.4	74.1	76.4	0	90	0.0	2/16/83
16	64	2	1	1	1	1	58	81.9	74.0	75.1	64.8	68.4	0	90	0.0	2/16/83
16	65	2	1	1	1	5	60	90.2	83.3	83.8	75.1	76.5	0	90	0.0	2/16/83
16	66	0	0	1	1	1	51	82.9	76.6	77.6	69.6	72.7	0	90	0.0	2/16/83
16	67	2	1	1	1	5	60	89.1	81.5	82.6	73.2	74.9	0	90	0.0	2/16/83
16	68	2	1	1	1	5	57	89.8	82.6	83.7	74.8	76.8	0	90	0.0	2/16/83
16	69	2	1	1	1	5	60	88.5	81.8	82.7	73.7	75.4	0	90	0.0	2/16/83
16	70	2	1	1	1	1	59	85.2	77.0	77.9	69.2	70.9	0	90	0.0	2/16/83





\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

S I T E	LOC.	EVENT			VEH		MIC					WS	WA	V	DATE			
		QUAL.	G	V	D	E	T	S	(1)	(2)	(3)					(4)	(5)	IP
		N	R	H	L	V	E	P	E	(1)	(2)	(3)	(4)	(5)	NE	NG	NT	DO
										5	5	10	5	10	DE	DL	DO	R
										DBA					D	E		
16	211	2	1	1	1	5	51	88.1	80.7	82.0	73.2	74.7	6	110	-3.1	2/16/83		
16	212	2	1	1	1	5	60	90.5	84.9	85.8	77.4	80.4	6	110	-3.1	2/16/83		
16	213	2	1	1	1	1	58	81.6	74.4	75.7	66.1	-1.0	6	110	-3.1	2/16/83		
16	214	2	1	1	1	5	60	90.2	83.5	84.3	75.9	77.3	6	110	-3.1	2/16/83		
16	215	2	1	1	1	1	46	78.2	70.5	72.8	62.4	-1.0	6	110	-3.1	2/16/83		
16	216	2	1	1	1	0	58	79.2	71.9	74.1	64.0	67.2	6	110	-3.1	2/16/83		
16	217	2	1	1	1	0	61	79.9	72.2	74.0	64.4	67.2	6	110	-3.1	2/16/83		
16	218	2	1	1	1	2	63	86.2	79.3	62.0	57.3	62.6	6	110	-3.1	2/16/83		
16	219	2	1	1	1	2	55	85.6	78.2	79.3	70.0	72.0	6	110	-3.1	2/16/83		
16	220	2	1	1	1	1	60	82.4	74.5	75.4	65.7	69.2	6	110	-3.1	2/16/83		
16	221	2	1	1	1	2	57	88.0	81.0	81.6	73.9	75.2	6	110	-3.1	2/16/83		
16	222	2	1	1	1	0	64	80.5	72.9	74.5	64.4	67.2	6	110	-3.1	2/16/83		
16	223	2	1	1	1	5	69	95.1	88.3	88.8	79.9	82.2	6	110	-3.1	2/16/83		
16	224	2	1	1	1	1	60	81.3	74.4	75.3	66.4	69.5	6	110	-3.1	2/16/83		
16	225	2	1	1	1	5	64	90.3	83.4	84.9	75.6	77.9	6	110	-3.1	2/16/83		
16	226	2	1	1	1	1	58	80.7	73.3	74.7	65.3	67.6	6	110	-3.1	2/16/83		
16	227	2	1	1	1	5	59	89.9	83.0	83.7	75.0	76.9	6	110	-3.1	2/16/83		
16	228	2	1	1	1	1	59	83.0	75.9	77.1	67.3	70.2	6	110	-3.1	2/16/83		
16	229	2	1	1	1	0	63	79.9	73.3	75.0	66.0	68.4	6	110	-3.1	2/16/83		
16	230	2	1	1	1	1	60	83.3	76.1	77.5	66.9	69.9	6	110	-3.1	2/16/83		
16	231	2	1	1	1	1	66	82.4	75.3	76.4	66.8	70.3	6	110	-3.1	2/16/83		
16	232	2	1	1	1	1	60	83.1	75.3	76.1	67.2	70.0	6	100	-1.6	2/16/83		
16	233	2	1	1	1	2	59	87.7	81.8	81.5	73.2	76.3	6	100	-1.6	2/16/83		
16	234	2	1	1	1	0	54	78.8	71.3	72.6	62.4	65.7	6	100	-1.6	2/16/83		
16	235	2	1	1	1	1	58	82.3	74.8	76.2	65.5	69.8	6	100	-1.6	2/16/83		
16	236	2	1	1	1	0	62	80.0	72.3	73.9	64.9	68.0	6	90	0.0	2/16/83		
16	237	2	1	1	1	1	60	80.9	74.1	75.5	65.2	68.3	6	90	0.0	2/16/83		
16	238	2	1	1	1	1	59	82.0	74.8	75.7	66.3	68.8	6	90	0.0	2/16/83		
16	239	2	1	1	1	1	54	80.2	73.6	74.7	65.2	67.8	6	90	0.0	2/16/83		
16	240	2	1	1	1	2	61	86.4	79.1	80.4	70.4	73.3	6	90	0.0	2/16/83		
16	241	2	1	1	1	5	55	89.9	82.9	83.3	75.6	76.8	6	90	0.0	2/16/83		
16	242	2	1	1	1	1	53	80.9	73.0	-1.0	64.0	65.1	6	90	0.0	2/16/83		
16	243	2	1	1	1	2	54	83.5	76.6	77.5	68.4	71.3	6	90	0.0	2/16/83		
16	244	2	1	1	1	5	62	91.4	84.6	86.2	76.0	78.7	6	90	0.0	2/16/83		
16	245	2	1	1	1	0	55	80.0	72.5	74.2	63.8	66.9	6	90	0.0	2/16/83		
16	246	2	1	1	1	1	62	82.5	75.4	76.2	67.8	71.0	6	90	0.0	2/16/83		
16	247	2	1	1	1	5	57	90.2	83.1	84.0	74.7	76.4	6	90	0.0	2/16/83		
16	248	2	1	1	1	1	52	85.6	77.8	78.6	68.6	71.0	6	90	0.0	2/16/83		
16	249	2	1	1	1	1	59	91.9	84.3	85.8	75.2	77.6	6	90	0.0	2/16/83		
16	250	2	1	1	1	1	57	80.7	73.2	74.5	64.3	67.6	6	90	0.0	2/16/83		
16	251	2	1	1	1	1	62	82.3	74.5	75.6	66.0	68.9	6	90	0.0	2/16/83		
16	252	2	1	1	1	1	68	83.5	75.8	77.2	68.3	70.3	6	90	0.0	2/16/83		
16	253	2	1	1	1	5	63	94.4	86.7	88.5	79.6	80.0	6	90	0.0	2/16/83		
16	254	2	1	1	1	2	55	84.1	76.7	77.6	69.0	70.9	6	90	0.0	2/16/83		
16	255	2	1	1	1	5	61	91.9	84.4	86.0	77.2	79.0	6	90	0.0	2/16/83		
16	256	2	1	1	1	0	51	77.7	70.9	-1.0	-1.0	-1.0	6	90	0.0	2/16/83		
16	257	2	1	1	1	0	62	81.5	74.0	-1.0	-1.0	-1.0	6	90	0.0	2/16/83		
16	258	2	1	1	1	1	57	78.8	71.3	73.0	62.3	65.7	6	90	0.0	2/16/83		
16	259	2	1	1	1	0	52	79.5	72.4	73.4	64.5	67.8	6	90	0.0	2/16/83		
16	260	2	1	1	1	2	53	86.2	79.2	79.8	72.1	73.3	6	90	0.0	2/16/83		
16	261	2	1	1	1	1	60	-1.0	76.0	-1.0	-1.0	-1.0	6	90	0.0	2/16/83		
16	262	2	1	1	1	1	65	85.0	76.8	79.0	67.0	70.7	6	90	0.0	2/16/83		
16	263	2	1	1	1	5	60	89.9	84.3	85.0	78.2	79.0	6	90	0.0	2/16/83		
16	264	2	1	1	1	4	63	89.8	83.2	83.5	75.6	77.2	6	90	0.0	2/16/83		
16	265	2	1	1	1	1	48	78.0	70.9	71.5	62.6	65.5	6	90	0.0	2/16/83		
16	266	2	1	1	1	0	60	82.2	74.5	75.6	67.1	68.0	6	90	0.0	2/16/83		
16	267	0	0	0	1	1	44	76.7	70.9	72.2	65.0	67.5	6	90	0.0	2/16/83		
16	268	2	1	1	1	0	53	79.6	72.3	73.3	63.4	66.9	6	90	0.0	2/16/83		
16	269	2	1	1	1	5	53	87.4	80.6	81.3	73.3	74.7	6	90	0.0	2/16/83		
16	270	2	1	1	1	1	58	80.2	72.4	74.0	64.1	67.0	6	90	0.0	2/16/83		
16	271	2	0	0	1	1	56	80.7	74.2	74.8	65.3	68.5	6	90	0.0	2/16/83		
16	272	2	1	1	1	5	58	89.2	81.4	82.6	73.8	75.6	6	90	0.0	2/16/83		
16	273	2	1	1	1	0	51	78.9	72.0	73.3	63.4	66.7	6	90	0.0	2/16/83		
16	274	2	1	1	1	0	53	77.7	70.1	72.0	63.9	65.4	6	90	0.0	2/16/83		
16	275	2	1	1	1	1	61	81.7	74.2	63.8	60.4	66.1	6	90	0.0	2/16/83		
16	276	2	1	1	1	1	65	81.1	73.6	75.7	65.7	68.5	6	90	0.0	2/16/83		

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH	MIC	WS	WA	V	DATE									
S	E	G	D	(1)	(2)	(3)	(4)	(5)	NE	NG	IC	DO				
ITE	N	V	E	5	5	10	5	10	DE	DL	DL	DO				
	R	H	L			DBA			D	E	R					
17	1	2	1	1	0	54	79.1	72.2	72.5	66.2	66.5	0	45	0.0	2/17/83	
17	2	2	1	1	1	60	80.1	73.7	74.4	68.5	68.2	0	45	0.0	2/17/83	
17	3	2	1	1	1	0	52	74.0	67.6	68.4	61.3	62.2	0	45	0.0	2/17/83
17	4	2	1	1	1	5	62	88.0	82.0	82.9	75.9	76.2	0	45	0.0	2/17/83
17	5	2	1	1	1	5	62	89.1	83.4	83.4	77.3	77.7	0	90	0.0	2/17/83
17	6	2	1	1	1	0	57	79.6	73.2	73.9	66.2	67.1	0	90	0.0	2/17/83
17	7	2	1	1	1	1	60	80.6	74.5	75.4	67.6	68.3	0	90	0.0	2/17/83
17	8	2	1	1	1	0	53	74.2	67.8	68.4	61.1	62.0	0	90	0.0	2/17/83
17	9	2	1	1	1	1	55	-1.0	70.0	-1.0	-1.0	-1.0	0	90	0.0	2/17/83
17	10	2	1	1	1	1	64	78.1	71.2	72.5	65.0	65.5	0	90	0.0	2/17/83
17	11	2	1	1	1	0	65	82.8	76.0	76.8	69.6	70.3	0	230	0.0	2/17/83
17	12	2	1	1	1	1	64	80.2	73.3	74.2	67.3	67.5	0	230	0.0	2/17/83
17	13	2	1	1	1	0	60	77.5	71.4	72.1	64.7	75.3	0	230	0.0	2/17/83
17	14	2	1	1	1	0	72	81.8	75.4	76.3	69.0	69.9	0	230	0.0	2/17/83
17	15	2	1	1	1	1	61	85.3	79.0	79.6	73.1	73.1	0	230	0.0	2/17/83
17	16	2	1	1	1	1	59	79.8	73.6	74.0	66.9	66.9	0	230	0.0	2/17/83
17	17	2	1	1	1	0	62	77.7	71.0	71.7	64.7	65.6	0	230	0.0	2/17/83
17	18	2	1	1	1	7	66	-1.0	76.0	-1.0	-1.0	-1.0	0	230	0.0	2/17/83
17	19	2	1	1	1	7	62	-1.0	74.0	-1.0	-1.0	-1.0	0	230	0.0	2/17/83
17	20	2	1	1	1	7	65	82.1	76.5	76.7	70.3	70.9	0	230	0.0	2/17/83
17	21	2	1	1	1	0	59	76.9	70.3	71.6	63.4	64.8	0	230	0.0	2/17/83
17	22	2	1	1	1	1	59	76.7	70.0	70.3	63.4	64.0	0	230	0.0	2/17/83
17	23	2	1	1	1	0	57	77.6	70.9	71.6	63.8	65.3	0	230	0.0	2/17/83
17	24	2	1	1	1	1	70	82.3	75.9	76.4	69.4	70.0	0	230	0.0	2/17/83
17	25	2	1	1	1	5	58	85.6	79.3	80.1	73.1	73.2	0	230	0.0	2/17/83
17	26	2	1	1	1	1	62	79.9	73.4	73.9	67.0	67.3	0	270	0.0	2/17/83
17	27	2	1	1	1	0	64	81.0	75.1	75.7	67.6	69.1	0	270	0.0	2/17/83
17	28	2	1	1	1	2	57	86.4	80.2	79.9	74.8	74.1	0	270	0.0	2/17/83
17	29	2	1	1	1	5	55	-1.0	79.0	-1.0	-1.0	-1.0	0	270	0.0	2/17/83
17	30	2	1	1	1	0	53	73.7	67.8	69.3	63.8	66.5	0	270	0.0	2/17/83
17	31	2	1	1	1	0	51	73.8	67.4	68.6	60.5	62.1	0	270	0.0	2/17/83
17	32	2	1	1	1	1	70	78.6	72.3	73.1	66.3	66.3	0	270	0.0	2/17/83
17	33	2	1	1	1	1	55	79.8	73.4	73.8	66.6	67.4	0	270	0.0	2/17/83
17	34	2	1	1	1	1	55	77.8	71.1	71.9	65.0	65.6	0	270	0.0	2/17/83
17	35	2	1	1	1	2	58	83.6	77.9	78.6	71.2	71.6	0	270	0.0	2/17/83
17	36	2	1	1	1	3	60	90.1	83.6	84.4	76.5	77.4	0	270	0.0	2/17/83
17	37	2	1	1	1	1	68	78.9	72.9	73.5	65.9	67.3	0	270	0.0	2/17/83
17	38	2	1	1	1	0	59	77.6	71.0	71.8	63.9	64.7	0	270	0.0	2/17/83
17	39	2	1	1	1	5	64	91.6	85.5	85.7	-1.0	-1.0	0	270	0.0	2/17/83
17	40	2	1	1	1	5	65	88.6	83.1	83.3	76.4	76.6	0	270	0.0	2/17/83
17	41	2	1	1	1	1	69	83.0	76.3	77.6	69.4	70.3	0	270	0.0	2/17/83
17	42	2	1	1	1	5	56	92.0	87.2	86.5	81.8	81.7	0	270	0.0	2/17/83
17	43	2	1	1	1	5	56	86.4	80.0	80.5	73.5	73.9	0	270	0.0	2/17/83
17	44	2	1	1	1	0	64	78.9	73.1	74.0	65.1	67.0	0	270	0.0	2/17/83
17	45	2	1	1	1	0	54	74.8	68.0	69.2	61.6	62.0	0	270	0.0	2/17/83
17	46	2	1	1	1	1	64	79.0	72.3	73.6	66.4	66.9	0	270	0.0	2/17/83
17	47	2	1	1	1	1	68	80.8	74.3	75.5	68.0	68.4	0	270	0.0	2/17/83
17	48	2	1	1	1	5	63	88.6	82.7	82.9	77.0	76.8	0	270	0.0	2/17/83
17	49	2	1	1	1	5	55	87.0	82.3	81.8	76.1	75.9	0	270	0.0	2/17/83
17	50	2	1	1	1	5	50	85.4	79.3	80.0	72.3	72.4	0	270	0.0	2/17/83
17	51	2	1	1	1	1	58	80.1	74.2	74.9	68.0	67.6	0	270	0.0	2/17/83
17	52	2	1	1	1	2	51	81.9	75.0	75.9	68.6	68.6	0	270	0.0	2/17/83
17	53	2	1	1	1	5	67	90.4	84.4	85.0	77.9	78.5	0	270	0.0	2/17/83
17	54	2	1	1	1	1	60	81.5	74.8	75.4	68.6	68.4	0	270	0.0	2/17/83
17	55	2	1	1	1	1	64	79.1	72.1	73.5	66.5	67.2	0	270	0.0	2/17/83
17	56	2	1	1	1	2	55	-1.0	74.0	-1.0	-1.0	-1.0	0	270	0.0	2/17/83
17	57	2	1	1	1	1	54	76.5	69.6	70.8	63.9	64.2	0	270	0.0	2/17/83
17	58	2	1	1	1	1	61	79.3	73.0	74.0	66.7	67.1	0	270	0.0	2/17/83
17	59	2	1	1	1	0	60	75.6	69.2	69.8	63.4	63.6	0	270	0.0	2/17/83
17	60	2	1	1	1	1	58	77.1	70.7	71.4	64.8	65.0	0	270	0.0	2/17/83
17	61	2	1	1	1	1	64	80.8	74.6	75.0	67.6	68.3	0	270	0.0	2/17/83
17	62	2	1	1	1	1	54	80.9	74.6	74.8	67.4	68.2	0	270	0.0	2/17/83
17	63	2	1	1	1	5	63	89.1	83.7	84.0	78.3	78.5	0	270	0.0	2/17/83
17	64	2	1	1	1	1	74	83.4	76.6	77.7	69.9	71.3	0	90	0.0	2/17/83
17	65	2	1	1	1	1	67	80.2	73.6	74.4	66.6	67.6	0	90	0.0	2/17/83
17	66	2	1	1	1	5	52	86.5	80.5	81.0	74.5	74.9	0	90	0.0	2/17/83
17	67	2	1	1	1	0	59	77.4	70.9	72.0	64.2	64.9	0	90	0.0	2/17/83
17	68	2	1	1	1	1	59	78.7	72.5	73.1	66.7	66.8	0	90	0.0	2/17/83
17	69	2	1	1	1	5	58	87.0	81.3	82.1	75.1	75.0	0	90	0.0	2/17/83
17	70	0	0	1	1	1	60	82.0	77.5	78.7	70.9	73.0	0	90	0.0	2/17/83

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT QUAL.	VEH TYPE	MIC	WS	WA	VE	DATE
SITE	EVENT	GVDE	(1) (2) (3) (4) (5)	IP	ING	IC	
		RLV	5 5 10 5 10	NE	DL	NT	
			DBA	DE	E	DO	
				D		R	
17 71	2 1 1 1	1 51	78.8 72.6 72.8 66.0 66.5	0	90	0.0	2/17/83
17 72	2 1 1 1	2 57	83.8 77.7 78.2 70.9 71.2	0	90	0.0	2/17/83
17 73	2 1 1 1	1 63	78.3 71.6 72.6 65.5 66.0	0	90	0.0	2/17/83
17 74	2 1 1 1	2 71	87.9 82.4 82.2 77.3 76.6	0	90	0.0	2/17/83
17 75	2 1 1 1	1 71	80.6 74.1 74.9 67.3 68.6	0	90	0.0	2/17/83
17 76	2 1 1 1	5 56	88.2 81.4 82.2 76.2 76.0	0	90	0.0	2/17/83
17 77	2 1 1 1	0 63	77.4 70.9 71.8 64.8 65.3	0	90	0.0	2/17/83
17 78	2 1 1 1	5 44	87.1 80.9 81.0 75.2 74.8	0	90	0.0	2/17/83
17 79	2 1 1 1	0 62	77.0 71.0 71.2 63.8 64.6	0	90	0.0	2/17/83
17 80	2 1 1 1	5 54	84.4 79.0 79.4 72.2 72.4	0	90	0.0	2/17/83
17 81	2 1 1 1	5 52	85.8 80.2 79.8 74.2 74.0	0	90	0.0	2/17/83
17 82	0 0 1 1	2 56	80.1 73.9 75.2 67.0 67.9	0	90	0.0	2/17/83
17 83	2 1 1 1	5 56	86.2 80.4 81.5 73.9 74.1	0	90	0.0	2/17/83
17 84	2 1 1 1	5 52	83.5 77.5 78.7 72.4 72.7	0	90	0.0	2/17/83
17 85	2 1 1 1	5 56	85.1 79.3 79.5 73.0 73.3	0	90	0.0	2/17/83
17 86	2 1 1 1	5 61	87.5 81.5 81.7 75.1 75.4	0	90	0.0	2/17/83
17 87	2 1 1 1	1 63	79.3 73.0 60.1 58.0 65.5	0	90	0.0	2/17/83
17 88	2 1 1 1	5 65	-1.0 86.0 -1.0 -1.0 -1.0	0	90	0.0	2/17/83
17 89	0 0 1 1	0 65	80.4 74.0 75.4 68.3 70.1	0	90	0.0	2/17/83
17 90	2 1 1 1	0 64	78.3 72.3 73.6 66.5 67.1	0	90	0.0	2/17/83
17 91	2 1 1 1	1 60	78.8 72.2 73.2 65.8 66.8	0	90	0.0	2/17/83
17 92	2 1 1 1	0 62	79.2 74.1 75.0 67.8 68.6	0	90	0.0	2/17/83
17 93	2 1 1 1	1 66	80.7 74.1 75.0 67.8 68.6	0	90	0.0	2/17/83
17 94	2 1 1 1	1 55	79.0 72.1 73.2 65.8 66.4	0	90	0.0	2/17/83
17 95	2 1 1 1	2 58	83.3 76.9 77.5 71.0 71.3	0	90	0.0	2/17/83
17 96	2 1 1 1	0 66	-1.0 72.0 -1.0 -1.0 -1.0	0	90	0.0	2/17/83
17 97	2 1 1 1	1 68	79.4 73.0 73.8 67.5 68.3	0	90	0.0	2/17/83
17 98	2 1 1 1	0 66	78.4 72.0 72.7 65.1 65.5	0	90	0.0	2/17/83
17 99	2 1 1 1	1 58	77.6 71.1 71.3 65.0 64.8	0	90	0.0	2/17/83
17 100	2 1 1 1	0 58	-1.0 68.0 -1.0 -1.0 -1.0	0	90	0.0	2/17/83
17 101	2 1 1 1	5 54	-1.0 79.0 -1.0 -1.0 -1.0	0	90	0.0	2/17/83
17 102	2 1 1 1	1 54	77.5 71.2 72.5 64.6 66.6	0	90	0.0	2/17/83
17 103	2 1 1 1	5 59	84.7 79.0 79.8 73.5 73.6	0	90	0.0	2/17/83
17 104	2 1 1 1	5 61	88.1 82.1 82.8 75.7 75.9	0	90	0.0	2/17/83
17 105	2 1 1 1	1 64	81.3 74.6 75.3 68.2 68.7	0	90	0.0	2/17/83
17 106	2 1 1 1	2 57	83.9 77.8 77.9 71.8 71.8	0	90	0.0	2/17/83
17 107	2 1 1 1	1 59	80.9 74.4 75.2 68.9 68.8	0	90	0.0	2/17/83
17 108	2 1 1 1	0 63	76.1 69.7 70.6 63.1 63.9	0	90	0.0	2/17/83
17 109	2 1 1 1	5 60	91.3 85.9 85.9 79.6 80.2	0	90	0.0	2/17/83
17 110	2 1 1 1	3 61	88.6 82.8 82.7 77.2 77.0	0	90	0.0	2/17/83
17 111	2 1 1 1	1 56	79.2 72.8 73.9 66.3 66.9	0	90	0.0	2/17/83
17 112	2 1 1 1	5 59	89.7 84.4 84.2 77.7 77.9	0	90	0.0	2/17/83
17 113	2 1 1 1	5 55	89.1 83.2 83.8 77.7 77.7	0	90	0.0	2/17/83
17 114	2 1 1 1	3 65	70.7 69.5 71.0 67.2 69.2	0	90	0.0	2/17/83
17 115	2 1 1 1	0 62	80.4 73.7 75.1 67.2 69.2	0	90	0.0	2/17/83
17 116	2 1 1 1	0 70	79.9 73.6 74.2 66.7 68.0	0	90	0.0	2/17/83
17 117	2 1 1 1	1 57	81.5 75.2 75.9 69.5 70.1	0	90	0.0	2/17/83
17 118	2 1 1 1	1 57	76.2 69.8 70.6 64.2 65.1	0	90	0.0	2/17/83
17 119	2 1 1 1	1 57	78.2 71.7 72.7 65.3 65.9	0	90	0.0	2/17/83
17 120	2 1 1 1	5 62	89.6 83.6 84.2 77.2 77.4	0	90	0.0	2/17/83
17 121	2 1 1 1	1 59	77.0 70.9 71.4 64.7 64.7	0	90	0.0	2/17/83
17 122	2 1 1 1	1 38	77.0 70.7 71.2 63.9 64.9	0	90	0.0	2/17/83
17 123	2 1 1 1	0 58	77.8 71.7 71.9 64.6 65.6	0	90	0.0	2/17/83
17 124	2 1 1 1	2 64	90.2 85.1 84.7 78.4 78.1	0	90	0.0	2/17/83
17 125	2 1 1 1	5 70	72.1 67.0 69.2 63.3 65.2	0	90	0.0	2/17/83
17 126	2 1 1 1	0 59	81.5 75.0 75.7 68.9 70.0	0	90	0.0	2/17/83
17 127	2 1 1 1	0 56	76.7 70.0 71.3 63.5 64.2	0	90	0.0	2/17/83
17 128	2 1 1 1	1 63	76.3 69.8 70.7 63.6 64.0	0	90	0.0	2/17/83
17 129	2 1 1 1	0 52	76.4 70.1 71.0 63.7 64.6	0	90	0.0	2/17/83
17 130	2 1 1 1	1 60	80.1 73.0 74.0 66.1 66.8	0	90	0.0	2/17/83
17 131	2 1 1 1	2 60	83.8 78.3 78.3 71.1 71.8	3	60	2.3	2/17/83
17 132	2 1 1 1	1 60	81.5 74.6 75.3 68.6 68.6	6	70	3.1	2/17/83
17 133	2 1 1 1	5 59	87.8 81.7 82.0 76.4 75.3	6	70	3.1	2/17/83
17 134	2 1 1 1	2 53	80.3 73.2 73.7 66.3 67.0	6	70	3.1	2/17/83
17 135	2 1 1 1	1 61	82.0 75.7 76.5 70.2 70.3	6	70	3.1	2/17/83
17 136	2 1 1 1	1 48	77.7 72.0 72.4 65.4 65.4	6	70	3.1	2/17/83
17 137	2 1 1 1	0 67	-1.0 72.0 -1.0 -1.0 -1.0	6	70	3.1	2/17/83
17 138	2 1 1 1	5 55	90.7 85.5 85.5 78.4 78.6	6	70	3.1	2/17/83
17 139	2 1 1 1	1 67	79.1 73.1 73.2 66.0 66.8	6	70	3.1	2/17/83
17 140	2 1 1 1	5 55	89.3 83.6 84.0 77.0 77.3	3	90	0.0	2/17/83

***** DATA SUMMARY *****														
LOC.	EVENT	VEH	MIC					WS	WA	V				
	QUAL.	T S						IP	IN	WE				
S	E	Y P	(1)	(2)	(3)	(4)	(5)	NE	NG	NT				
I	V	E E	5	5	10	5	10	DE	DL	DO				
T	N	R H L V	DBA					D	E	R	DATE			
E	T													
17	141	2 1 1 1	1 63	80.8	74.3	75.2	68.0	68.9	3	90	0.0	2/17/83		
17	142	2 1 1 1	2 60	90.0	84.4	84.6	78.5	78.7	3	90	0.0	2/17/83		
17	143	2 1 1 1	1 53	79.2	72.8	72.9	65.8	66.4	3	90	0.0	2/17/83		
17	144	2 1 1 1	1 63	80.3	73.1	73.8	67.6	67.9	3	90	0.0	2/17/83		
17	145	2 1 1 1	5 64	86.6	81.0	81.5	74.4	75.4	3	90	0.0	2/17/83		
17	146	2 1 1 1	0 64	83.1	76.9	78.1	71.6	71.3	3	90	0.0	2/17/83		
17	147	2 1 1 1	1 63	78.9	72.5	73.7	66.2	66.9	3	90	0.0	2/17/83		
17	148	2 1 1 1	2 53	80.4	73.7	74.8	67.7	68.0	3	90	0.0	2/17/83		
17	149	2 1 1 1	1 63	81.4	75.8	76.2	68.8	68.3	3	60	2.3	2/17/83		
17	150	2 1 1 1	1 61	83.7	77.5	78.2	71.1	71.2	0	20	0.0	2/17/83		
17	151	2 1 1 1	5 57	85.6	80.2	80.5	75.5	75.1	0	0	0.0	2/17/83		
17	152	2 1 1 1	2 55	79.1	72.6	73.4	66.4	66.7	0	0	0.0	2/17/83		
17	153	2 1 1 1	1 69	80.1	73.2	74.7	66.4	67.1	0	0	0.0	2/17/83		
17	154	2 1 1 1	1 71	81.8	75.6	76.3	68.8	69.4	0	0	0.0	2/17/83		
17	155	2 1 1 1	0 62	-1.0	70.0	-1.0	-1.0	-1.0	0	0	0.0	2/17/83		
17	156	2 1 1 1	1 64	79.1	72.2	73.4	65.5	66.2	0	0	0.0	2/17/83		
17	157	2 1 1 1	1 53	76.9	70.3	71.4	63.5	64.4	0	0	0.0	2/17/83		
17	158	2 1 1 1	1 62	-1.0	73.0	-1.0	-1.0	-1.0	0	0	0.0	2/17/83		
17	159	2 1 1 1	1 62	82.5	76.5	76.6	70.5	70.8	0	0	0.0	2/17/83		
17	160	2 1 1 1	5 62	-1.0	82.0	-1.0	-1.0	-1.0	0	0	0.0	2/17/83		
17	161	2 1 1 1	1 58	78.5	72.3	73.4	65.9	66.6	0	0	0.0	2/17/83		

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	V	DATE
SITE	QUAL.	T S	(1) (2) (3) (4) (5)	IP	IN	IC	
E	G V D E	Y P	(1) (2) (3) (4) (5)	NE	NG	NT	
T	R H L V	E E	5 5 10 5 10	DE	DL	DO	
		D	DBA	D	E	R	
18 1	2 1 1 1	5 29	87.5 81.5 81.7 0.0 0.0	3	30	3.9	8/30/83
18 2	2 1 1 1	0 34	73.5 67.5 67.6 0.0 0.0	3	30	3.9	8/30/83
18 3	0 0 1 1	2 35	78.6 73.6 73.6 0.0 0.0	3	30	3.9	8/30/83
18 4	2 1 1 1	3 34	83.3 76.4 77.1 0.0 0.0	3	30	3.9	8/30/83
18 5	0 0 1 1	5 35	82.9 77.9 78.4 0.0 0.0	3	30	3.9	8/30/83
18 6	2 1 1 1	1 38	73.2 68.0 67.8 0.0 0.0	3	60	2.3	8/30/83
18 7	2 1 1 1	1 35	74.7 68.7 68.6 0.0 0.0	3	60	2.3	8/30/83
18 8	2 1 1 1	1 28	69.8 64.6 64.3 0.0 0.0	3	60	2.3	8/30/83
18 9	2 1 1 1	2 32	81.5 75.2 75.4 0.0 0.0	3	60	2.3	8/30/83
18 10	2 1 1 1	5 31	83.1 76.6 77.3 0.0 0.0	3	60	2.3	8/30/83
18 11	2 1 1 1	5 29	84.7 78.1 78.9 0.0 0.0	6	60	4.5	8/30/83
18 12	2 1 1 1	5 26	90.1 83.0 83.3 0.0 0.0	6	60	4.5	8/30/83
18 13	2 1 1 1	5 35	81.9 76.1 76.8 0.0 0.0	3	60	2.3	8/30/83
18 14	2 1 1 1	5 31	86.9 80.5 81.8 0.0 0.0	3	60	2.3	8/30/83
18 15	2 1 1 1	3 33	78.9 73.6 73.6 0.0 0.0	3	60	2.3	8/30/83
18 16	2 1 1 1	4 35	84.6 79.1 79.3 0.0 0.0	3	60	2.3	8/30/83
18 17	2 1 1 1	5 30	82.6 78.3 78.6 0.0 0.0	3	60	2.3	8/30/83
18 18	2 1 1 1	3 34	81.5 75.8 76.4 0.0 0.0	3	60	2.3	8/30/83
18 19	2 1 1 1	5 38	87.8 82.4 82.1 0.0 0.0	3	60	2.3	8/30/83
18 20	2 1 1 1	3 36	80.6 74.7 74.8 0.0 0.0	6	60	4.5	8/30/83
18 21	2 1 1 1	3 28	88.5 82.0 82.2 0.0 0.0	6	60	4.5	8/30/83
18 22	2 1 1 1	2 33	76.2 70.3 70.0 0.0 0.0	6	60	4.5	8/30/83
18 23	2 1 1 1	6 33	87.4 82.1 82.2 0.0 0.0	6	60	4.5	8/30/83
18 24	2 1 1 1	3 39	90.2 84.2 84.7 0.0 0.0	0	60	0.0	8/30/83
18 25	2 1 1 1	2 41	83.7 77.6 77.6 0.0 0.0	0	60	0.0	8/30/83
18 26	2 1 1 1	5 21	84.7 78.4 78.6 0.0 0.0	0	60	0.0	8/30/83
18 27	2 1 1 1	5 38	84.4 78.9 78.6 0.0 0.0	0	60	0.0	8/30/83
18 28	2 1 1 1	3 28	83.3 76.9 77.3 0.0 0.0	0	60	0.0	8/30/83
18 29	2 1 1 1	3 31	79.3 74.2 74.1 0.0 0.0	0	60	0.0	8/30/83
18 30	2 1 1 1	5 30	88.0 82.8 83.4 0.0 0.0	0	60	0.0	8/30/83
18 31	2 1 1 1	5 35	87.6 82.3 82.9 0.0 0.0	0	60	0.0	8/30/83
18 32	2 1 1 1	4 31	87.1 81.0 81.2 0.0 0.0	0	60	0.0	8/30/83
18 33	2 1 1 1	5 31	82.2 77.0 77.0 0.0 0.0	0	60	0.0	8/30/83
18 34	2 1 1 1	2 32	78.1 72.4 72.5 0.0 0.0	6	70	3.1	8/30/83
18 35	2 1 1 1	2 27	83.7 76.5 77.3 0.0 0.0	6	70	3.1	8/30/83
18 36	2 1 1 1	5 29	85.1 79.1 79.4 0.0 0.0	6	70	3.1	8/30/83
18 37	2 1 1 1	3 32	77.5 71.7 71.8 0.0 0.0	6	70	3.1	8/30/83
18 38	2 1 1 1	5 34	82.7 76.4 76.8 0.0 0.0	6	70	3.1	8/30/83
18 39	2 1 1 1	5 28	80.6 74.7 74.9 0.0 0.0	0	60	0.0	8/30/83
18 40	2 1 1 1	5 32	86.1 79.5 80.0 0.0 0.0	0	60	0.0	8/30/83
18 41	2 1 1 1	3 41	84.7 79.0 79.1 0.0 0.0	0	60	0.0	8/30/83
18 42	2 1 1 1	5 27	92.4 85.3 85.8 0.0 0.0	0	270	0.0	8/30/83
18 43	2 1 1 1	5 33	85.5 78.4 78.7 0.0 0.0	0	270	0.0	8/30/83
18 44	2 1 1 1	3 36	91.8 85.2 85.5 0.0 0.0	0	270	0.0	8/30/83
18 45	2 1 1 1	5 31	84.6 78.4 79.3 0.0 0.0	0	270	0.0	8/30/83
18 46	2 1 1 1	5 37	86.8 79.7 80.8 0.0 0.0	0	270	0.0	8/30/83
18 47	2 1 1 1	3 36	83.2 76.6 77.4 0.0 0.0	0	270	0.0	8/30/83
18 48	2 1 1 1	4 39	87.1 81.2 81.7 0.0 0.0	3	60	2.3	8/30/83
18 49	2 1 1 1	5 38	86.2 80.3 80.5 0.0 0.0	3	60	2.3	8/30/83
18 50	2 1 1 1	5 30	83.7 77.6 77.7 0.0 0.0	3	60	2.3	8/30/83
18 51	2 1 1 1	3 37	84.8 78.0 78.7 0.0 0.0	3	60	2.3	8/30/83
18 52	2 1 1 1	5 35	84.9 79.2 79.7 0.0 0.0	3	60	2.3	8/30/83
18 53	2 1 1 1	3 35	83.5 77.0 77.7 0.0 0.0	3	60	2.3	8/30/83
18 54	2 1 1 1	2 36	84.4 78.8 78.5 0.0 0.0	3	60	2.3	8/30/83
18 55	2 1 1 1	3 36	77.3 72.5 72.2 0.0 0.0	3	60	2.3	8/30/83
18 56	2 1 1 1	5 32	85.7 79.0 79.3 0.0 0.0	3	60	2.3	8/30/83
18 57	2 1 1 1	5 35	81.9 75.9 76.2 0.0 0.0	3	60	2.3	8/30/83
18 58	2 1 1 1	5 39	87.9 80.9 83.4 0.0 0.0	3	60	2.3	8/30/83
18 59	2 1 1 1	2 30	77.8 74.5 74.2 0.0 0.0	3	50	2.9	8/30/83
18 60	0 0 1 1	1 38	73.9 69.6 70.0 0.0 0.0	3	50	2.9	8/30/83
18 61	2 1 1 1	5 31	84.2 77.7 78.6 0.0 0.0	3	50	2.9	8/30/83
18 62	2 1 1 1	3 30	82.1 76.4 76.8 0.0 0.0	6	60	4.5	8/30/83
18 63	2 1 1 1	4 34	86.5 80.6 82.3 0.0 0.0	6	60	4.5	8/30/83
18 64	2 1 1 1	3 32	79.8 74.6 75.0 0.0 0.0	6	60	4.5	8/30/83
18 65	2 1 1 1	2 35	81.3 75.7 75.6 0.0 0.0	6	60	4.5	8/30/83
18 66	2 1 1 1	2 36	80.7 75.1 75.5 0.0 0.0	6	60	4.5	8/30/83
18 67	2 1 1 1	3 30	81.7 76.0 76.9 0.0 0.0	6	60	4.5	8/30/83
18 68	2 1 1 1	1 37	76.0 71.9 70.8 0.0 0.0	3	60	2.3	8/30/83
18 69	2 1 1 1	5 34	83.8 77.9 78.4 0.0 0.0	3	60	2.3	8/30/83
18 70	2 1 1 1	3 29	78.8 72.1 72.5 0.0 0.0	3	60	2.3	8/30/83

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

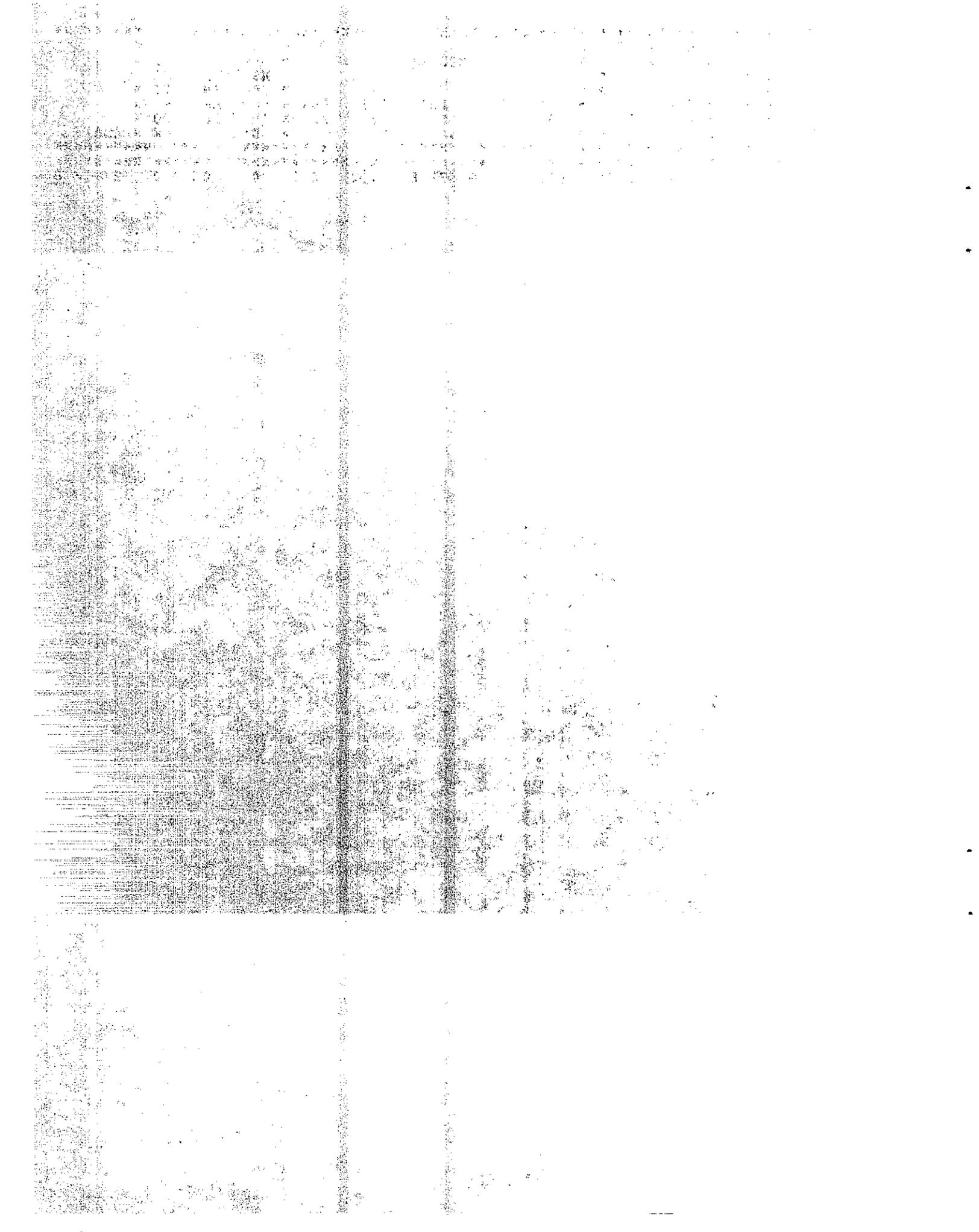
LOC.	* EVENT * * QUAL. *	* VEH * * TYPE *	* S * * P * * E * * E * * D *	(1) 5	(2) 5	(3) 10	(4) 5	(5) 10	WS IP NE DE D	WA IN NG DL E	V WE IC NT DO R	DATE	
S I T E	E V E N T	G V D E L E H L V	* * * * * * * * *			DBA							
18	71	2 1 1 1		5 22	80.0	77.7	78.4	0.0	0.0	3	60	2.3	8/30/83
18	72	0 0 1 1		5 27	81.4	75.8	76.1	0.0	0.0	3	60	2.3	8/30/83
18	73	0 0 1 1		2 32	78.9	74.3	74.5	0.0	0.0	3	60	2.3	8/30/83
18	74	0 0 1 1		3 22	83.4	76.2	77.3	0.0	0.0	3	60	2.3	8/30/83
18	75	0 0 1 1		3 34	84.8	78.9	79.0	0.0	0.0	3	60	2.3	8/30/83
18	76	0 0 1 1		5 30	83.5	77.3	77.4	0.0	0.0	3	60	2.3	8/30/83
18	77	0 0 1 1		3 29	85.2	79.8	78.8	0.0	0.0	3	60	2.3	8/30/83
18	78	0 0 1 1		2 36	83.9	77.5	78.0	0.0	0.0	3	60	2.3	8/30/83
18	79	0 0 1 1		0 0	83.0	76.6	77.0	0.0	0.0	3	60	2.3	8/30/83
18	80	2 1 1 1		3 30	84.3	78.0	78.3	0.0	0.0	3	60	2.3	8/30/83
18	81	0 0 1 1		4 31	77.9	72.3	73.2	0.0	0.0	3	60	2.3	8/30/83
18	82	2 1 1 1		3 40	-1.0	75.9	76.2	0.0	0.0	3	60	2.3	8/30/83
18	83	2 1 1 1		2 33	82.3	77.1	76.7	0.0	0.0	3	60	2.3	8/30/83
18	84	2 1 1 1		5 30	82.9	76.2	77.2	0.0	0.0	0	60	0.0	8/30/83
18	85	2 1 1 1		5 32	82.8	75.8	76.2	0.0	0.0	0	60	0.0	8/30/83
18	86	2 1 1 1		2 36	78.2	72.4	72.1	0.0	0.0	0	150	0.0	1/19/84
18	87	2 1 1 1		3 39	86.6	80.0	81.2	0.0	0.0	0	150	0.0	1/19/84
18	88	2 1 1 1		4 39	88.7	82.3	83.0	0.0	0.0	0	150	0.0	1/19/84
18	89	2 1 1 1		2 30	80.4	73.6	73.2	0.0	0.0	0	150	0.0	1/19/84
18	90	2 1 1 1		1 38	76.8	70.2	71.3	0.0	0.0	0	150	0.0	1/19/84
18	91	2 1 1 1		1 36	76.1	71.6	70.6	0.0	0.0	0	150	0.0	1/19/84
18	92	2 1 1 1		5 29	86.2	79.5	80.2	0.0	0.0	0	150	0.0	1/19/84
18	93	2 1 1 1		2 34	85.4	78.7	78.8	0.0	0.0	0	260	0.0	1/19/84
18	94	2 1 1 1		0 45	76.5	72.0	71.2	0.0	0.0	0	260	0.0	1/19/84
18	95	2 1 1 1		1 39	76.2	69.7	70.2	0.0	0.0	0	260	0.0	1/19/84
18	96	2 1 1 1		5 35	82.7	75.6	76.7	0.0	0.0	0	260	0.0	1/19/84
18	97	2 1 1 1		0 41	77.6	71.9	71.4	0.0	0.0	0	260	0.0	1/19/84
18	98	2 1 1 1		5 31	86.1	78.5	78.9	0.0	0.0	0	260	0.0	1/19/84
18	99	1 1 1 1		1 36	73.3	69.1	69.4	0.0	0.0	0	260	0.0	1/19/84
18	100	2 1 1 1		1 41	81.6	74.7	74.2	0.0	0.0	0	30	0.0	1/19/84
18	101	2 1 1 1		2 37	82.4	76.3	77.1	0.0	0.0	0	30	0.0	1/19/84
18	102	1 1 1 1		2 28	78.3	73.6	74.2	0.0	0.0	0	30	0.0	1/19/84
18	103	2 1 1 1		5 39	84.8	78.6	78.0	0.0	0.0	0	30	0.0	1/19/84
18	104	2 1 1 1		1 38	77.6	71.0	70.1	0.0	0.0	0	30	0.0	1/19/84
18	105	2 1 1 1		3 29	82.7	78.0	78.1	0.0	0.0	0	30	0.0	1/19/84
18	106	2 1 1 1		2 41	84.6	77.8	77.9	0.0	0.0	0	30	0.0	1/19/84
18	107	2 1 1 1		5 35	83.3	77.4	77.7	0.0	0.0	0	80	0.0	1/19/84
18	108	2 1 1 1		0 35	76.5	70.6	70.9	0.0	0.0	0	80	0.0	1/19/84
18	109	2 1 1 1		5 35	83.4	77.3	77.7	0.0	0.0	0	80	0.0	1/19/84
18	110	2 1 1 1		5 40	87.1	80.9	81.0	0.0	0.0	0	80	0.0	1/19/84
18	111	2 1 1 1		3 25	83.9	78.0	77.0	0.0	0.0	3	280	0.8	1/19/84
18	112	2 1 1 1		5 27	84.7	78.0	78.7	0.0	0.0	3	280	0.8	1/19/84
18	113	2 1 1 1		3 37	85.8	80.2	79.6	0.0	0.0	3	280	0.8	1/19/84
18	114	2 1 1 1		5 34	87.6	81.3	80.6	0.0	0.0	3	280	0.8	1/19/84
18	115	2 0 1 1		5 34	92.2	85.7	85.5	0.0	0.0	3	280	0.8	1/19/84
18	116	2 1 1 1		5 28	86.5	78.6	79.6	0.0	0.0	3	280	0.8	1/19/84
18	117	2 1 1 1		5 36	82.7	76.2	76.2	0.0	0.0	3	280	0.8	1/19/84
18	118	2 1 1 1		2 39	86.8	79.5	79.7	0.0	0.0	3	280	0.8	1/19/84
18	119	2 1 1 1		3 37	84.0	78.4	77.6	0.0	0.0	3	280	0.8	1/19/84
18	120	2 1 1 1		2 27	83.1	79.1	79.3	0.0	0.0	3	280	0.8	1/19/84
18	121	2 1 1 1		2 39	76.9	72.6	71.5	0.0	0.0	3	280	0.8	1/19/84
18	122	2 1 1 1		2 42	76.8	71.9	71.2	0.0	0.0	3	280	0.8	1/19/84
18	123	2 1 1 1		3 31	80.8	75.5	74.8	0.0	0.0	0	40	0.0	1/19/84
18	124	2 1 1 1		5 32	91.8	84.4	86.4	0.0	0.0	0	40	0.0	1/19/84
18	125	2 1 1 1		2 34	89.5	82.4	81.9	0.0	0.0	0	40	0.0	1/19/84
18	126	2 1 1 1		5 28	84.9	77.5	77.9	0.0	0.0	0	40	0.0	1/19/84
18	127	2 1 1 1		3 34	83.1	76.1	76.1	0.0	0.0	0	40	0.0	1/19/84
18	128	2 1 1 1		3 28	82.1	74.9	74.5	0.0	0.0	0	40	0.0	1/19/84
18	129	2 1 1 1		5 34	86.8	80.2	80.4	0.0	0.0	3	70	1.5	1/19/84
18	130	2 1 1 1		2 35	80.6	75.2	74.6	0.0	0.0	3	70	1.5	1/19/84
18	131	2 1 1 1		3 38	88.2	81.6	81.6	0.0	0.0	0	90	0.0	1/19/84
18	132	2 1 1 1		3 26	84.4	78.9	78.4	0.0	0.0	0	90	0.0	1/19/84
18	133	1 1 1 1		2 34	81.7	76.3	75.9	0.0	0.0	0	90	0.0	1/19/84
18	134	2 1 1 1		5 27	85.8	79.2	79.5	0.0	0.0	0	90	0.0	1/19/84
18	135	2 1 1 1		3 28	78.1	71.1	71.4	0.0	0.0	0	90	0.0	1/19/84

\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC	WS	WA	WE	DATE						
SITE	EVENT	TYPE	(1)	(2)	(3)	(4)	(5)	IP	IN	IC	DO	DATE	
	GRHLV	PEE	5	5	10	5	10	DE	NG	NT	DL	DL	DL
			DBA					D	E	R			
19	1	1 1 1 1	5 32	86.2	80.1	80.7	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	2	1 1 1 1	5 36	84.5	80.5	81.0	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	3	1 1 1 1	5 38	86.7	80.6	80.8	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	4	1 1 1 1	1 55	83.2	75.7	76.5	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	5	1 1 1 1	1 34	76.1	69.3	69.2	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	6	1 1 1 1	1 44	82.4	75.3	75.7	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	7	1 1 1 1	0 35	74.4	67.6	67.9	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	8	1 1 1 1	3 39	85.2	78.0	78.5	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	9	1 1 1 1	3 33	86.4	79.4	79.6	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	10	1 1 1 1	1 39	76.2	67.9	69.0	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	11	1 1 1 1	2 30	79.3	74.2	74.4	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	12	1 1 1 1	2 39	79.8	72.4	72.3	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	13	2 1 1 1	2 38	79.1	72.8	73.1	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	14	2 1 1 1	2 44	85.0	78.7	78.4	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	15	2 1 1 1	2 33	81.3	74.3	74.4	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	16	2 1 1 1	2 37	83.4	76.3	76.1	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	17	2 0 1 1	5 32	89.9	84.6	83.6	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	18	2 1 1 1	3 35	83.7	77.5	77.6	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	19	2 1 1 1	2 34	79.2	72.8	72.9	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	20	2 1 1 1	2 41	82.6	75.6	75.7	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	21	2 1 1 1	5 40	89.8	83.0	83.7	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	22	2 1 1 1	5 29	89.9	83.7	83.6	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	23	2 1 1 1	3 37	86.3	78.9	78.5	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	24	2 1 1 1	3 43	87.0	80.5	80.6	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	25	2 1 1 1	2 33	86.7	79.4	79.4	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	26	2 1 1 1	3 39	92.5	86.5	85.7	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	27	2 1 1 1	5 33	88.6	82.1	82.2	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	28	2 1 1 1	5 40	91.9	83.5	84.5	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	29	2 1 1 1	2 42	84.2	77.6	77.8	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	30	2 1 1 1	2 46	84.6	78.4	78.5	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	31	2 1 1 1	3 35	83.3	76.6	76.5	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	32	2 1 1 1	2 46	85.8	78.1	78.1	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	33	2 1 1 1	3 45	86.7	80.3	80.0	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	34	2 1 1 1	2 41	82.4	75.4	75.8	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	35	2 1 1 1	3 39	84.3	77.8	77.7	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	36	2 1 1 1	3 43	86.6	80.1	80.2	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	37	2 1 1 1	3 35	88.5	81.5	81.6	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	38	2 1 1 1	2 39	88.5	81.0	81.2	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	39	2 1 1 1	3 50	88.7	82.5	82.3	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	40	2 1 1 1	2 31	85.0	78.8	79.0	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	41	2 1 1 1	2 46	83.0	64.0	66.0	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	42	2 1 1 1	2 47	83.0	76.4	76.7	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	43	2 1 1 1	3 46	87.9	81.6	81.2	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	44	1 1 1 1	5 31	86.2	80.3	81.6	0.0	0.0	3	270	0.0	2/ 1/ 8	
19	45	2 1 1 1	1 42	79.3	70.6	70.5	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	46	2 1 1 1	1 49	79.1	71.2	72.2	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	47	2 1 1 1	5 36	88.5	82.0	82.1	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	48	2 0 1 1	3 41	88.7	81.5	81.9	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	49	2 1 1 1	2 40	87.8	81.0	81.0	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	50	2 1 1 1	1 45	79.2	72.6	73.5	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	51	2 0 1 1	5 37	87.2	80.9	80.9	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	52	2 1 1 1	5 31	87.4	80.5	82.2	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	53	2 1 1 1	3 34	85.1	78.4	79.0	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	54	2 1 1 1	3 45	88.8	82.3	82.3	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	55	2 1 1 1	3 35	87.9	82.3	80.9	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	56	2 1 1 1	3 31	85.0	77.1	77.6	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	57	2 1 1 1	5 36	90.5	83.1	83.7	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	58	2 1 1 1	5 40	85.9	79.2	79.4	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	59	2 1 1 1	3 38	87.8	80.7	81.9	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	60	2 1 1 1	2 39	81.8	75.4	76.3	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	61	2 1 1 1	5 45	87.3	80.0	80.9	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	62	2 1 1 1	5 25	81.5	75.4	75.7	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	63	2 1 1 1	5 33	87.7	82.8	83.2	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	64	2 1 1 1	3 36	87.2	78.5	79.1	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	65	2 1 1 1	3 28	83.2	75.5	76.2	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	66	2 1 1 1	2 30	76.8	69.9	70.2	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	67	2 1 1 1	2 34	83.4	74.5	75.6	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	68	2 1 1 1	3 35	84.5	77.9	78.4	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	69	2 1 1 1	2 45	84.0	76.3	77.1	0.0	0.0	0	0	0.0	2/ 1/ 8	
19	70	2 1 1 1	3 37	89.1	81.5	81.9	0.0	0.0	0	0	0.0	2/ 1/ 8	

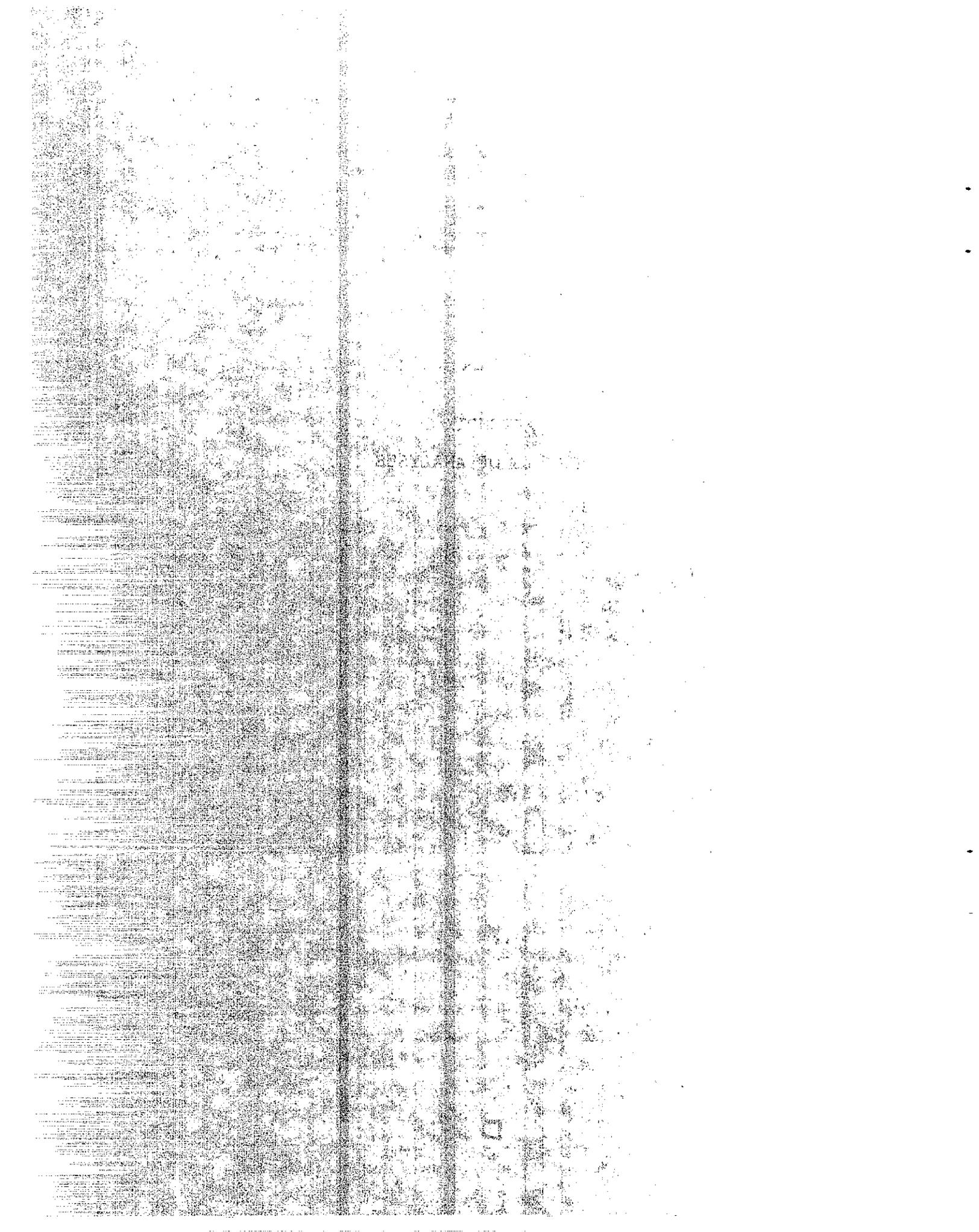
\*\*\*\*\* DATA SUMMARY \*\*\*\*\*

LOC.	EVENT	VEH	MIC					WS	WA	V	
	QUAL.	T S	(1)	(2)	(3)	(4)	(5)	IP	IN	IC	
S	E	Y P	5	5	10	5	10	NE	NG	NT	
I	N	E	5	5	10	5	10	DE	DL	DO	
T	E	R H L V	DBA					D	E	R	DATE
E	T										
19	71	2 1 1 1	3 30	84.1	77.4	77.8	0.0	0.0	0	0 0.0	2/ 1/ 8



APPENDIX D  
RESULTS OF ANALYSES

D



\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-com 15:01:29 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
$L0 = A + B \cdot \text{LOG}(\text{MPH})$	A = 14.13	5.27	7.73	7.86	20.06
	B = 36.36	37.79	36.90	32.38	26.61
NUMBER OF OBSERVATIONS	415	425	417	191	190
STD. ERROR OF Y ON LOG(X)	2.32	2.52	2.36	2.76	2.55
INDEX OF DETERMINATION	0.63	0.61	0.63	0.39	0.34
COEFF. OF CORRELATION	0.79	0.78	0.79	0.63	0.58
F RATIO	694.94	656.98	702.69	121.55	96.01
L0 :					
MEAN	76.60	70.23	71.12	63.99	66.19
VARIANCE	14.46	16.14	14.95	12.45	9.74
STD. DEV.	3.80	4.02	3.87	3.53	3.12
L0E :					
$A + 0.115 \cdot S0^2$	14.75	6.00	8.37	8.74	20.80

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-com 15:01:29 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
SPEED CLASS DATA					
CLASS 0 ( <25 )					
NUMBER OF POINTS	2	2	2	0	0
MIN. PTS. REQUIRED	7595	7285	6110	0	0
MEAN MPH	24.00	24.00	24.00	0.00	0.00
MEAN ENERGY (DBA)	68.23	61.85	62.24	0.00	0.00
MEAN DBA	65.95	59.65	60.35	0.00	0.00
STD. DEV. MEAN DBA	6.86	6.72	6.15	0.00	0.00
CLASS 1 (25-28)					
NUMBER OF POINTS	1	1	1	0	0
MIN. PTS. REQUIRED	0	0	0	0	0
MEAN MPH	28.00	28.00	28.00	0.00	0.00
MEAN ENERGY (DBA)	69.60	62.80	63.60	0.00	0.00
MEAN DBA	69.60	62.80	63.60	0.00	0.00
STD. DEV. MEAN DBA	0.00	0.00	0.00	0.00	0.00
CLASS 2 (29-32)					
NUMBER OF POINTS	8	8	8	0	0
MIN. PTS. REQUIRED	37	38	36	0	0
MEAN MPH	30.50	30.50	30.50	0.00	0.00
MEAN ENERGY (DBA)	69.73	63.30	64.30	0.00	0.00
MEAN DBA	68.94	62.54	63.57	0.00	0.00
STD. DEV. MEAN DBA	2.56	2.60	2.53	0.00	0.00
CLASS 3 (33-36)					
NUMBER OF POINTS	19	20	20	5	5
MIN. PTS. REQUIRED	37	35	30	1	12
MEAN MPH	34.37	34.40	34.40	35.20	35.20
MEAN ENERGY (DBA)	70.86	64.42	65.21	58.59	61.54
MEAN DBA	69.82	63.39	64.37	58.58	61.40
STD. DEV. MEAN DBA	2.90	2.83	2.61	0.31	1.24
CLASS 4 (37-40)					
NUMBER OF POINTS	9	9	9	1	1
MIN. PTS. REQUIRED	24	18	16	0	0
MEAN MPH	38.78	38.78	38.78	40.00	40.00
MEAN ENERGY (DBA)	70.77	64.12	65.53	58.20	60.80
MEAN DBA	70.31	63.73	65.19	58.20	60.80
STD. DEV. MEAN DBA	2.14	1.85	1.73	0.00	0.00
CLASS 5 (41-44)					
NUMBER OF POINTS	37	37	37	23	23
MIN. PTS. REQUIRED	25	29	24	42	28
MEAN MPH	42.54	42.54	42.54	42.43	42.43
MEAN ENERGY (DBA)	73.98	67.08	68.24	62.48	64.74
MEAN DBA	72.85	65.85	67.24	60.77	63.62
STD. DEV. MEAN DBA	2.50	2.70	2.44	3.12	2.56

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-com 15:01:30 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
CLASS 6 (45-48)					
NUMBER OF POINTS	40	40	40	19	19
MIN. PTS. REQUIRED	28	36	31	24	33
MEAN MPH	46.70	46.70	46.70	46.37	46.37
MEAN ENERGY (DBA)	75.48	69.14	70.01	62.28	65.05
MEAN DBA	74.65	68.07	69.12	61.55	64.07
STD. DEV. MEAN DBA	2.63	3.02	2.80	2.33	2.72
CLASS 7 (49-52)					
NUMBER OF POINTS	43	44	42	17	17
MIN. PTS. REQUIRED	12	15	12	21	19
MEAN MPH	50.65	50.64	50.64	50.59	50.59
MEAN ENERGY (DBA)	76.96	70.52	71.36	63.08	65.82
MEAN DBA	76.61	70.07	71.00	62.66	65.41
STD. DEV. MEAN DBA	1.75	1.96	1.76	2.16	2.03
CLASS 8 (53-56)					
NUMBER OF POINTS	83	84	84	29	29
MIN. PTS. REQUIRED	14	21	20	36	23
MEAN MPH	54.72	54.73	54.73	54.59	54.59
MEAN ENERGY (DBA)	77.93	71.91	72.48	65.26	66.80
MEAN DBA	77.47	71.24	71.90	64.30	66.26
STD. DEV. MEAN DBA	1.89	2.29	2.24	2.93	2.34
CLASS 9 (57-60)					
NUMBER OF POINTS	88	91	90	45	45
MIN. PTS. REQUIRED	19	24	18	31	28
MEAN MPH	58.48	58.47	58.48	58.56	58.56
MEAN ENERGY (DBA)	79.13	73.09	73.71	65.97	68.23
MEAN DBA	78.60	72.36	73.20	64.98	67.23
STD. DEV. MEAN DBA	2.16	2.44	2.14	2.79	2.66
CLASS 10 (61-64)					
NUMBER OF POINTS	61	62	60	38	37
MIN. PTS. REQUIRED	23	24	23	35	25
MEAN MPH	62.59	62.58	62.60	62.66	62.65
MEAN ENERGY (DBA)	79.83	73.83	74.65	67.39	68.69
MEAN DBA	79.14	73.04	73.93	66.18	67.89
STD. DEV. MEAN DBA	2.40	2.44	2.39	2.94	2.52
CLASS 11 (>64)					
NUMBER OF POINTS	24	27	24	14	14
MIN. PTS. REQUIRED	49	33	47	63	68
MEAN MPH	66.67	66.59	66.67	66.57	66.57
MEAN ENERGY (DBA)	81.36	74.28	75.84	68.44	70.12
MEAN DBA	80.24	73.52	74.74	66.81	68.31
STD. DEV. MEAN DBA	3.39	2.80	3.32	3.67	3.82

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-std 15:04:03 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
L0 = A + B*LOG(MPH) A =	14.91	5.34	9.10	12.91	21.23
B =	36.83	38.47	36.89	29.99	26.57
NUMBER OF OBSERVATIONS	819	838	824	419	416
STD. ERROR OF Y ON LOG(X)	2.90	2.86	2.88	2.89	2.40
INDEX OF DETERMINATION	0.52	0.54	0.52	0.32	0.35
COEFF. OF CORRELATION	0.72	0.74	0.72	0.57	0.59
F RATIO	869.97	984.74	890.31	196.22	221.87
L0 :					
MEAN	78.73	72.01	73.03	65.44	67.77
VARIANCE	17.39	17.78	17.24	12.26	8.85
STD. DEV.	4.17	4.22	4.15	3.50	2.97
L0E :					
A + 0.115*S0^2	15.88	6.28	10.06	13.87	21.89

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-std 15:04:03 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
SPEED CLASS DATA					
CLASS 0 ( <25 )					
NUMBER OF POINTS	1	1	1	0	0
MIN. PTS. REQUIRED	0	0	0	0	0
MEAN MPH	21.00	21.00	21.00	0.00	0.00
MEAN ENERGY (DBA)	62.40	55.30	56.90	0.00	0.00
MEAN DBA	62.40	55.30	56.90	0.00	0.00
STD. DEV. MEAN DBA	0.00	0.00	0.00	0.00	0.00
CLASS 1 (25-28)					
NUMBER OF POINTS	5	5	5	0	0
MIN. PTS. REQUIRED	173	164	138	0	0
MEAN MPH	27.20	27.20	27.20	0.00	0.00
MEAN ENERGY (DBA)	71.32	64.10	64.77	0.00	0.00
MEAN DBA	68.98	62.14	63.00	0.00	0.00
STD. DEV. MEAN DBA	4.73	4.61	4.23	0.00	0.00
CLASS 2 (29-32)					
NUMBER OF POINTS	13	13	13	3	3
MIN. PTS. REQUIRED	19	27	20	34	1
MEAN MPH	30.62	30.62	30.62	31.33	31.33
MEAN ENERGY (DBA)	70.09	63.53	64.37	59.67	62.04
MEAN DBA	69.63	62.88	63.91	59.53	62.03
STD. DEV. MEAN DBA	2.02	2.36	2.07	1.36	0.21
CLASS 3 (33-36)					
NUMBER OF POINTS	26	26	26	4	4
MIN. PTS. REQUIRED	36	44	32	34	54
MEAN MPH	34.73	34.73	34.73	34.25	34.25
MEAN ENERGY (DBA)	71.72	65.31	66.08	58.72	61.71
MEAN DBA	70.64	63.92	65.13	58.45	61.27
STD. DEV. MEAN DBA	2.93	3.22	2.73	1.83	2.30
CLASS 4 (37-40)					
NUMBER OF POINTS	24	24	24	6	6
MIN. PTS. REQUIRED	40	44	34	23	10
MEAN MPH	38.33	38.33	38.33	38.50	38.50
MEAN ENERGY (DBA)	74.56	67.56	68.40	61.27	63.51
MEAN DBA	73.48	66.41	67.46	60.92	63.37
STD. DEV. MEAN DBA	3.05	3.20	2.80	1.88	1.23
CLASS 5 (41-44)					
NUMBER OF POINTS	51	51	51	27	27
MIN. PTS. REQUIRED	36	35	29	25	17
MEAN MPH	42.73	42.73	42.73	42.81	42.81
MEAN ENERGY (DBA)	75.65	68.57	69.62	62.18	64.77
MEAN DBA	74.41	67.32	68.61	61.46	64.29
STD. DEV. MEAN DBA	2.98	2.96	2.69	2.41	2.03

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-std 15:04:04 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
<b>CLASS 6 (45-48)</b>					
NUMBER OF POINTS	52	52	52	28	27
MIN. PTS. REQUIRED	30	32	27	26	15
MEAN MPH	46.63	46.63	46.63	46.50	46.52
MEAN ENERGY (DBA)	76.52	69.49	70.81	62.92	65.40
MEAN DBA	75.72	68.59	70.05	62.27	65.00
STD. DEV. MEAN DBA	2.73	2.81	2.58	2.48	1.90
<b>CLASS 7 (49-52)</b>					
NUMBER OF POINTS	72	73	72	20	20
MIN. PTS. REQUIRED	50	44	45	18	34
MEAN MPH	50.76	50.78	50.76	50.75	50.75
MEAN ENERGY (DBA)	80.86	73.61	74.98	64.46	67.95
MEAN DBA	79.00	71.91	73.26	64.00	66.82
STD. DEV. MEAN DBA	3.55	3.32	3.34	2.03	2.78
<b>CLASS 8 (53-56)</b>					
NUMBER OF POINTS	167	174	167	76	76
MIN. PTS. REQUIRED	26	29	25	37	25
MEAN MPH	54.49	54.49	54.49	54.46	54.46
MEAN ENERGY (DBA)	80.09	73.44	74.45	66.74	68.71
MEAN DBA	79.24	72.50	73.63	65.55	67.91
STD. DEV. MEAN DBA	2.53	2.71	2.49	3.02	2.49
<b>CLASS 9 (57-60)</b>					
NUMBER OF POINTS	175	181	178	102	100
MIN. PTS. REQUIRED	37	33	37	41	29
MEAN MPH	58.54	58.56	58.54	58.63	58.64
MEAN ENERGY (DBA)	81.15	74.44	75.37	67.12	68.99
MEAN DBA	79.93	73.38	74.20	65.90	68.06
STD. DEV. MEAN DBA	3.05	2.89	3.03	3.20	2.70
<b>CLASS 10 (61-64)</b>					
NUMBER OF POINTS	154	158	155	101	101
MIN. PTS. REQUIRED	31	27	37	38	22
MEAN MPH	62.26	62.26	62.26	62.32	62.32
MEAN ENERGY (DBA)	81.80	75.19	76.04	67.92	69.68
MEAN DBA	80.79	74.24	75.01	66.55	68.85
STD. DEV. MEAN DBA	2.79	2.62	3.03	3.09	2.33
<b>CLASS 11 (&gt;64)</b>					
NUMBER OF POINTS	79	80	80	52	52
MIN. PTS. REQUIRED	33	33	33	29	22
MEAN MPH	68.23	68.20	68.20	68.33	68.33
MEAN ENERGY (DBA)	83.13	76.54	77.49	69.13	70.67
MEAN DBA	82.04	75.38	76.38	67.97	69.88
STD. DEV. MEAN DBA	2.86	2.85	2.85	2.69	2.34

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-com A-std 15:07:29 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
L0 = A + B*LOG(MPH) A =	13.33	4.31	7.48	9.92	19.18
B =	37.44	38.83	37.57	31.54	27.55
NUMBER OF OBSERVATIONS	1234	1263	1241	610	606
STD. ERROR OF Y ON LOG(X)	2.82	2.81	2.79	2.88	2.50
INDEX OF DETERMINATION	0.54	0.56	0.55	0.35	0.36
COEFF. OF CORRELATION	0.74	0.75	0.74	0.59	0.60
F RATIO	1460.56	1609.05	1519.16	330.28	333.39
L0 :					
MEAN	78.01	71.41	72.39	64.99	67.28
VARIANCE	17.40	17.92	17.27	12.76	9.66
STD. DEV.	4.17	4.23	4.16	3.57	3.11
L0E :					
A + 0.115*S0^2	14.25	5.21	8.37	10.88	19.90

D-7

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-com A-std 15:07:29 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
<b>SPEED CLASS DATA</b>					
CLASS 0 (<25)					
NUMBER OF POINTS	3	3	3	0	0
MIN. PTS. REQUIRED	513	535	424	0	0
MEAN MPH	23.00	23.00	23.00	0.00	0.00
MEAN ENERGY (DBA)	67.00	60.55	61.07	0.00	0.00
MEAN DBA	64.77	58.20	59.20	0.00	0.00
STD. DEV. MEAN DBA	5.27	5.37	4.78	0.00	0.00
CLASS 1 (25-28)					
NUMBER OF POINTS	6	6	6	0	0
MIN. PTS. REQUIRED	119	113	95	0	0
MEAN MPH	27.33	27.33	27.33	0.00	0.00
MEAN ENERGY (DBA)	71.08	63.90	64.60	0.00	0.00
MEAN DBA	69.08	62.25	63.10	0.00	0.00
STD. DEV. MEAN DBA	4.24	4.13	3.79	0.00	0.00
CLASS 2 (29-32)					
NUMBER OF POINTS	21	21	21	3	3
MIN. PTS. REQUIRED	21	25	21	34	1
MEAN MPH	30.57	30.57	30.57	31.33	31.33
MEAN ENERGY (DBA)	69.96	63.44	64.34	59.67	62.04
MEAN DBA	69.37	62.75	63.78	59.53	62.03
STD. DEV. MEAN DBA	2.20	2.40	2.20	1.36	0.21
CLASS 3 (33-36)					
NUMBER OF POINTS	45	46	46	9	9
MIN. PTS. REQUIRED	34	37	29	7	15
MEAN MPH	34.58	34.59	34.59	34.78	34.78
MEAN ENERGY (DBA)	71.38	64.95	65.72	58.65	61.62
MEAN DBA	70.29	63.69	64.80	58.52	61.34
STD. DEV. MEAN DBA	2.91	3.03	2.68	1.14	1.66
CLASS 4 (37-40)					
NUMBER OF POINTS	33	33	33	7	7
MIN. PTS. REQUIRED	40	39	30	24	13
MEAN MPH	38.45	38.45	38.45	38.71	38.71
MEAN ENERGY (DBA)	73.81	66.86	67.78	60.94	63.21
MEAN DBA	72.62	65.68	66.84	60.53	63.00
STD. DEV. MEAN DBA	3.15	3.11	2.73	2.00	1.48
CLASS 5 (41-44)					
NUMBER OF POINTS	88	88	88	50	50
MIN. PTS. REQUIRED	33	34	28	30	21
MEAN MPH	42.65	42.65	42.65	42.64	42.64
MEAN ENERGY (DBA)	75.02	68.00	69.09	62.32	64.76
MEAN DBA	73.75	66.70	68.04	61.14	63.98
STD. DEV. MEAN DBA	2.88	2.93	2.66	2.75	2.29

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) A-com A-std 15:07:30 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
CLASS 6 (45-48)					
NUMBER OF POINTS	92	92	92	47	46
MIN. PTS. REQUIRED	30	34	29	23	21
MEAN MPH	46.66	46.66	46.66	46.45	46.46
MEAN ENERGY (DBA)	76.10	69.34	70.48	62.67	65.26
MEAN DBA	75.26	68.36	69.65	61.98	64.62
STD. DEV. MEAN DBA	2.73	2.90	2.70	2.42	2.29
CLASS 7 (49-52)					
NUMBER OF POINTS	115	117	114	37	37
MIN. PTS. REQUIRED	41	36	37	19	26
MEAN MPH	50.72	50.73	50.72	50.68	50.68
MEAN ENERGY (DBA)	79.77	72.68	73.97	63.88	67.10
MEAN DBA	78.10	71.21	72.42	63.39	66.17
STD. DEV. MEAN DBA	3.21	3.01	3.06	2.17	2.53
CLASS 8 (53-56)					
NUMBER OF POINTS	250	258	251	105	105
MIN. PTS. REQUIRED	25	28	26	37	26
MEAN MPH	54.56	54.57	54.57	54.50	54.50
MEAN ENERGY (DBA)	79.48	72.99	73.88	66.38	68.26
MEAN DBA	78.65	72.09	73.05	65.20	67.45
STD. DEV. MEAN DBA	2.48	2.64	2.54	3.03	2.55
CLASS 9 (57-60)					
NUMBER OF POINTS	263	272	268	147	145
MIN. PTS. REQUIRED	32	31	31	38	29
MEAN MPH	58.52	58.53	58.52	58.61	58.61
MEAN ENERGY (DBA)	80.57	74.03	74.88	66.80	68.77
MEAN DBA	79.49	73.04	73.86	65.62	67.80
STD. DEV. MEAN DBA	2.85	2.79	2.80	3.10	2.71
CLASS 10 (61-64)					
NUMBER OF POINTS	215	220	215	139	138
MIN. PTS. REQUIRED	31	27	34	37	23
MEAN MPH	62.35	62.35	62.36	62.41	62.41
MEAN ENERGY (DBA)	81.32	74.85	75.70	67.78	69.43
MEAN DBA	80.32	73.91	74.71	66.45	68.59
STD. DEV. MEAN DBA	2.78	2.62	2.90	3.05	2.41
CLASS 11 ( >64 )					
NUMBER OF POINTS	103	107	104	66	66
MIN. PTS. REQUIRED	38	35	37	34	31
MEAN MPH	67.86	67.79	67.85	67.95	67.95
MEAN ENERGY (DBA)	82.78	76.07	77.16	69.00	70.56
MEAN DBA	81.62	74.91	76.00	67.72	69.55
STD. DEV. MEAN DBA	3.07	2.94	3.03	2.93	2.76

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) MT 15:09:34 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
L0 = A + B*LOG(MPH) A =	40.56	34.42	34.06	27.27	29.04
B =	25.79	25.59	26.17	25.33	25.35
NUMBER OF OBSERVATIONS	313	317	312	187	187
STD. ERROR OF Y ON LOG(X)	2.72	2.83	2.86	3.39	2.52
INDEX OF DETERMINATION	0.45	0.42	0.43	0.14	0.23
COEFF. OF CORRELATION	0.67	0.65	0.66	0.38	0.48
F RATIO	251.62	229.19	233.70	31.34	56.68
L0 :					
MEAN	84.57	78.10	78.72	71.53	73.33
VARIANCE	13.36	13.82	14.33	13.35	8.26
STD. DEV.	3.65	3.72	3.78	3.65	2.87
L0E :					
A + 0.115*S0^2	41.41	35.34	35.00	28.59	29.77

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) MT 15:09:34 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
SPEED CLASS DATA					
CLASS 0 ( <25 )					
NUMBER OF POINTS	1	1	1	0	0
MIN. PTS. REQUIRED	0	0	0	0	0
MEAN MPH	22.00	22.00	22.00	0.00	0.00
MEAN ENERGY (DBA)	70.20	63.30	64.30	0.00	0.00
MEAN DBA	70.20	63.30	64.30	0.00	0.00
STD. DEV. MEAN DBA	0.00	0.00	0.00	0.00	0.00
CLASS 1 (25-28)					
NUMBER OF POINTS	7	7	7	0	0
MIN. PTS. REQUIRED	135	178	166	0	0
MEAN MPH	27.43	27.43	27.43	0.00	0.00
MEAN ENERGY (DBA)	80.20	74.37	75.00	0.00	0.00
MEAN DBA	78.44	72.03	72.90	0.00	0.00
STD. DEV. MEAN DBA	4.75	5.46	5.26	0.00	0.00
CLASS 2 (29-32)					
NUMBER OF POINTS	8	8	8	0	0
MIN. PTS. REQUIRED	40	45	41	0	0
MEAN MPH	30.50	30.50	30.50	0.00	0.00
MEAN ENERGY (DBA)	80.43	74.48	74.59	0.00	0.00
MEAN DBA	79.57	73.61	73.76	0.00	0.00
STD. DEV. MEAN DBA	2.68	2.85	2.72	0.00	0.00
CLASS 3 (33-36)					
NUMBER OF POINTS	20	20	20	3	3
MIN. PTS. REQUIRED	52	50	42	90	50
MEAN MPH	34.10	34.10	34.10	33.33	33.33
MEAN ENERGY (DBA)	82.59	76.02	76.00	67.56	68.78
MEAN DBA	81.05	74.63	74.86	67.20	68.57
STD. DEV. MEAN DBA	3.44	3.38	3.08	2.20	1.65
CLASS 4 (37-40)					
NUMBER OF POINTS	15	15	15	3	3
MIN. PTS. REQUIRED	56	48	44	239	84
MEAN MPH	38.67	38.67	38.67	38.33	38.33
MEAN ENERGY (DBA)	83.64	76.73	77.16	71.93	72.64
MEAN DBA	82.29	75.58	76.14	70.93	72.27
STD. DEV. MEAN DBA	3.48	3.23	3.10	3.59	2.14
CLASS 5 (41-44)					
NUMBER OF POINTS	16	16	16	7	7
MIN. PTS. REQUIRED	28	31	26	11	17
MEAN MPH	42.38	42.38	42.38	42.86	42.86
MEAN ENERGY (DBA)	82.51	76.25	76.46	70.19	71.57
MEAN DBA	81.90	75.50	75.89	70.01	71.27
STD. DEV. MEAN DBA	2.49	2.62	2.37	1.37	1.70

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) MT 15:09:34 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
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	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
<b>CLASS 6 (45-48)</b>					
NUMBER OF POINTS	19	19	19	6	6
MIN. PTS. REQUIRED	27	59	43	42	37
MEAN MPH	46.32	46.32	46.32	46.17	46.17
MEAN ENERGY (DBA)	82.70	75.96	76.64	68.25	69.93
MEAN DBA	82.13	74.95	75.90	67.70	69.43
STD. DEV. MEAN DBA	2.50	3.66	3.14	2.53	2.36
<b>CLASS 7 (49-52)</b>					
NUMBER OF POINTS	31	32	31	14	14
MIN. PTS. REQUIRED	24	23	20	38	24
MEAN MPH	50.71	50.69	50.71	50.86	50.86
MEAN ENERGY (DBA)	84.79	78.48	79.10	70.98	72.47
MEAN DBA	84.12	77.85	78.55	70.16	71.95
STD. DEV. MEAN DBA	2.44	2.42	2.25	2.87	2.25
<b>CLASS 8 (53-56)</b>					
NUMBER OF POINTS	67	69	67	47	47
MIN. PTS. REQUIRED	30	29	29	34	24
MEAN MPH	54.57	54.58	54.57	54.57	54.57
MEAN ENERGY (DBA)	85.16	78.98	79.60	71.05	72.89
MEAN DBA	84.35	78.11	78.81	70.06	72.23
STD. DEV. MEAN DBA	2.72	2.71	2.67	2.91	2.43
<b>CLASS 9 (57-60)</b>					
NUMBER OF POINTS	77	78	77	63	63
MIN. PTS. REQUIRED	22	23	20	40	19
MEAN MPH	58.45	58.45	58.45	58.44	58.44
MEAN ENERGY (DBA)	87.18	80.78	81.47	73.48	74.72
MEAN DBA	86.53	80.11	80.87	72.45	74.19
STD. DEV. MEAN DBA	2.35	2.37	2.22	3.17	2.15
<b>CLASS 10 (61-64)</b>					
NUMBER OF POINTS	44	44	43	36	36
MIN. PTS. REQUIRED	19	24	55	86	45
MEAN MPH	62.07	62.07	62.09	62.06	62.06
MEAN ENERGY (DBA)	88.41	81.74	82.38	75.00	75.94
MEAN DBA	87.84	81.02	81.43	73.05	74.86
STD. DEV. MEAN DBA	2.18	2.46	3.71	4.62	3.34
<b>CLASS 11 (&gt;64)</b>					
NUMBER OF POINTS	8	8	8	8	8
MIN. PTS. REQUIRED	16	8	9	33	12
MEAN MPH	67.38	67.38	67.38	67.38	67.38
MEAN ENERGY (DBA)	87.89	81.24	82.10	75.03	75.76
MEAN DBA	87.62	81.10	81.94	74.46	75.56
STD. DEV. MEAN DBA	1.68	1.21	1.29	2.44	1.44

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-3 15:11:21 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
LØ = A + B*LOG(MPH) A =	62.05	54.25	52.37	79.00	76.92
B =	14.93	15.80	17.19	-2.48	-.48
NUMBER OF OBSERVATIONS	203	205	204	106	106
STD. ERROR OF Y ON LOG(X)	3.26	2.99	2.91	3.65	2.86
INDEX OF DETERMINATION	0.20	0.25	0.29	0.00	0.00
COEFF. OF CORRELATION	0.45	0.50	0.54	-1.06	-.01
F RATIO	50.55	67.08	83.87	0.34	0.02
LØ :					
MEAN	87.05	80.69	81.14	74.72	76.09
VARIANCE	13.20	11.87	11.95	13.27	8.08
STD. DEV.	3.63	3.45	3.46	3.64	2.84
LØE :					
A + 0.115*SØ^2	63.27	55.28	53.34	80.53	77.86

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-3 15:11:21 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
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	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
<b>SPEED CLASS DATA</b>					
<b>CLASS 1 (25-28)</b>					
NUMBER OF POINTS	10	10	10	3	3
MIN. PTS. REQUIRED	46	52	53	49	42
MEAN MPH	27.20	27.20	27.20	27.00	27.00
MEAN ENERGY (DBA)	84.99	78.50	78.60	76.15	76.14
MEAN DBA	84.15	77.59	77.65	75.97	75.97
STD. DEV. MEAN DBA	2.99	3.19	3.21	1.63	1.50
<b>CLASS 2 (29-32)</b>					
NUMBER OF POINTS	14	14	14	3	3
MIN. PTS. REQUIRED	110	102	100	795	643
MEAN MPH	30.43	30.43	30.43	30.33	30.33
MEAN ENERGY (DBA)	87.40	81.32	81.33	83.82	83.29
MEAN DBA	83.29	77.27	77.48	80.43	80.50
STD. DEV. MEAN DBA	4.86	4.68	4.62	6.55	5.89
<b>CLASS 3 (33-36)</b>					
NUMBER OF POINTS	19	19	19	2	2
MIN. PTS. REQUIRED	54	42	411424	633	
MEAN MPH	34.89	34.89	34.89	35.50	35.50
MEAN ENERGY (DBA)	85.68	79.04	79.22	77.19	76.92
MEAN DBA	84.36	77.87	78.12	76.70	76.70
STD. DEV. MEAN DBA	3.49	3.09	3.06	2.97	1.98
<b>CLASS 4 (37-40)</b>					
NUMBER OF POINTS	14	15	15	1	1
MIN. PTS. REQUIRED	30	34	35	0	0
MEAN MPH	38.07	38.20	38.20	37.00	37.00
MEAN ENERGY (DBA)	87.66	80.95	81.04	77.10	77.10
MEAN DBA	86.90	80.01	80.15	77.10	77.10
STD. DEV. MEAN DBA	2.51	2.71	2.77	0.00	0.00
<b>CLASS 5 (41-44)</b>					
NUMBER OF POINTS	8	9	8	3	3
MIN. PTS. REQUIRED	24	21	22	198	57
MEAN MPH	42.63	42.78	42.63	43.00	43.00
MEAN ENERGY (DBA)	87.51	80.00	81.37	73.55	75.67
MEAN DBA	87.07	79.62	80.97	72.70	75.43
STD. DEV. MEAN DBA	2.05	1.98	2.00	3.27	1.76
<b>CLASS 6 (45-48)</b>					
NUMBER OF POINTS	15	15	15	6	6
MIN. PTS. REQUIRED	23	18	19	32	14
MEAN MPH	46.40	46.40	46.40	47.17	47.17
MEAN ENERGY (DBA)	87.23	80.78	81.25	73.38	74.61
MEAN DBA	86.73	80.37	80.82	72.80	74.38
STD. DEV. MEAN DBA	2.23	2.00	2.05	2.19	1.46

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-3 15:11:22 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
CLASS 7 (49-52)					
NUMBER OF POINTS	27	27	27	13	13
MIN. PTS. REQUIRED	28	25	23	43	25
MEAN MPH	51.04	51.04	51.04	51.08	51.08
MEAN ENERGY (DBA)	88.63	82.31	82.73	73.73	75.32
MEAN DBA	87.93	81.67	82.14	72.80	74.74
STD. DEV. MEAN DBA	2.56	2.42	2.33	3.01	2.30
CLASS 8 (53-56)					
NUMBER OF POINTS	41	41	41	31	31
MIN. PTS. REQUIRED	44	43	39	51	34
MEAN MPH	54.49	54.49	54.49	54.42	54.42
MEAN ENERGY (DBA)	88.99	82.90	83.07	75.25	76.35
MEAN DBA	87.74	81.66	81.99	73.67	75.32
STD. DEV. MEAN DBA	3.32	3.28	3.12	3.58	2.93
CLASS 9 (57-60)					
NUMBER OF POINTS	34	34	34	27	27
MIN. PTS. REQUIRED	23	18	17	40	20
MEAN MPH	58.71	58.71	58.71	58.74	58.74
MEAN ENERGY (DBA)	89.55	83.00	83.68	76.43	77.42
MEAN DBA	88.85	82.44	83.11	75.41	76.84
STD. DEV. MEAN DBA	2.42	2.14	2.08	3.06	2.19
CLASS 10 (61-64)					
NUMBER OF POINTS	17	17	17	13	13
MIN. PTS. REQUIRED	35	36	30	48	32
MEAN MPH	62.35	62.35	62.35	62.38	62.38
MEAN ENERGY (DBA)	89.94	83.71	84.11	77.93	78.37
MEAN DBA	89.05	82.75	83.26	76.74	77.55
STD. DEV. MEAN DBA	2.78	2.82	2.60	3.17	2.59
CLASS 11 ( >64 )					
NUMBER OF POINTS	4	4	4	4	4
MIN. PTS. REQUIRED	1004	504	498	305	209
MEAN MPH	66.00	66.00	66.00	66.00	66.00
MEAN ENERGY (DBA)	89.50	82.38	83.76	77.04	77.10
MEAN DBA	85.17	79.90	81.15	75.42	75.82
STD. DEV. MEAN DBA	9.96	7.05	7.02	5.49	4.54

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-4 15:12:59 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
L0 = A + B*LOG(MPH) A =	59.53	58.74	59.11	41.99	60.76
B =	17.11	13.69	13.86	18.64	8.87
NUMBER OF OBSERVATIONS	51	51	50	35	35
STD. ERROR OF Y ON LOG(X)	2.31	2.34	2.72	3.19	3.01
INDEX OF DETERMINATION	0.25	0.17	0.14	0.03	0.01
COEFF. OF CORRELATION	0.50	0.41	0.37	0.19	0.10
F RATIO	16.26	10.15	7.67	1.19	0.30
L0 :					
MEAN	89.13	82.43	83.08	74.88	76.41
VARIANCE	6.96	6.47	8.43	10.22	8.90
STD. DEV.	2.64	2.54	2.90	3.20	2.98
L0E :					
A + 0.115*S0^2	60.15	59.37	59.97	43.16	61.81

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-4 15:13:00 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
SPEED CLASS DATA					
CLASS 2 (29-32)					
NUMBER OF POINTS	1	1	1	0	0
MIN. PTS. REQUIRED	0	0	0	0	0
MEAN MPH	31.00	31.00	31.00	0.00	0.00
MEAN ENERGY (DBA)	87.10	81.00	81.20	0.00	0.00
MEAN DBA	87.10	81.00	81.20	0.00	0.00
STD. DEV. MEAN DBA	0.00	0.00	0.00	0.00	0.00
CLASS 3 (33-36)					
NUMBER OF POINTS	2	2	2	0	0
MIN. PTS. REQUIRED	291	182	726	0	0
MEAN MPH	34.50	34.50	34.50	0.00	0.00
MEAN ENERGY (DBA)	85.65	79.91	81.05	0.00	0.00
MEAN DBA	85.55	79.85	80.80	0.00	0.00
STD. DEV. MEAN DBA	1.34	1.06	2.12	0.00	0.00
CLASS 4 (37-40)					
NUMBER OF POINTS	3	3	3	0	0
MIN. PTS. REQUIRED	28	37	31	0	0
MEAN MPH	39.00	39.00	39.00	0.00	0.00
MEAN ENERGY (DBA)	87.48	81.15	81.83	0.00	0.00
MEAN DBA	87.37	81.00	81.70	0.00	0.00
STD. DEV. MEAN DBA	1.22	1.41	1.30	0.00	0.00
CLASS 5 (41-44)					
NUMBER OF POINTS	1	1	1	0	0
MIN. PTS. REQUIRED	0	0	0	0	0
MEAN MPH	42.00	42.00	42.00	0.00	0.00
MEAN ENERGY (DBA)	84.50	77.20	77.60	0.00	0.00
MEAN DBA	84.50	77.20	77.60	0.00	0.00
STD. DEV. MEAN DBA	0.00	0.00	0.00	0.00	0.00
CLASS 6 (45-48)					
NUMBER OF POINTS	3	3	3	1	1
MIN. PTS. REQUIRED	543	771	611	0	0
MEAN MPH	47.00	47.00	47.00	48.00	48.00
MEAN ENERGY (DBA)	92.64	86.95	86.73	83.90	84.80
MEAN DBA	90.27	83.67	84.07	83.90	84.80
STD. DEV. MEAN DBA	5.42	6.45	5.74	0.00	0.00
CLASS 7 (49-52)					
NUMBER OF POINTS	5	5	5	2	2
MIN. PTS. REQUIRED	84	58	77	98	233
MEAN MPH	50.20	50.20	50.20	50.50	50.50
MEAN ENERGY (DBA)	88.80	82.35	83.32	71.18	74.13
MEAN DBA	88.04	81.70	82.52	71.15	74.05
STD. DEV. MEAN DBA	3.30	2.74	3.17	0.78	1.20

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-4 15:13:00 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
CLASS 8 (53-56)					
NUMBER OF POINTS	9	9	8	7	7
MIN. PTS. REQUIRED	14	14	14	25	24
MEAN MPH	54.67	54.67	54.75	54.57	54.57
MEAN ENERGY (DBA)	88.65	82.20	82.79	74.20	75.85
MEAN DBA	88.39	81.93	82.52	73.81	75.47
STD. DEV. MEAN DBA	1.62	1.60	1.58	2.06	2.01
CLASS 9 (57-60)					
NUMBER OF POINTS	13	13	13	13	13
MIN. PTS. REQUIRED	9	7	42	25	26
MEAN MPH	58.38	58.38	58.38	58.38	58.38
MEAN ENERGY (DBA)	89.48	82.39	83.32	74.58	76.44
MEAN DBA	89.29	82.24	82.69	74.14	75.93
STD. DEV. MEAN DBA	1.37	1.21	2.97	2.27	2.32
CLASS 10 (61-64)					
NUMBER OF POINTS	13	13	13	11	11
MIN. PTS. REQUIRED	29	28	27	56	56
MEAN MPH	62.31	62.31	62.31	62.45	62.45
MEAN ENERGY (DBA)	91.45	84.65	85.40	76.78	77.86
MEAN DBA	90.87	84.02	84.85	76.04	77.08
STD. DEV. MEAN DBA	2.48	2.44	2.40	3.35	3.37
CLASS 11 (>64)					
NUMBER OF POINTS	1	1	1	1	1
MIN. PTS. REQUIRED	0	0	0	0	0
MEAN MPH	65.00	65.00	65.00	65.00	65.00
MEAN ENERGY (DBA)	92.00	84.50	85.70	77.70	78.20
MEAN DBA	92.00	84.50	85.70	77.70	78.20
STD. DEV. MEAN DBA	0.00	0.00	0.00	0.00	0.00

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-5 15:15:25 \*  
 ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
$L0 = A + B \cdot \text{LOG}(\text{MPH})$	A = 58.46	50.30	50.78	17.78	23.37
	B = 17.75	18.88	18.96	32.92	30.65
NUMBER OF OBSERVATIONS	881	898	886	566	562
STD. ERROR OF Y ON LOG(X)	2.58	2.57	2.49	2.91	2.44
INDEX OF DETERMINATION	0.23	0.26	0.27	0.13	0.16
COEFF. OF CORRELATION	0.48	0.51	0.52	0.37	0.40
F RATIO	268.60	307.09	329.88	86.97	106.14
<b>L0 :</b>					
MEAN	89.20	83.00	83.62	75.83	77.41
VARIANCE	8.69	8.88	8.48	9.77	7.09
STD. DEV.	2.95	2.98	2.91	3.13	2.66
<b>L0E :</b>					
$A + 0.115 \cdot S0^2$	59.23	51.06	51.49	18.76	24.06

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-5 15:15:25 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
<b>SPEED CLASS DATA</b>					
<b>CLASS 0 ( &lt;25 )</b>					
NUMBER OF POINTS	3	3	3	0	0
MIN. PTS. REQUIRED	242	345	357	0	0
MEAN MPH	21.00	21.00	21.00	0.00	0.00
MEAN ENERGY (DBA)	81.79	76.68	77.10	0.00	0.00
MEAN DBA	80.77	75.57	75.97	0.00	0.00
STD. DEV. MEAN DBA	3.61	4.32	4.39	0.00	0.00
<b>CLASS 1 (25-28)</b>					
NUMBER OF POINTS	8	8	8	0	0
MIN. PTS. REQUIRED	88	72	74	0	0
MEAN MPH	27.00	27.00	27.00	0.00	0.00
MEAN ENERGY (DBA)	87.45	80.40	80.87	0.00	0.00
MEAN DBA	85.81	78.96	79.42	0.00	0.00
STD. DEV. MEAN DBA	3.97	3.60	3.64	0.00	0.00
<b>CLASS 2 (29-32)</b>					
NUMBER OF POINTS	22	22	22	0	0
MIN. PTS. REQUIRED	25	23	27	0	0
MEAN MPH	30.59	30.59	30.59	0.00	0.00
MEAN ENERGY (DBA)	86.35	79.96	80.78	0.00	0.00
MEAN DBA	85.63	79.32	80.00	0.00	0.00
STD. DEV. MEAN DBA	2.41	2.30	2.50	0.00	0.00
<b>CLASS 3 (33-36)</b>					
NUMBER OF POINTS	19	19	19	0	0
MIN. PTS. REQUIRED	30	30	28	0	0
MEAN MPH	34.74	34.74	34.74	0.00	0.00
MEAN ENERGY (DBA)	86.04	79.86	80.18	0.00	0.00
MEAN DBA	85.28	79.14	79.49	0.00	0.00
STD. DEV. MEAN DBA	2.59	2.59	2.51	0.00	0.00
<b>CLASS 4 (37-40)</b>					
NUMBER OF POINTS	16	16	16	0	0
MIN. PTS. REQUIRED	27	21	28	0	0
MEAN MPH	38.75	38.75	38.75	0.00	0.00
MEAN ENERGY (DBA)	87.75	80.78	81.65	0.00	0.00
MEAN DBA	87.01	80.27	80.94	0.00	0.00
STD. DEV. MEAN DBA	2.46	2.16	2.49	0.00	0.00
<b>CLASS 5 (41-44)</b>					
NUMBER OF POINTS	39	38	38	3	3
MIN. PTS. REQUIRED	21	18	16	98	10
MEAN MPH	43.16	43.16	43.16	43.67	43.67
MEAN ENERGY (DBA)	88.95	82.14	82.87	73.61	74.47
MEAN DBA	88.37	81.64	82.42	73.23	74.43
STD. DEV. MEAN DBA	2.27	2.09	2.01	2.30	0.72

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-5 15:15:26 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
-----					
CLASS 6 (45-48)					
NUMBER OF POINTS	58	59	58	16	16
MIN. PTS. REQUIRED	18	21	16	21	12
MEAN MPH	46.14	46.14	46.14	46.38	46.38
MEAN ENERGY (DBA)	88.31	81.93	82.58	73.76	75.43
MEAN DBA	87.84	81.36	82.16	73.27	75.14
STD. DEV. MEAN DBA	2.11	2.30	2.00	2.18	1.60
CLASS 7 (49-52)					
NUMBER OF POINTS	72	74	74	34	33
MIN. PTS. REQUIRED	31	29	30	36	28
MEAN MPH	50.97	51.00	51.00	51.03	51.00
MEAN ENERGY (DBA)	88.89	82.77	83.18	75.25	76.54
MEAN DBA	87.77	81.77	82.16	74.05	75.47
STD. DEV. MEAN DBA	2.80	2.71	2.74	2.99	2.64
CLASS 8 (53-56)					
NUMBER OF POINTS	175	183	179	134	134
MIN. PTS. REQUIRED	25	29	26	36	25
MEAN MPH	54.63	54.62	54.61	54.74	54.74
MEAN ENERGY (DBA)	89.69	83.67	84.10	76.07	77.40
MEAN DBA	88.91	82.72	83.33	74.81	76.59
STD. DEV. MEAN DBA	2.51	2.69	2.53	3.02	2.51
CLASS 9 (57-60)					
NUMBER OF POINTS	250	253	250	203	203
MIN. PTS. REQUIRED	20	21	19	29	18
MEAN MPH	58.60	58.59	58.59	58.65	58.65
MEAN ENERGY (DBA)	90.23	84.18	84.76	76.68	77.92
MEAN DBA	89.61	83.51	84.14	75.83	77.41
STD. DEV. MEAN DBA	2.23	2.30	2.17	2.70	2.12
CLASS 10 (61-64)					
NUMBER OF POINTS	180	182	179	145	142
MIN. PTS. REQUIRED	22	21	19	30	23
MEAN MPH	62.07	62.08	62.08	62.01	62.01
MEAN ENERGY (DBA)	91.61	85.36	85.94	77.83	79.09
MEAN DBA	90.83	84.63	85.31	76.91	78.39
STD. DEV. MEAN DBA	2.34	2.31	2.20	2.74	2.42
CLASS 11 (>64)					
NUMBER OF POINTS	40	41	40	31	31
MIN. PTS. REQUIRED	80	67	66	78	64
MEAN MPH	66.92	66.88	66.92	67.13	67.13
MEAN ENERGY (DBA)	93.81	87.52	88.20	80.62	81.61
MEAN DBA	91.94	85.95	86.47	78.67	79.98
STD. DEV. MEAN DBA	4.47	4.09	4.06	4.42	4.01
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\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 1 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-3 HT-4 HT-5 15:18:26 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
REGRESSION EQUATION :					
L0 = A + B*LOG(MPH) A =	57.52	49.54	49.09	48.03	49.31
B =	18.18	19.18	19.79	15.70	15.85
NUMBER OF OBSERVATIONS	1135	1154	1140	707	703
STD. ERROR OF Y ON LOG(X)	2.73	2.68	2.63	3.15	2.65
INDEX OF DETERMINATION	0.26	0.29	0.31	0.05	0.07
COEFF. OF CORRELATION	0.51	0.53	0.56	0.23	0.27
F RATIO	395.37	459.70	507.52	39.43	56.73
L0 :					
MEAN	88.81	82.57	83.15	75.61	77.16
VARIANCE	10.08	10.06	9.98	10.46	7.56
STD. DEV.	3.17	3.17	3.16	3.23	2.75
L0E :					
A + 0.115*S0^2	58.38	50.37	49.88	49.17	50.12

\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 2 \*  
 SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-3 HT-4 HT-5 15:18:26 \*  
 ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 MIN. EVENT QUAL. 1 1 1 1 \*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
SPEED CLASS DATA					
CLASS 0 (<25)					
NUMBER OF POINTS	3	3	3	0	0
MIN. PTS. REQUIRED	242	345	357	0	0
MEAN MPH	21.00	21.00	21.00	0.00	0.00
MEAN ENERGY (DBA)	81.79	76.68	77.10	0.00	0.00
MEAN DBA	80.77	75.57	75.97	0.00	0.00
STD. DEV. MEAN DBA	3.61	4.32	4.39	0.00	0.00
CLASS 1 (25-28)					
NUMBER OF POINTS	18	18	18	3	3
MIN. PTS. REQUIRED	53	50	52	49	42
MEAN MPH	27.11	27.11	27.11	27.00	27.00
MEAN ENERGY (DBA)	86.26	79.45	79.76	76.15	76.14
MEAN DBA	84.89	78.20	78.44	75.97	75.97
STD. DEV. MEAN DBA	3.45	3.35	3.42	1.63	1.50
CLASS 2 (29-32)					
NUMBER OF POINTS	37	37	37	3	3
MIN. PTS. REQUIRED	53	49	52	795	643
MEAN MPH	30.54	30.54	30.54	30.33	30.33
MEAN ENERGY (DBA)	86.80	80.55	81.01	83.82	83.29
MEAN DBA	84.79	78.59	79.08	80.43	80.50
STD. DEV. MEAN DBA	3.66	3.49	3.61	6.55	5.89
CLASS 3 (33-36)					
NUMBER OF POINTS	40	40	40	2	2
MIN. PTS. REQUIRED	36	32	32	1424	633
MEAN MPH	34.80	34.80	34.80	35.50	35.50
MEAN ENERGY (DBA)	85.85	79.49	79.80	77.19	76.92
MEAN DBA	84.85	78.57	78.90	76.70	76.70
STD. DEV. MEAN DBA	3.00	2.83	2.83	2.97	1.98
CLASS 4 (37-40)					
NUMBER OF POINTS	33	34	34	1	1
MIN. PTS. REQUIRED	22	22	26	0	0
MEAN MPH	38.48	38.53	38.53	37.00	37.00
MEAN ENERGY (DBA)	87.69	80.89	81.41	77.10	77.10
MEAN DBA	87.00	80.22	80.66	77.10	77.10
STD. DEV. MEAN DBA	2.35	2.33	2.54	0.00	0.00
CLASS 5 (41-44)					
NUMBER OF POINTS	47	48	47	6	6
MIN. PTS. REQUIRED	21	20	18	43	12
MEAN MPH	43.04	43.06	43.04	43.33	43.33
MEAN ENERGY (DBA)	88.67	81.74	82.58	73.58	75.11
MEAN DBA	88.06	81.17	82.07	72.97	74.93
STD. DEV. MEAN DBA	2.30	2.26	2.15	2.55	1.32

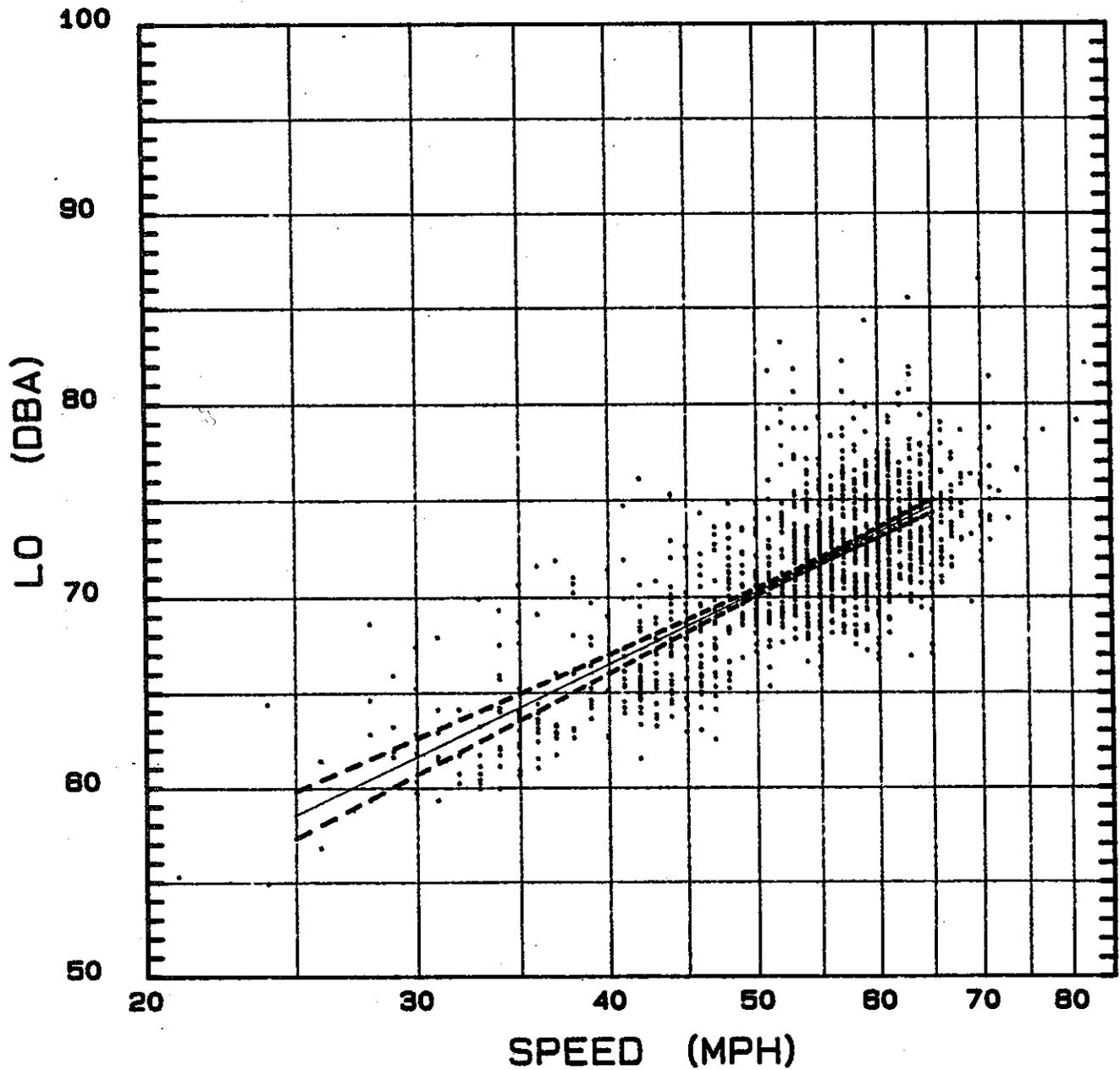
\*\*\*\*\* DATA SUMMARY \*\*\*\*\* PAGE : 3 \*  
 \* SITES-1,2,3,5,6,7,9,10,11,12,14,15,16,17,18,19 84/06/22 \*  
 \* ALL VEHICLE SPEEDS VEHICLE TYPE(S) HT-3 HT-4 HT-5 15:18:27 \*  
 \* ALL WIND SPEEDS ALL WIND ANGLES ALL WIND VECTORS \*  
 \* MIN. EVENT QUAL. 1 1 1 1 \*  
 \*\*\*\*\*

	MIC-1	MIC-2	MIC-3	MIC-4	MIC-5
<b>CLASS 6 (45-48)</b>					
NUMBER OF POINTS	76	77	76	23	23
MIN. PTS. REQUIRED	22	25	21	40	28
MEAN MPH	46.22	46.22	46.22	46.65	46.65
MEAN ENERGY (DBA)	88.42	82.10	82.63	75.17	76.53
MEAN DBA	87.72	81.26	81.97	73.61	75.37
STD. DEV. MEAN DBA	2.36	2.50	2.28	3.06	2.56
<b>CLASS 7 (49-52)</b>					
NUMBER OF POINTS	104	106	106	49	48
MIN. PTS. REQUIRED	30	27	28	36	25
MEAN MPH	50.95	50.97	50.97	51.02	51.00
MEAN ENERGY (DBA)	88.82	82.64	83.08	74.78	76.16
MEAN DBA	87.82	81.74	82.17	73.60	75.21
STD. DEV. MEAN DBA	2.74	2.62	2.64	3.00	2.51
<b>CLASS 8 (53-56)</b>					
NUMBER OF POINTS	225	233	228	172	172
MIN. PTS. REQUIRED	29	31	28	39	27
MEAN MPH	54.60	54.60	54.59	54.67	54.67
MEAN ENERGY (DBA)	89.53	83.49	83.89	75.87	77.17
MEAN DBA	88.68	82.51	83.06	74.57	76.31
STD. DEV. MEAN DBA	2.68	2.79	2.66	3.11	2.61
<b>CLASS 9 (57-60)</b>					
NUMBER OF POINTS	297	300	297	243	243
MIN. PTS. REQUIRED	20	21	20	30	19
MEAN MPH	58.60	58.60	58.59	58.65	58.65
MEAN ENERGY (DBA)	90.13	83.99	84.59	76.56	77.80
MEAN DBA	89.51	83.34	83.96	75.69	77.27
STD. DEV. MEAN DBA	2.23	2.27	2.23	2.74	2.16
<b>CLASS 10 (61-64)</b>					
NUMBER OF POINTS	210	212	209	169	166
MIN. PTS. REQUIRED	24	23	21	31	25
MEAN MPH	62.11	62.12	62.11	62.07	62.07
MEAN ENERGY (DBA)	91.48	85.21	85.79	77.78	78.97
MEAN DBA	90.69	84.44	85.11	76.84	78.23
STD. DEV. MEAN DBA	2.43	2.40	2.31	2.80	2.51
<b>CLASS 11 (&gt;64)</b>					
NUMBER OF POINTS	45	46	45	36	36
MIN. PTS. REQUIRED	113	85	81	82	69
MEAN MPH	66.80	66.76	66.80	66.94	66.94
MEAN ENERGY (DBA)	93.53	87.20	87.90	80.28	81.21
MEAN DBA	91.34	85.39	85.98	78.28	79.47
STD. DEV. MEAN DBA	5.32	4.60	4.51	4.52	4.17

# CALIFORNIA VEHICLE NOISE EMISSIONS LO VS. SPEED

VEHICLE TYPE: ALL AUTOS  
MIC.#2 HT-5FT. DIST-50FT.

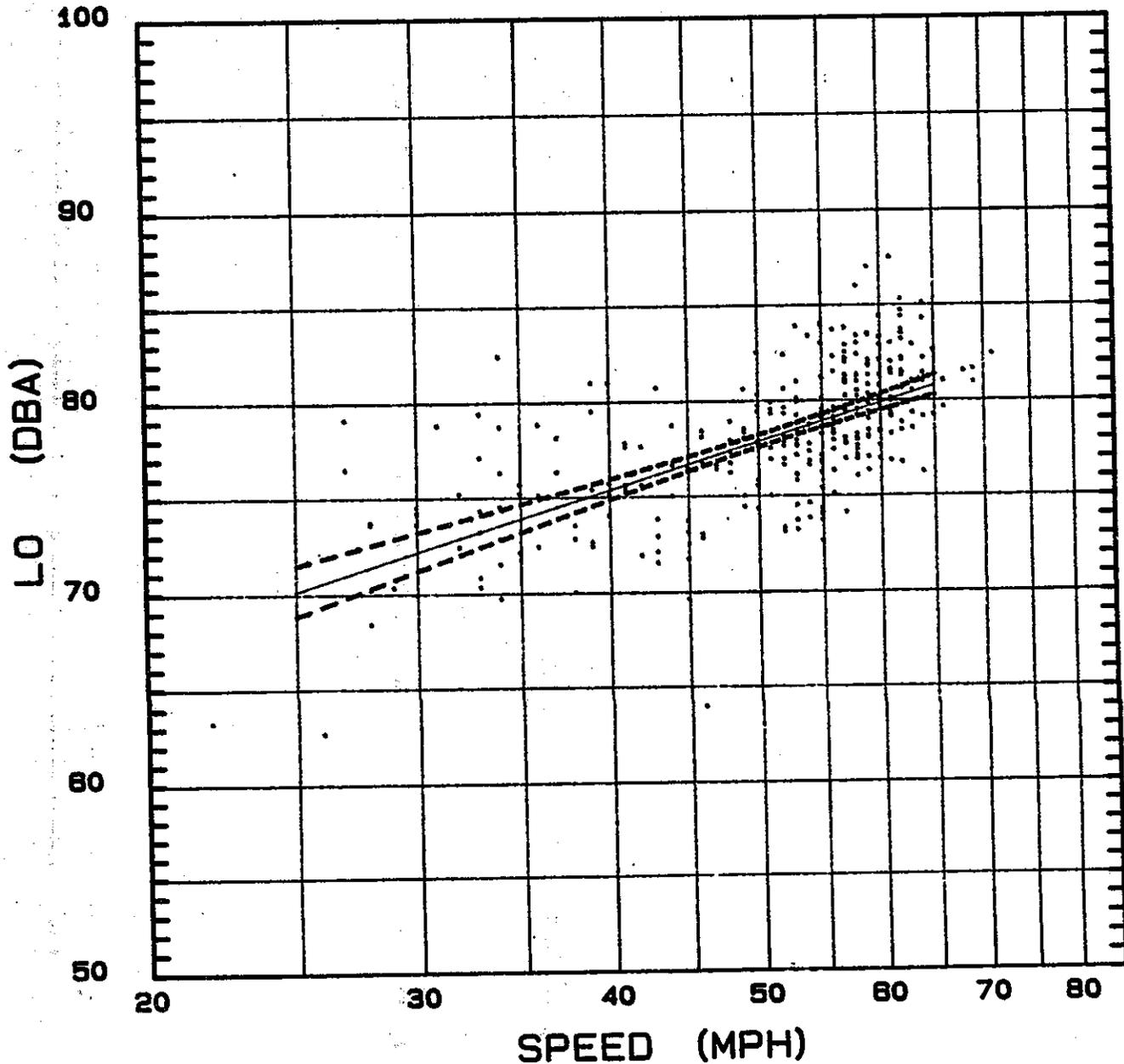
- ALL SITES -- ALL DATA POINTS
- ALL SITES  $LO = 4.31 + 38.83 \times \text{LOG}(\text{MPH})$
- - - - 95% CONFIDENCE INTERVALS FOR PREDICTION EQUATION



# CALIFORNIA VEHICLE NOISE EMISSIONS LO VS. SPEED

VEHICLE TYPE: MEDIUM TRUCKS  
MIC.#2 HT-5FT. DIST.-50FT.

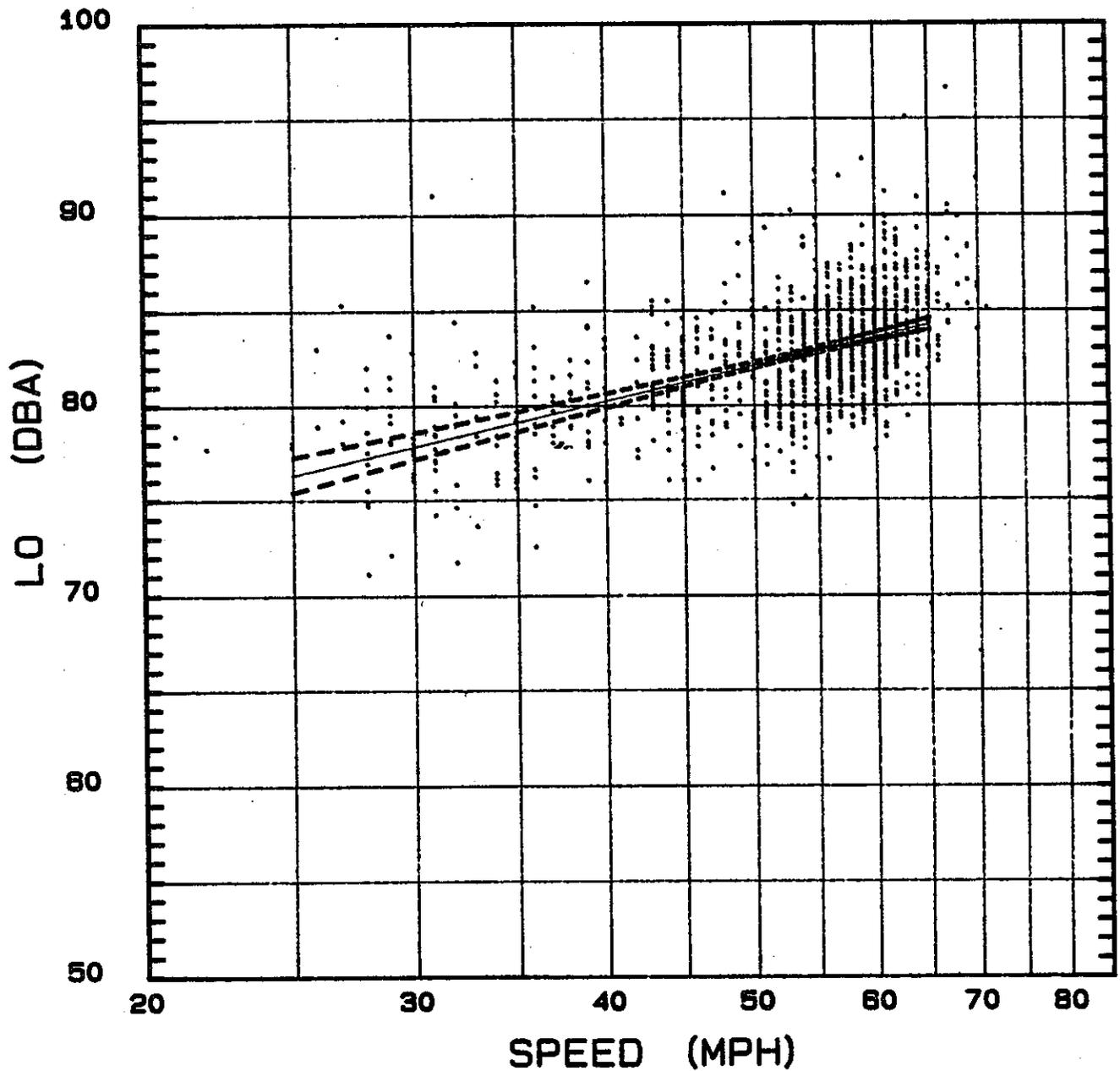
- ALL SITES -- ALL DATA POINTS
- ALL SITES  $LO = 34.42 + 25.59 * LOG(MPH)$
- - - - 95% CONFIDENCE INTERVALS FOR PREDICTION EQUATION



# CALIFORNIA VEHICLE NOISE EMISSIONS LO VS. SPEED

VEHICLE TYPE: HEAVY TRUCKS  
MIC.#2 HT-5FT. DIST-50FT.

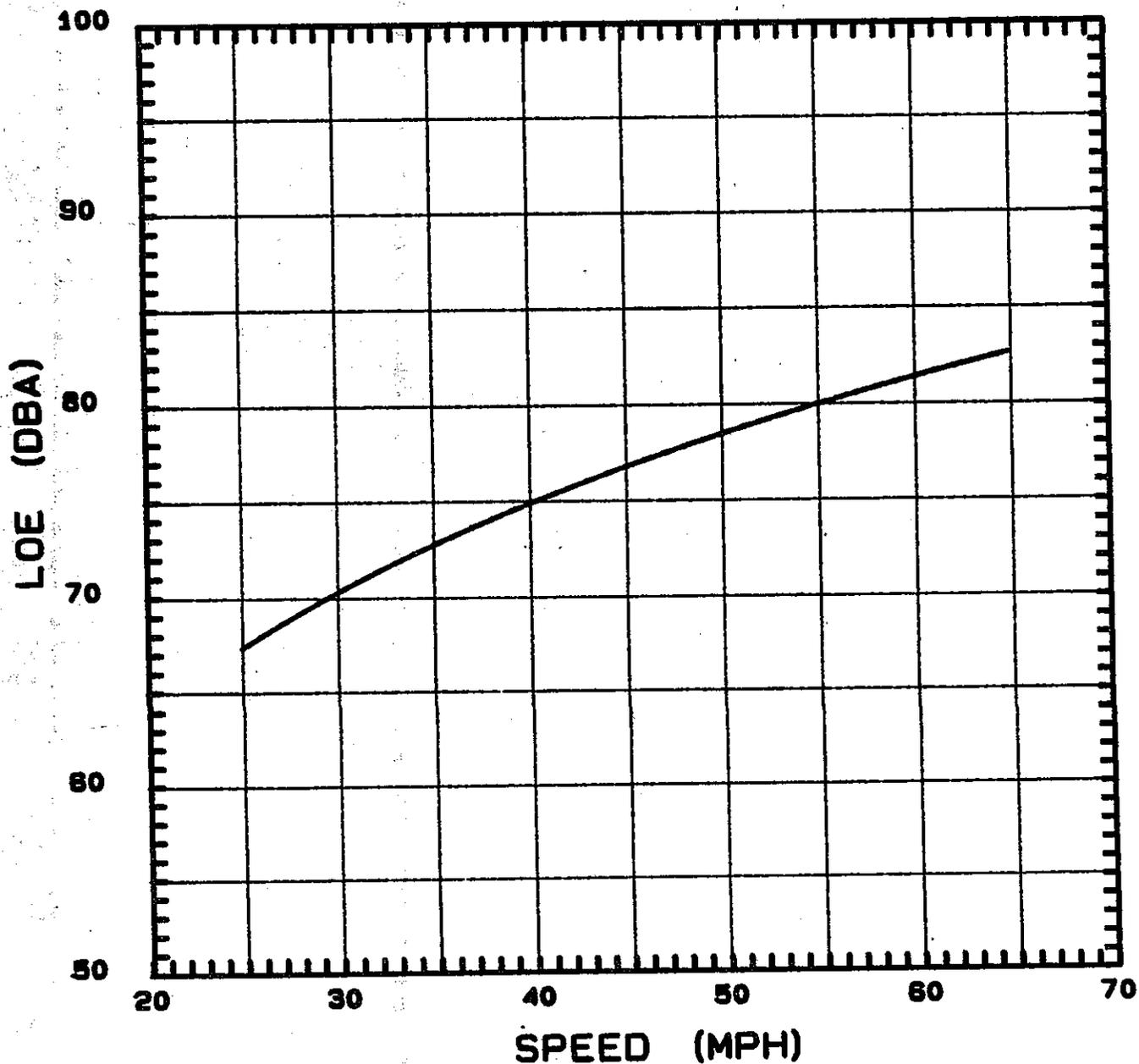
- ALL SITES -- ALL DATA POINTS
- ALL SITES  $LO = 49.54 + 19.18 * LOG(MPH)$
- - - - 95% CONFIDENCE INTERVALS FOR PREDICTION EQUATION



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

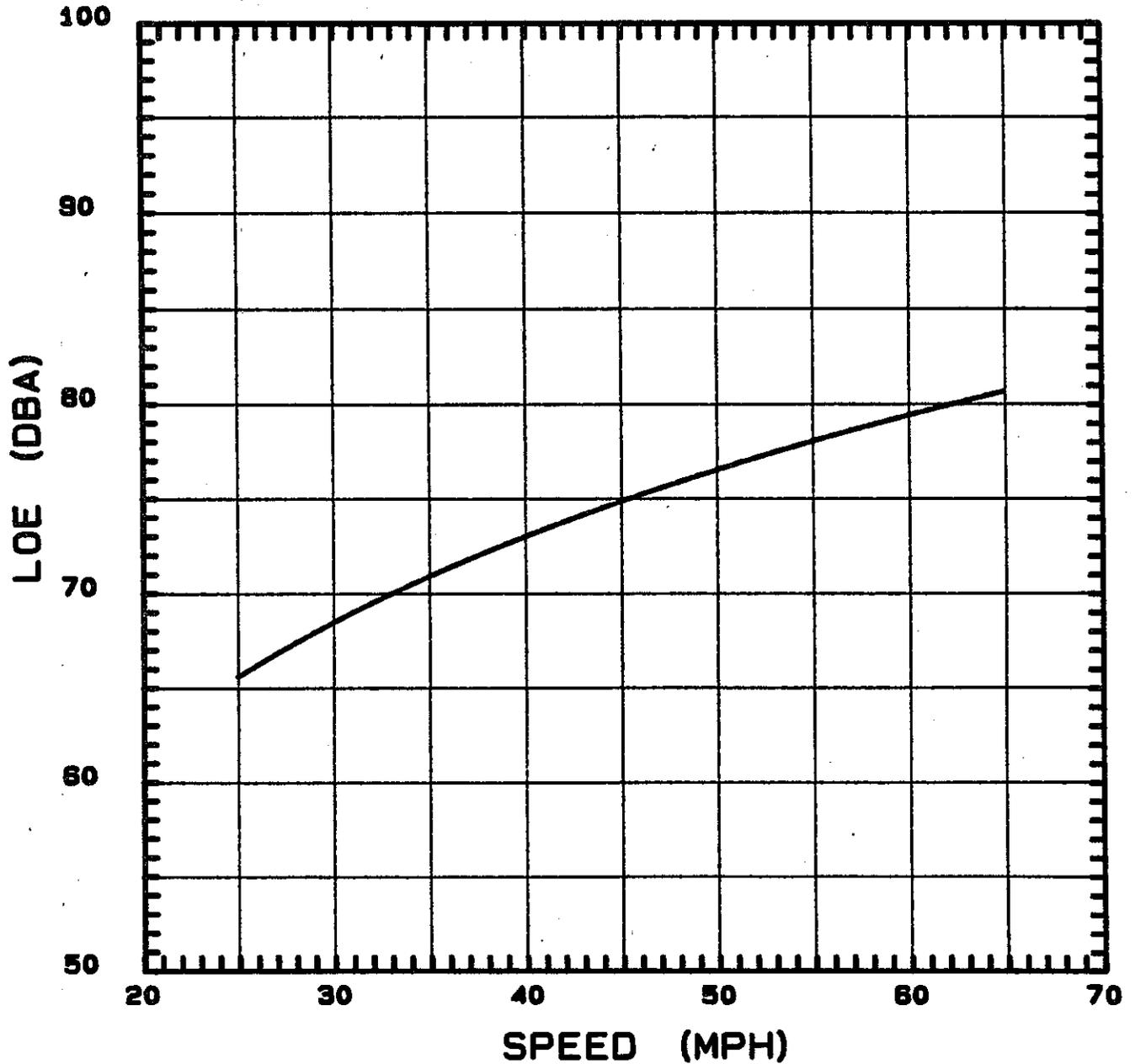
— VEH. TYPE: AUTO-STD LOE=15.88+36.83\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

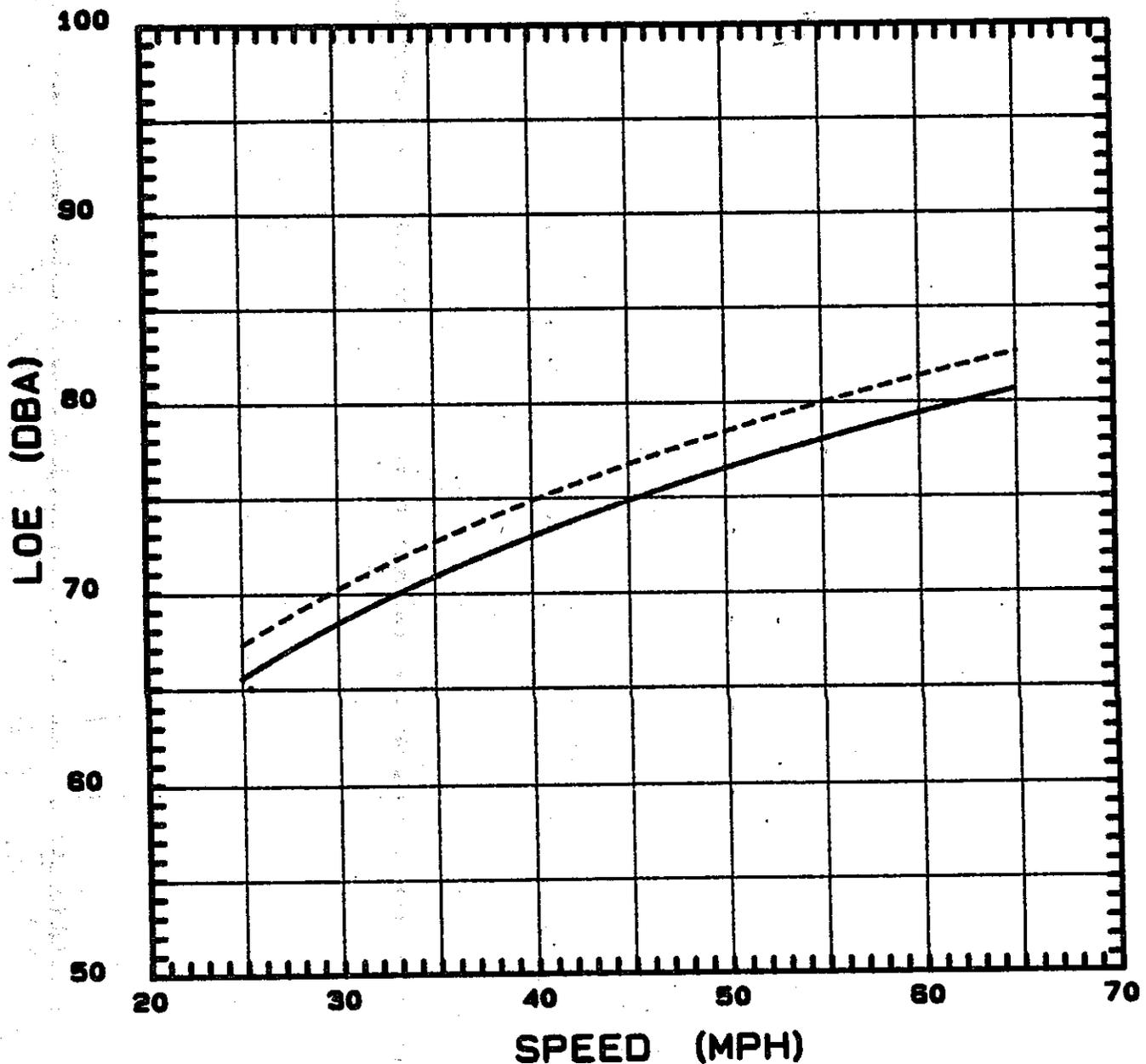
— VEH. TYPE: AUTO-COMP     $LOE = 14.75 + 36.36 * LOG(MPH)$



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

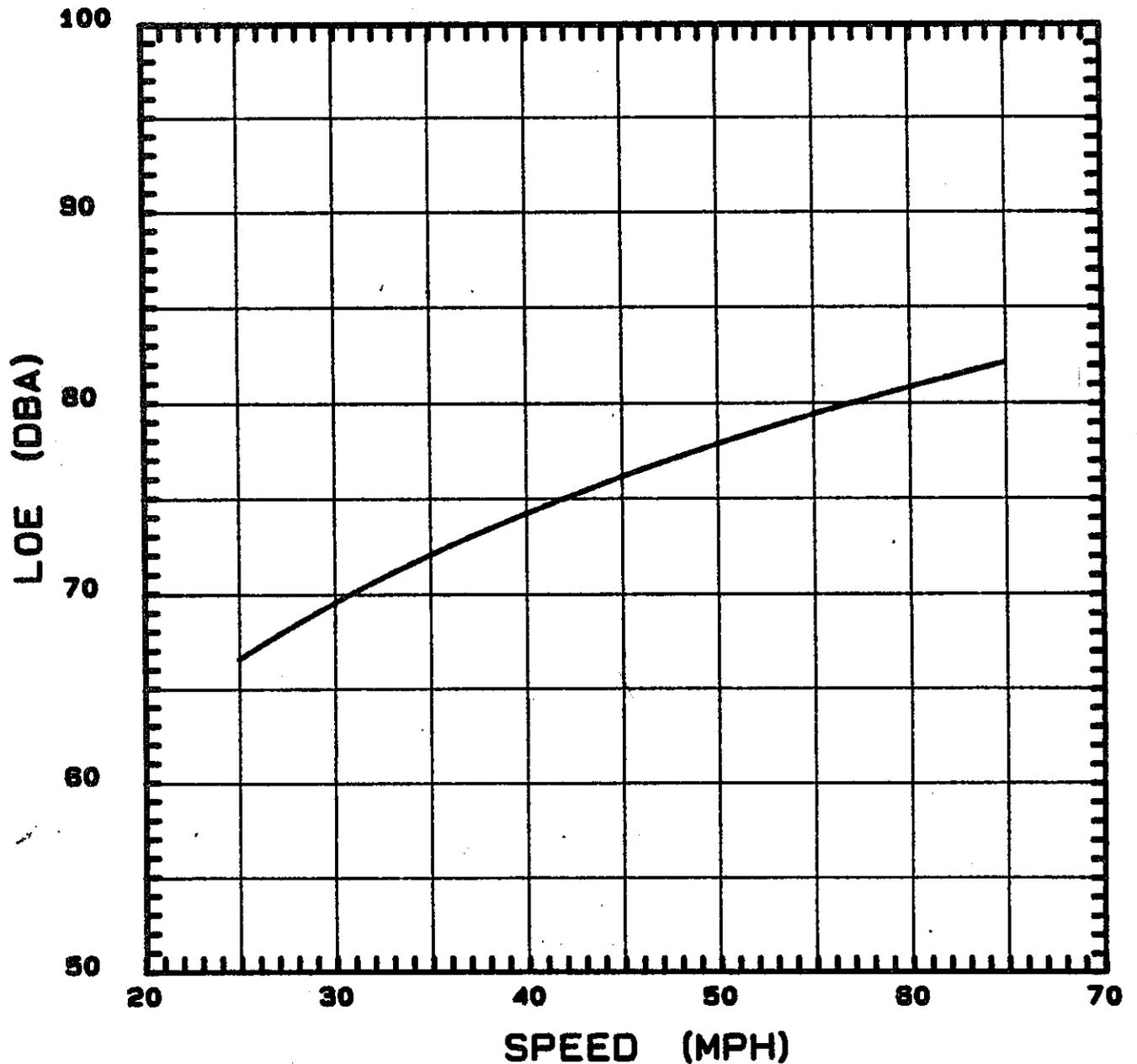
- VEH. TYPE: AUTO-COMP LOE=14.75+36.36\*LOG (MPH)  
- - - VEH. TYPE: AUTO-STD LOE=15.88+36.83\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

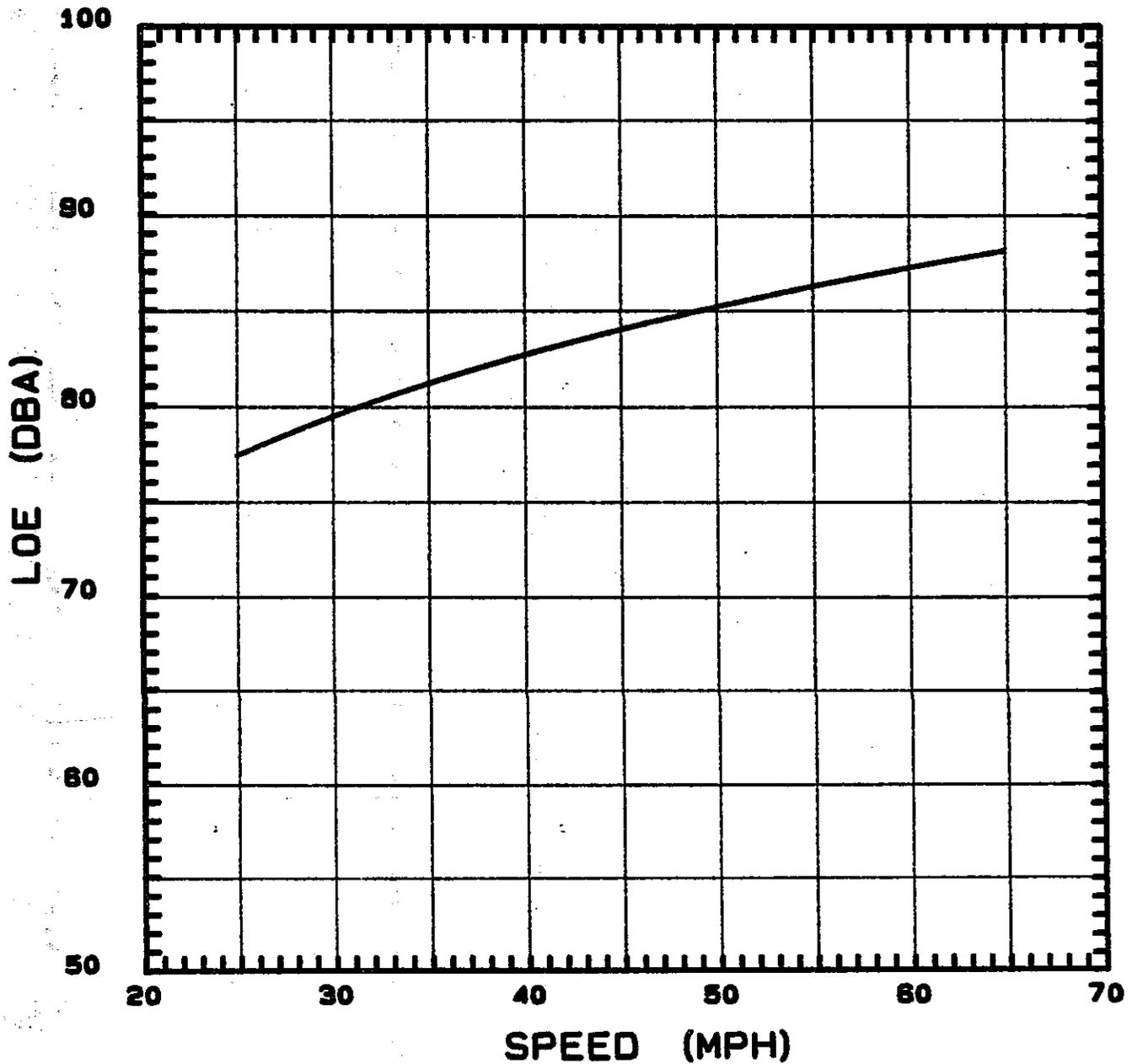
— VEH. TYPE: ALL AUTOS LOE=14.25+37.44\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

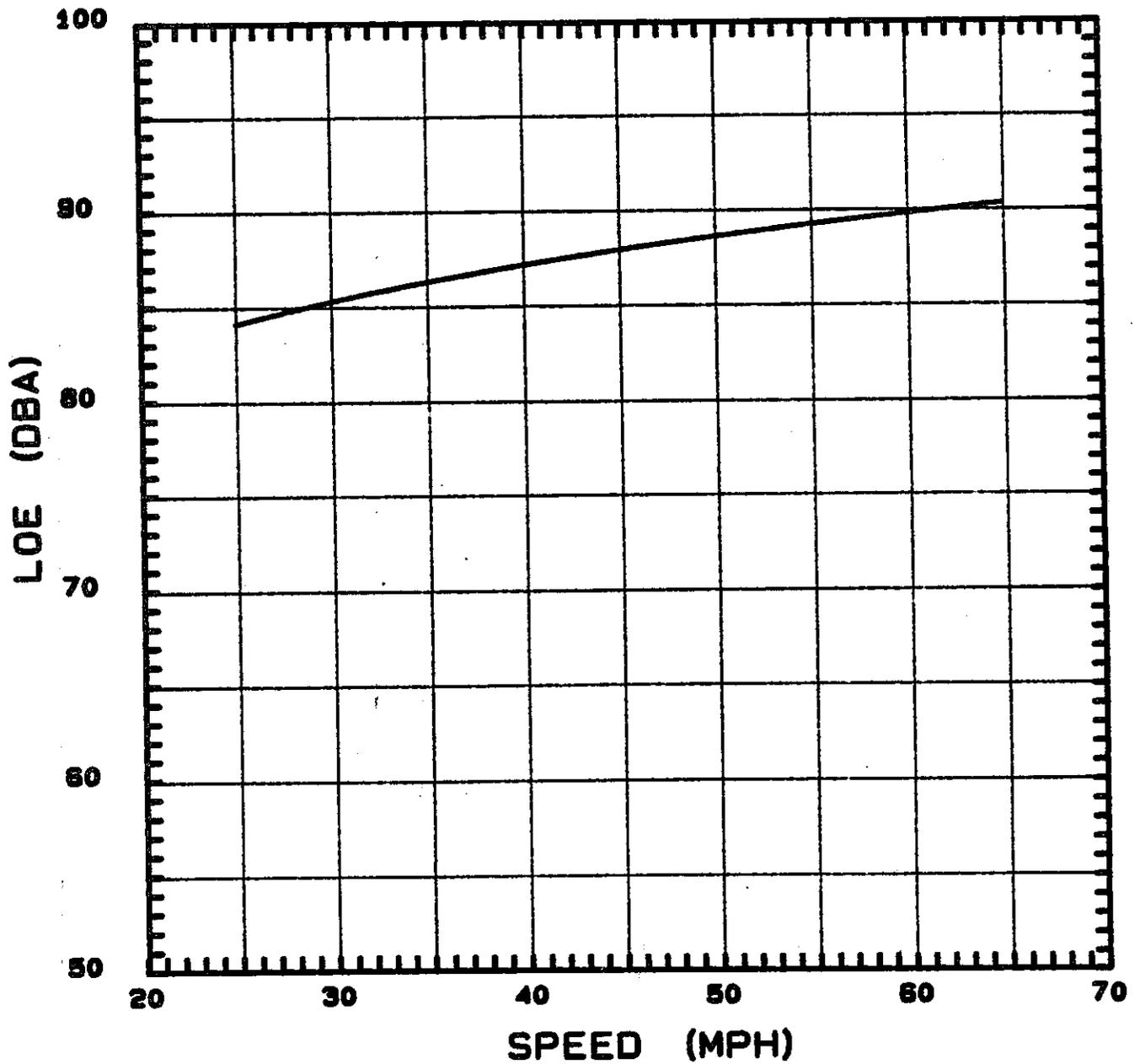
— VEH. TYPE: MEDIUM TRUCKS  $LOE=41.41+25.79 \times \text{LOG}(\text{MPH})$



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

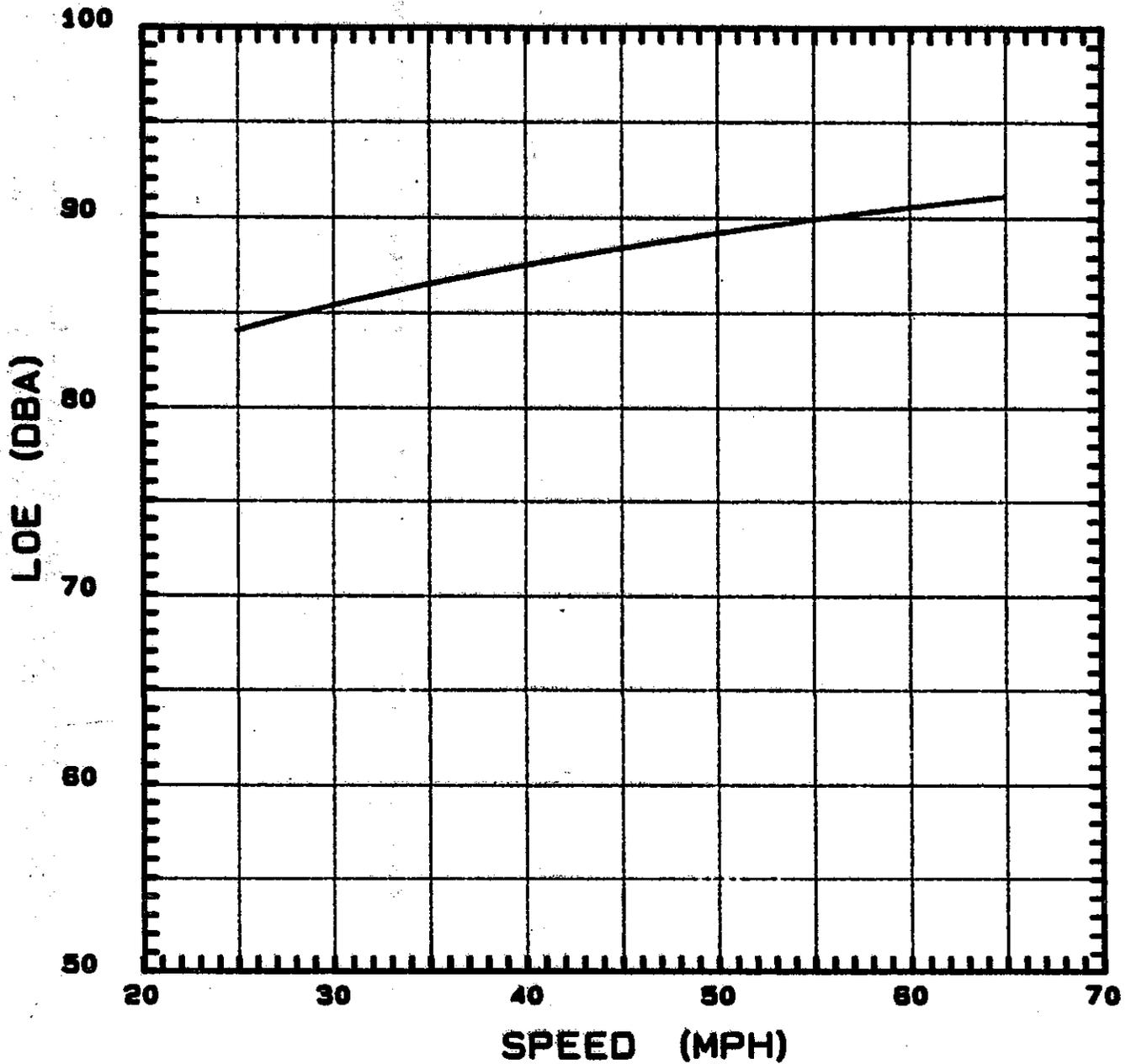
— VEH. TYPE: HT 3-AXLE LOE=63.27+14.93\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

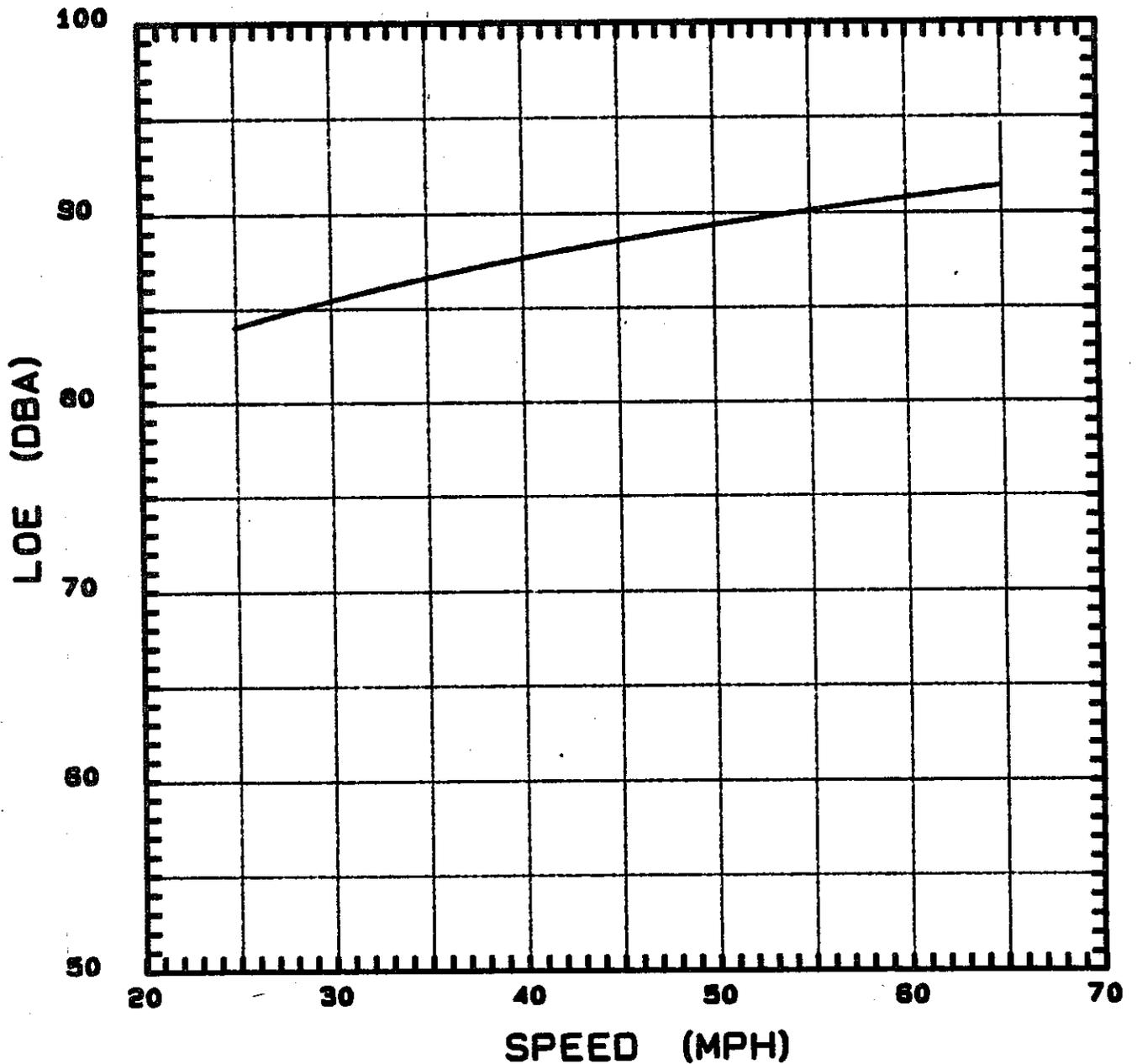
— VEH. TYPE: HT 4-AXLE LOE=60.15+17.11\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

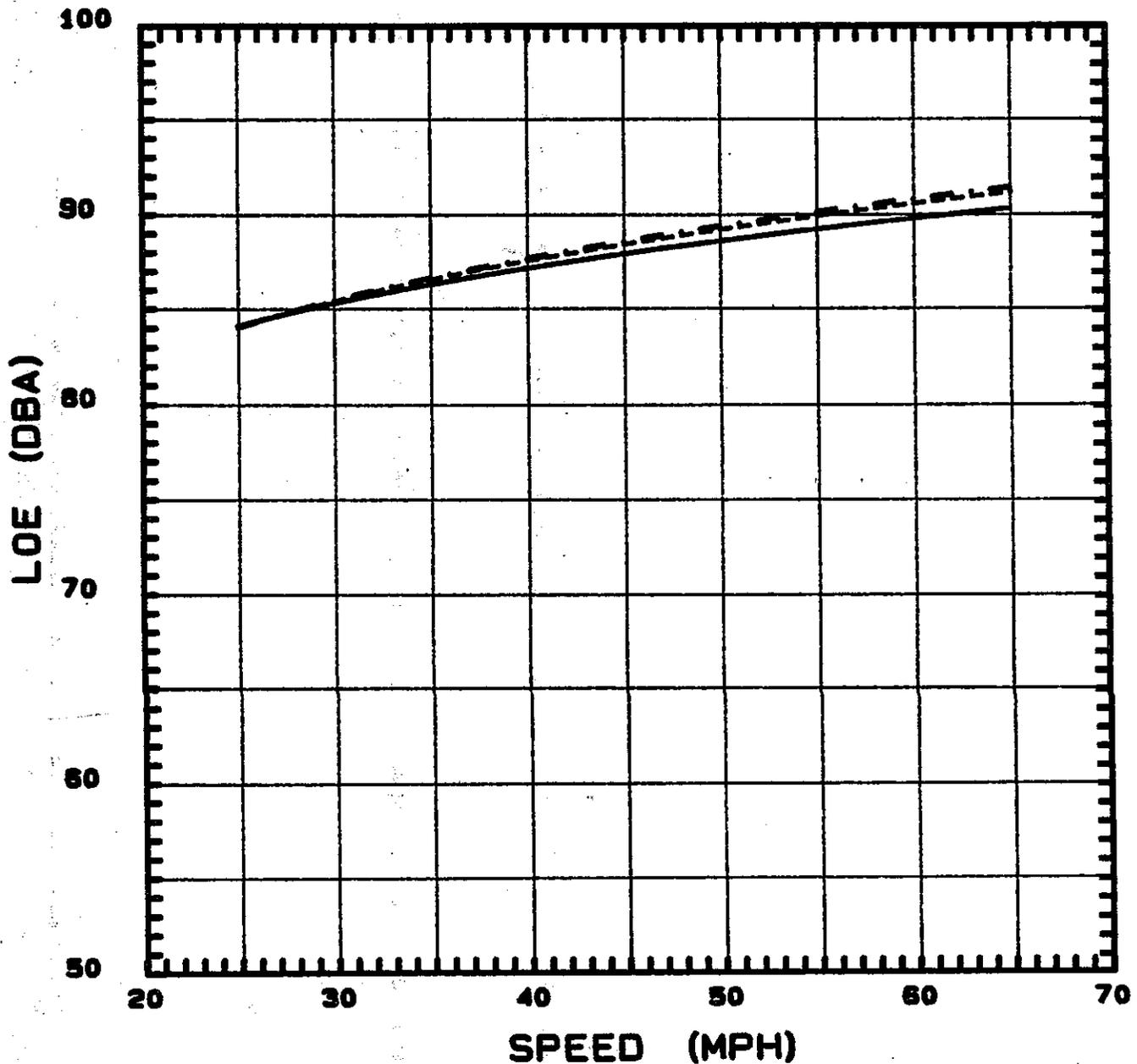
— VEH. TYPE: HT 5-AXLE . LOE=59.23+17.75\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

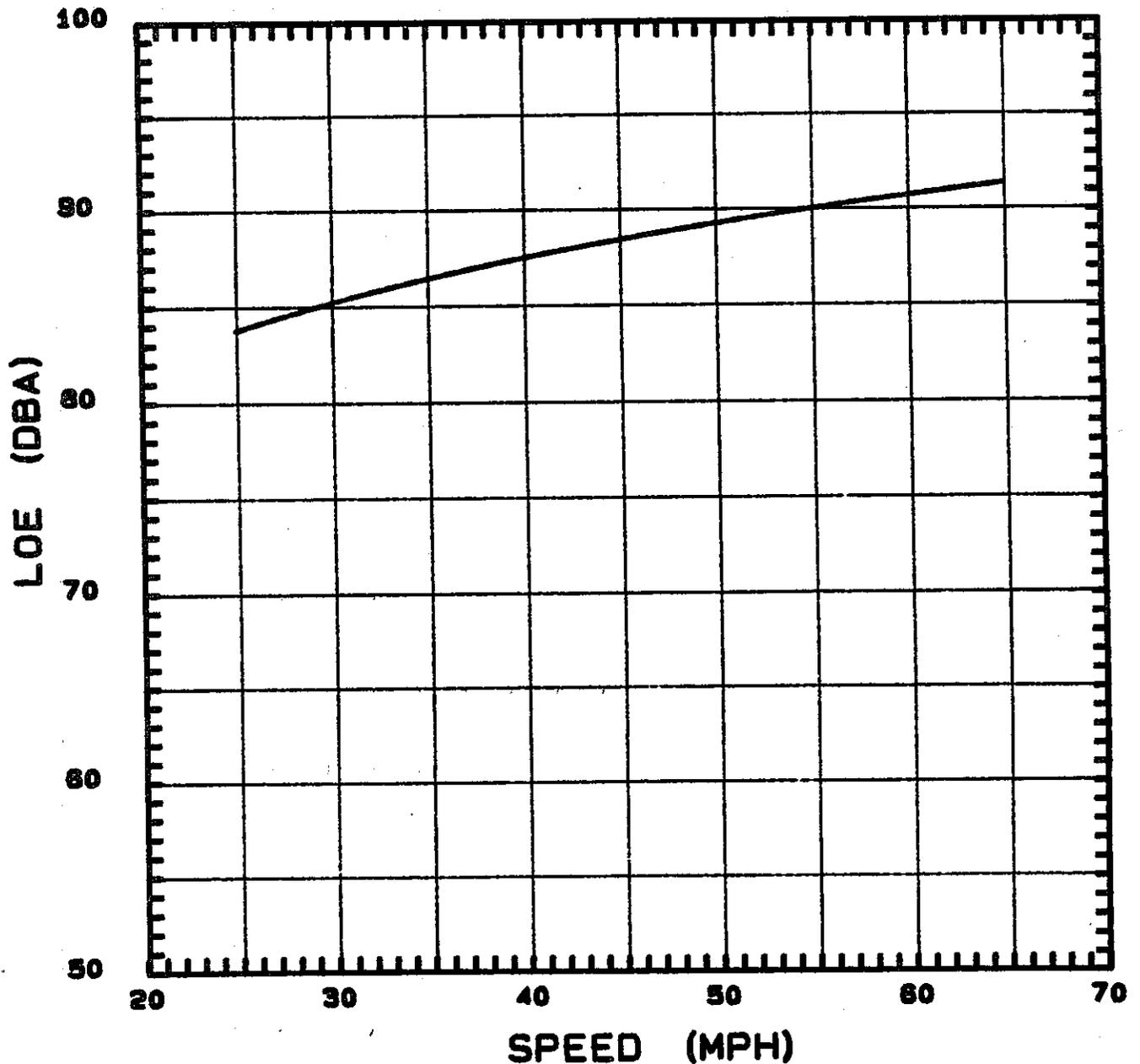
- VEH. TYPE: HT 3-AXLE     $LOE=63.27+14.93*\text{LOG}(\text{MPH})$
- - - VEH. TYPE: HT 4-AXLE     $LOE=60.15+17.11*\text{LOG}(\text{MPH})$
- · - VEH. TYPE: HT 5-AXLE     $LOE=59.23+17.75*\text{LOG}(\text{MPH})$



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#1 HT-5FT. DIST-25FT.

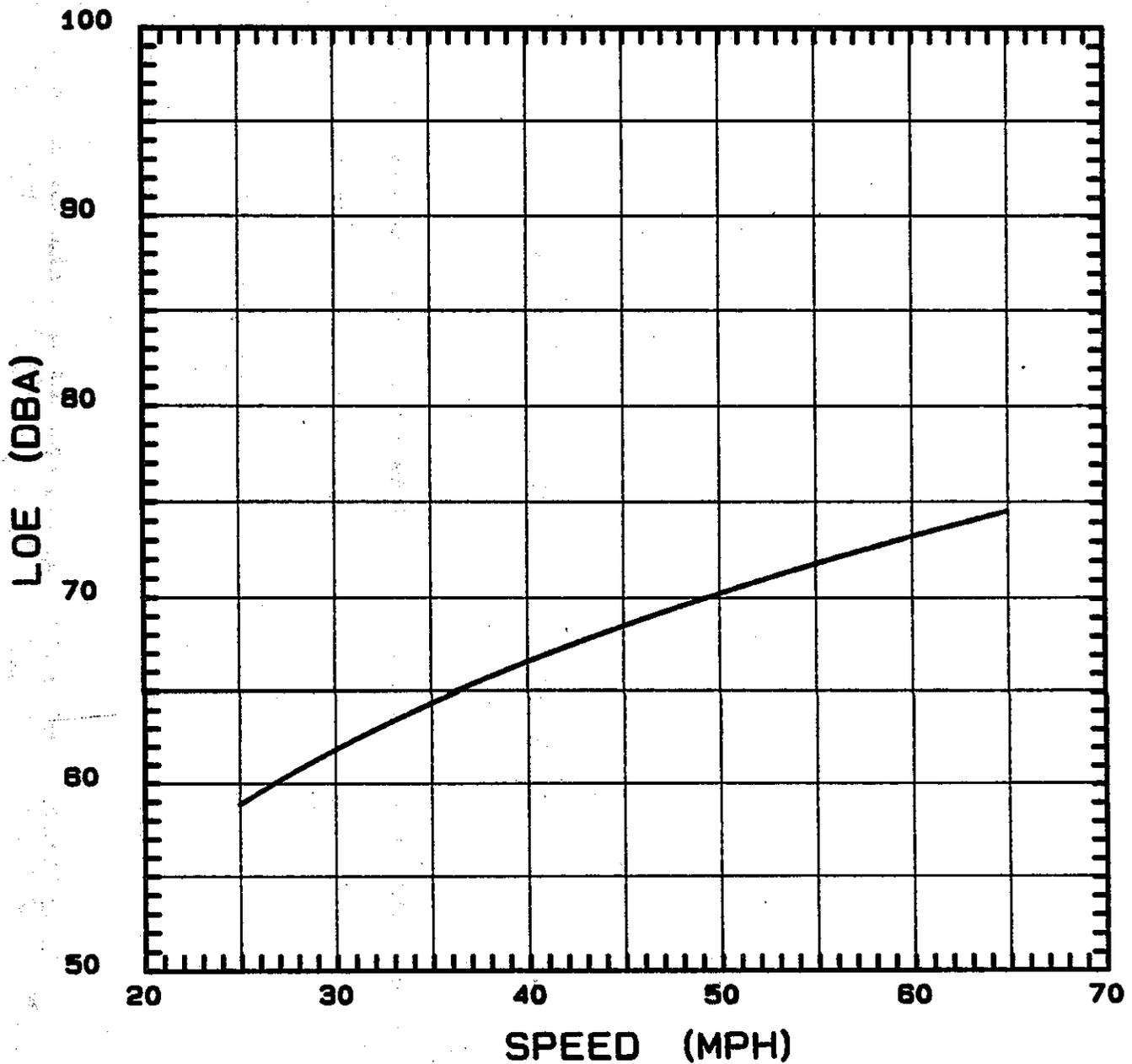
— VEH. TYPE: ALL HT  $LOE = 58.38 + 18.18 \times \text{LOG}(\text{MPH})$



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

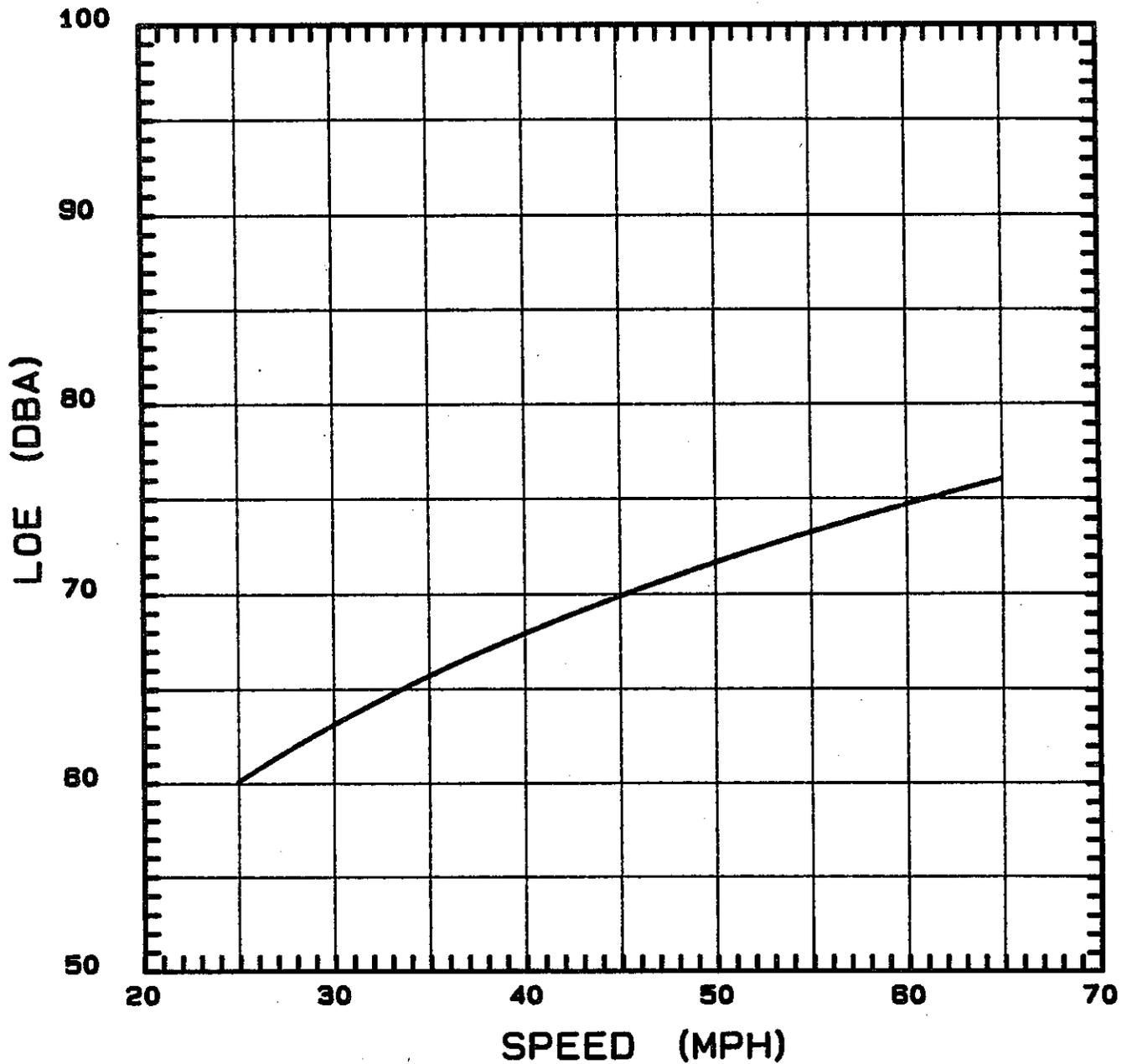
— VEH. TYPE: AUTO-COMP LOE=6+37.79\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

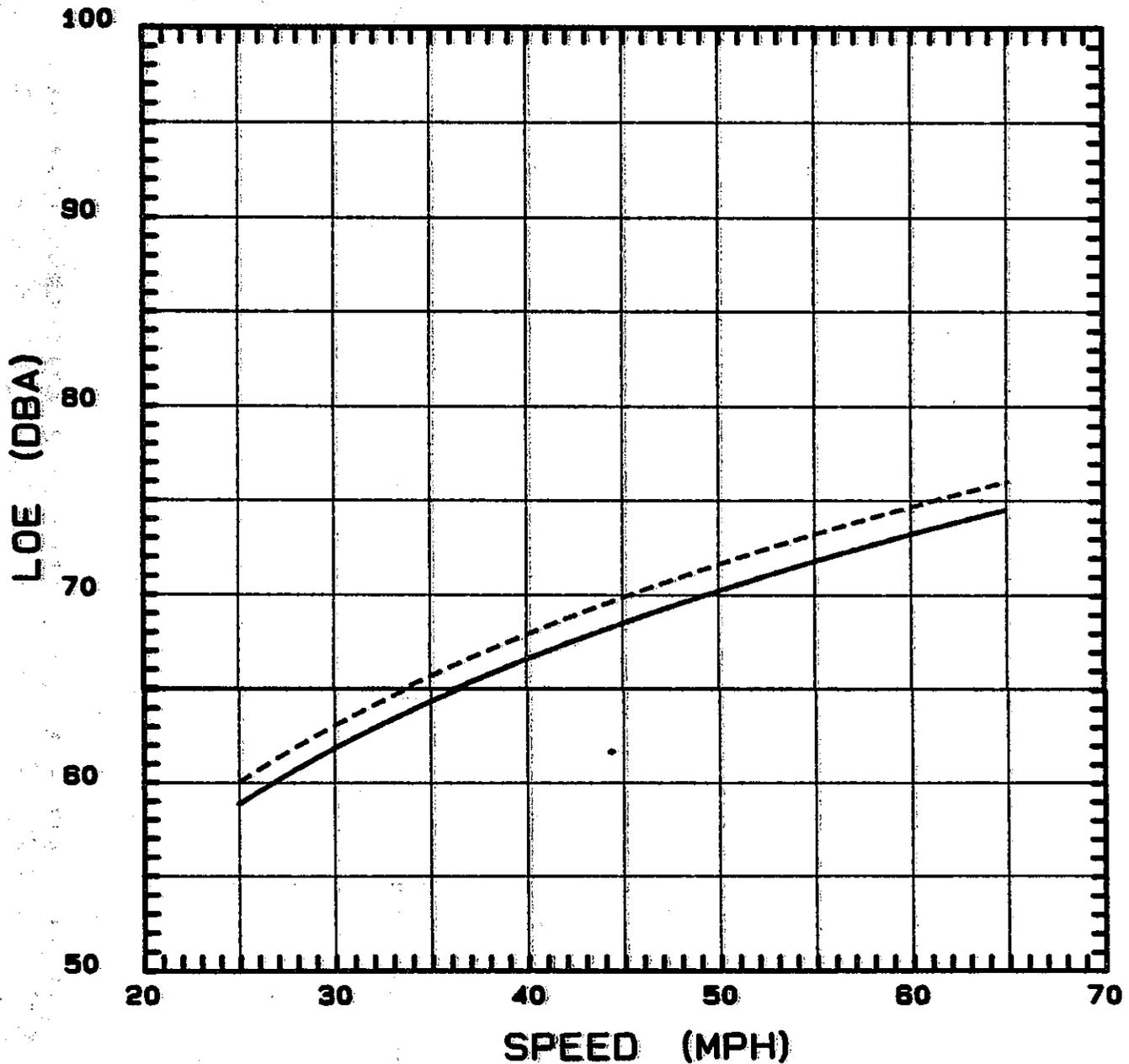
— VEH. TYPE: AUTO-STD LOE=6.28+38.47\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

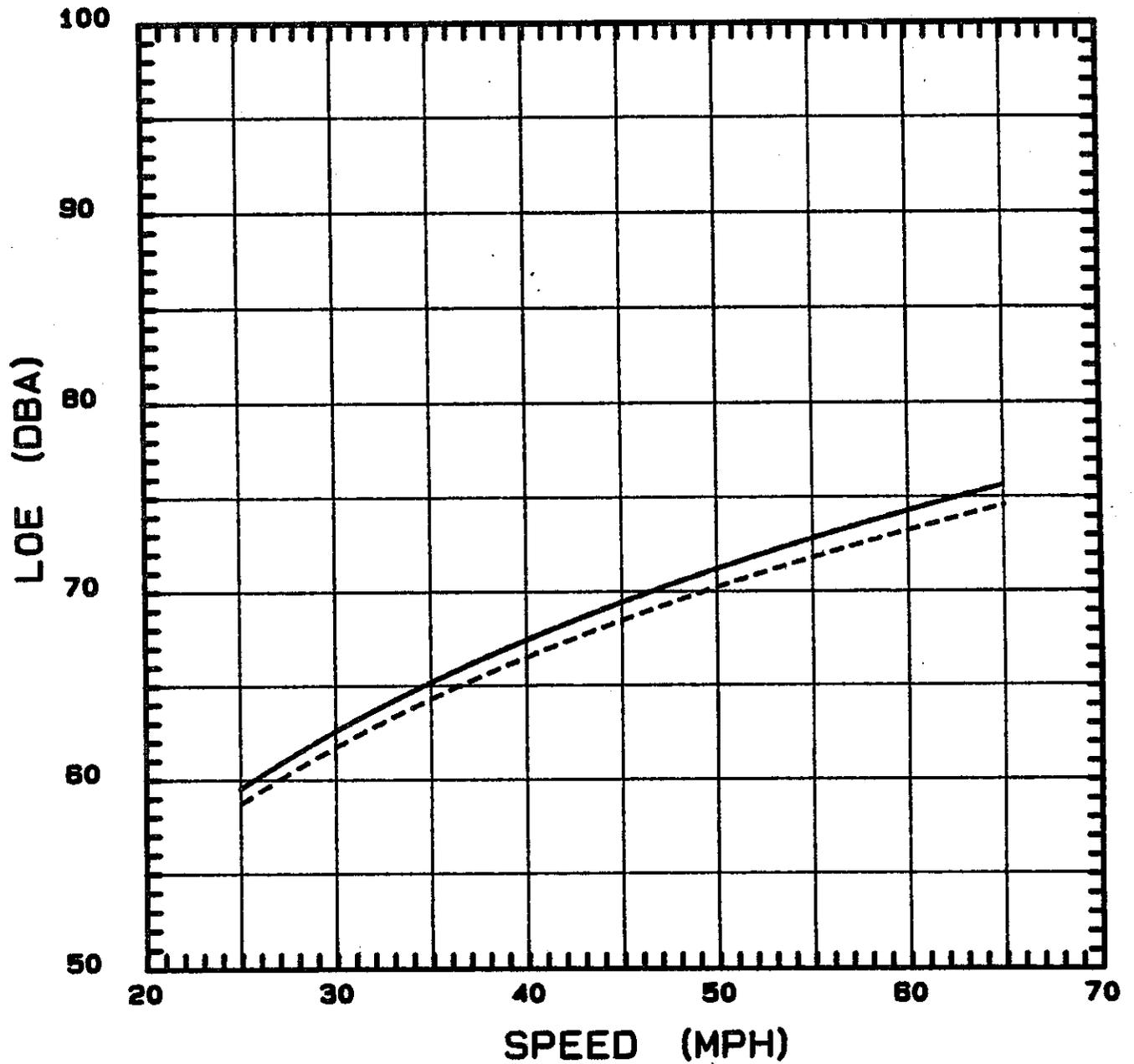
- VEH. TYPE: AUTO-COMP LOE=6+37.79\*LOG (MPH)  
- - - VEH. TYPE: AUTO-STD LOE=6.28+38.47\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

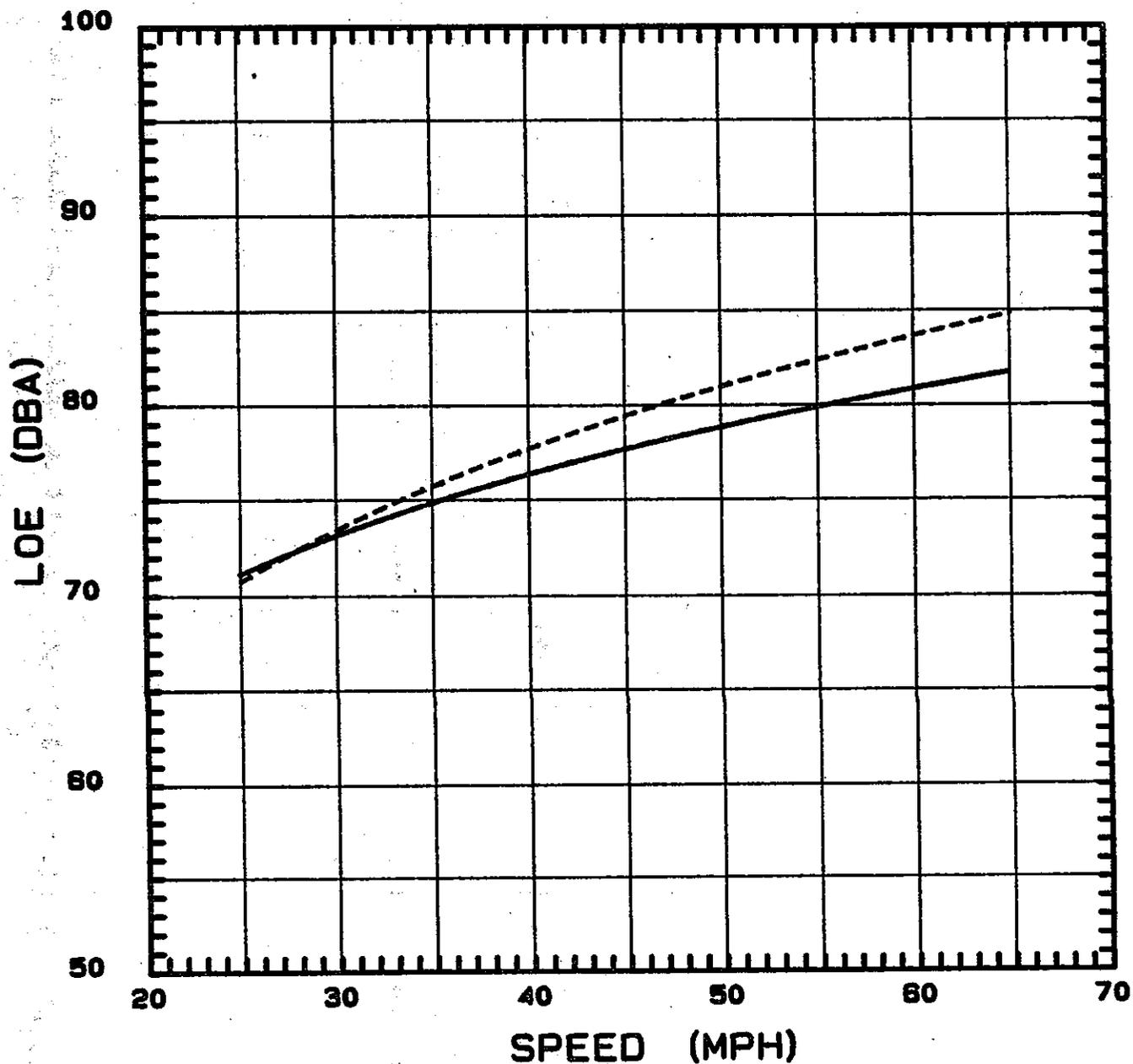
- VEH. TYPE: ALL AUTOS LOE=5.21+38.83\*LOG (MPH)  
- - - VEH. TYPE: FHWA AUTOS LOE=5.5+38.1\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

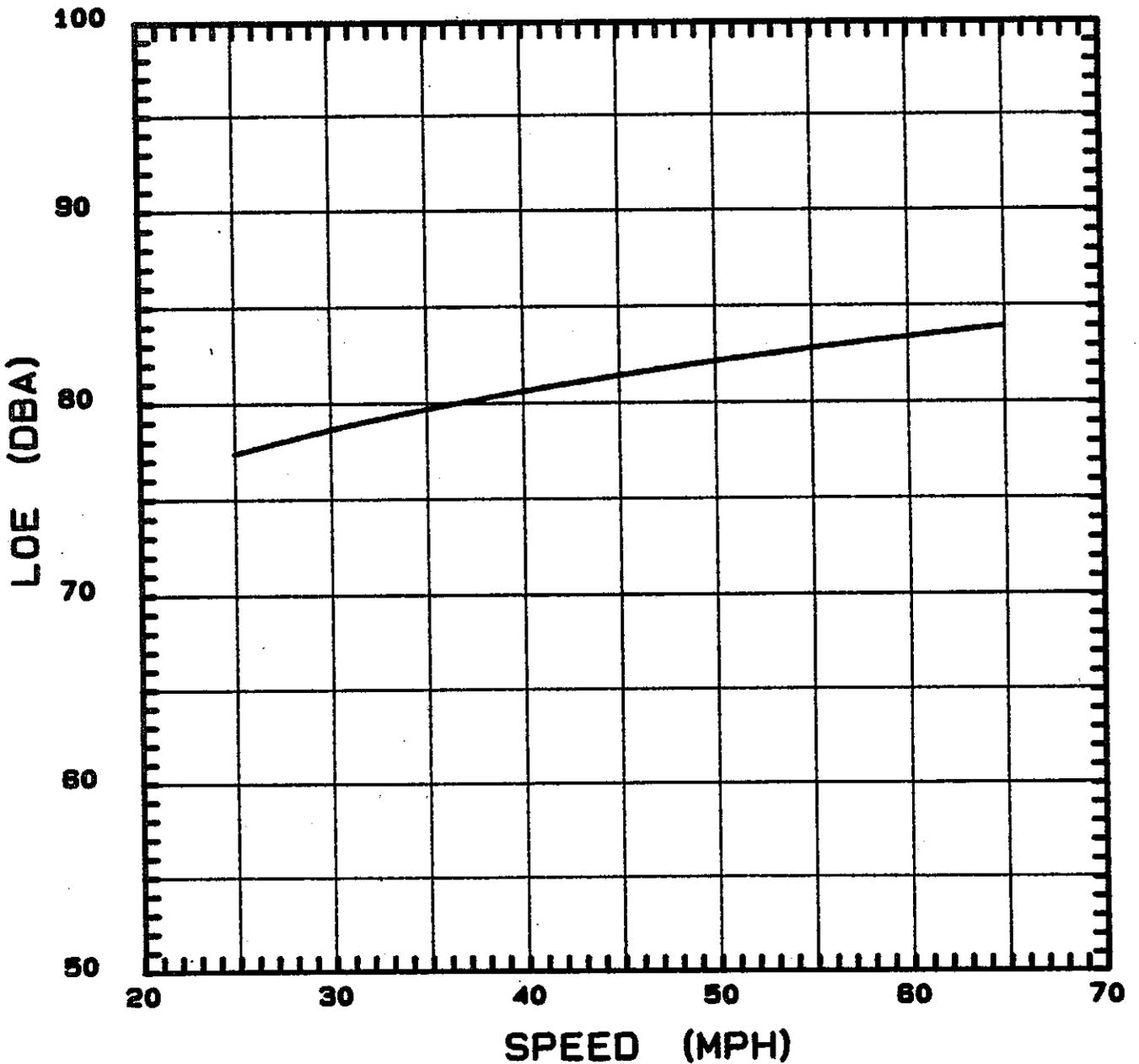
- VEH. TYPE: MEDIUM TRUCKS LOE=35.34+25.59\*LOG (MPH)  
- - - VEH. TYPE: FHWA MT LOE=23.4+33.9\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

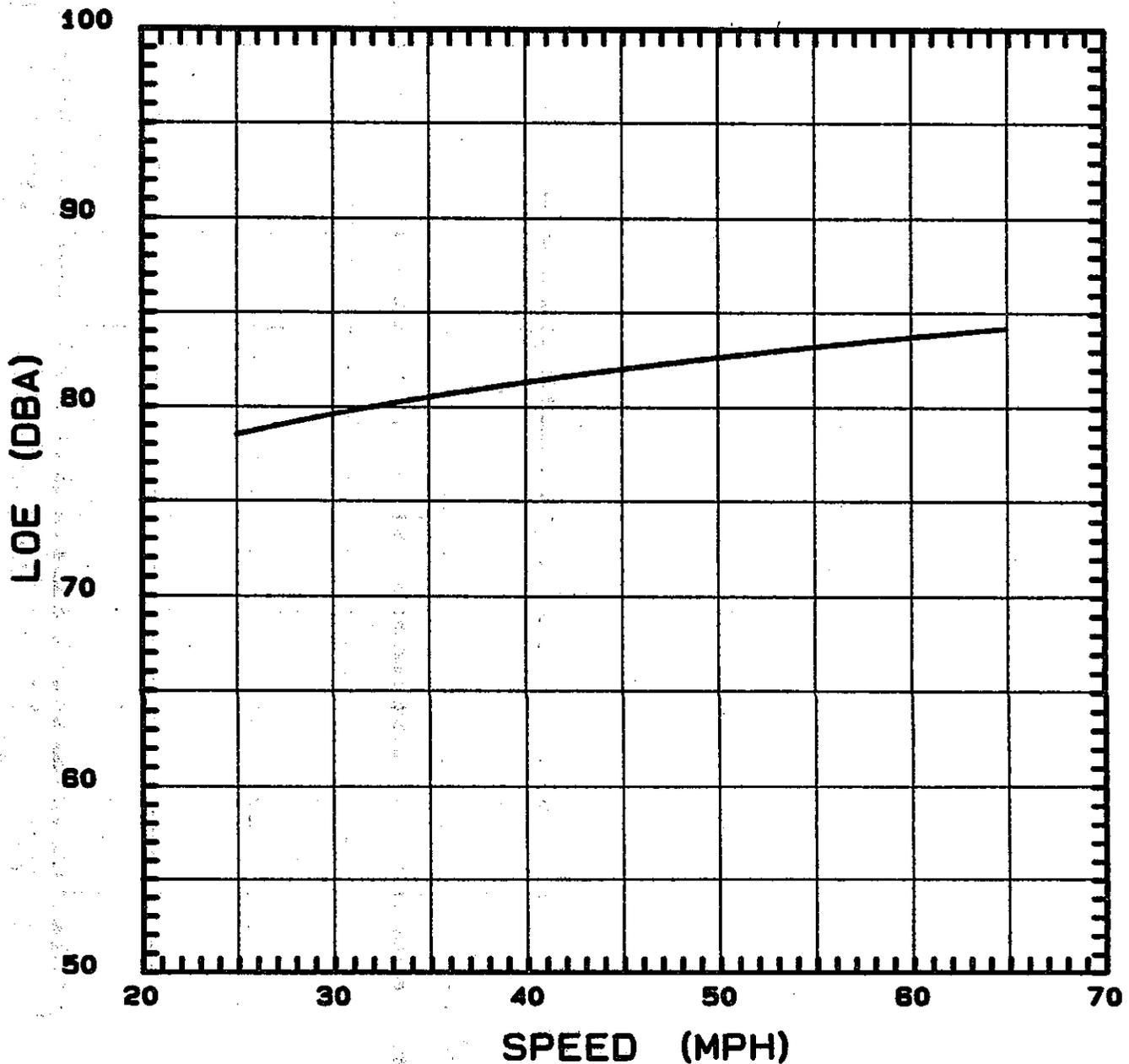
— VEH. TYPE: HT 3-AXLE LOE=55.28+15.8\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

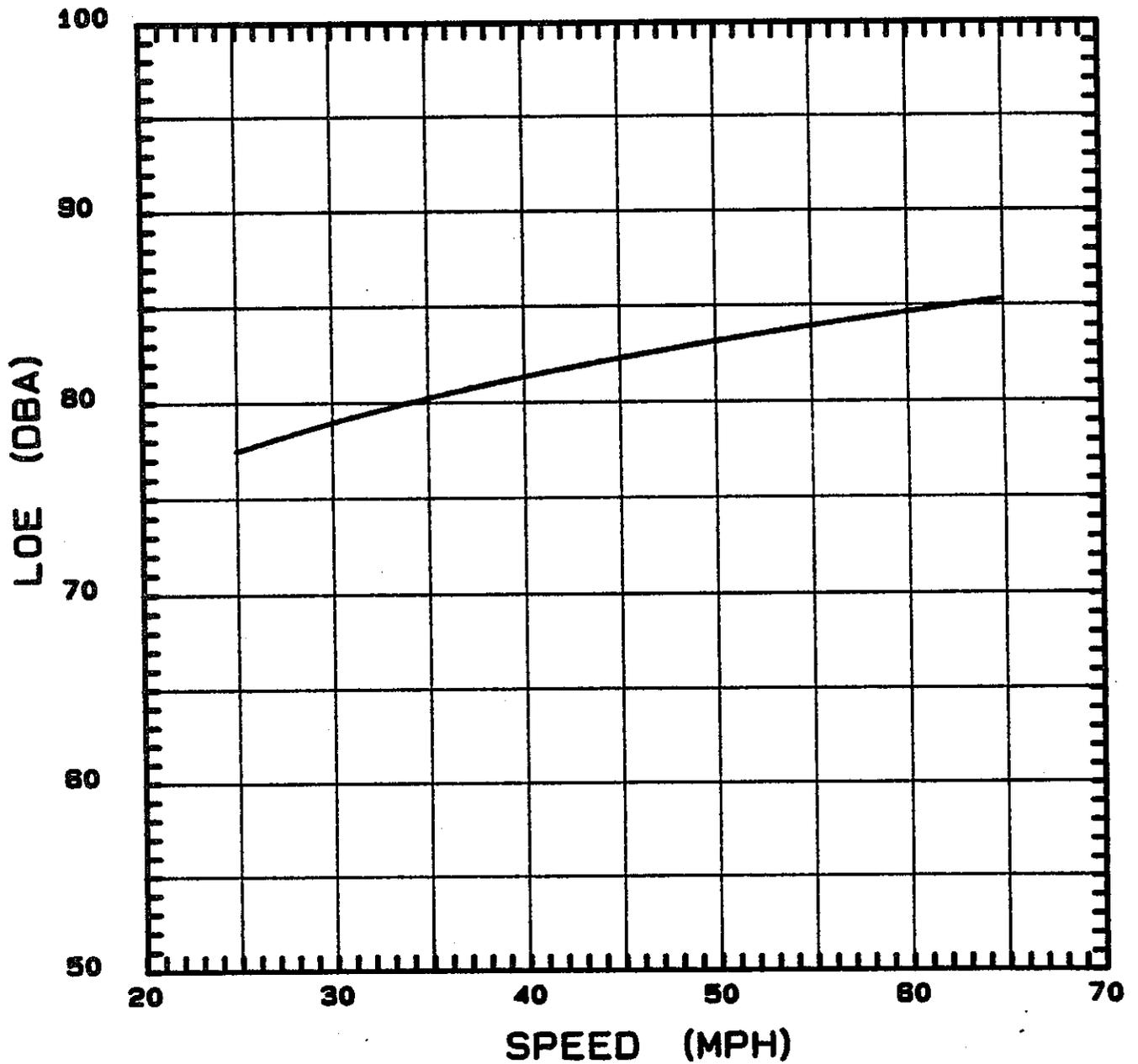
— VEH. TYPE: HT 4-AXLE  $LOE=59.37+13.69 \times \text{LOG}(\text{MPH})$



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

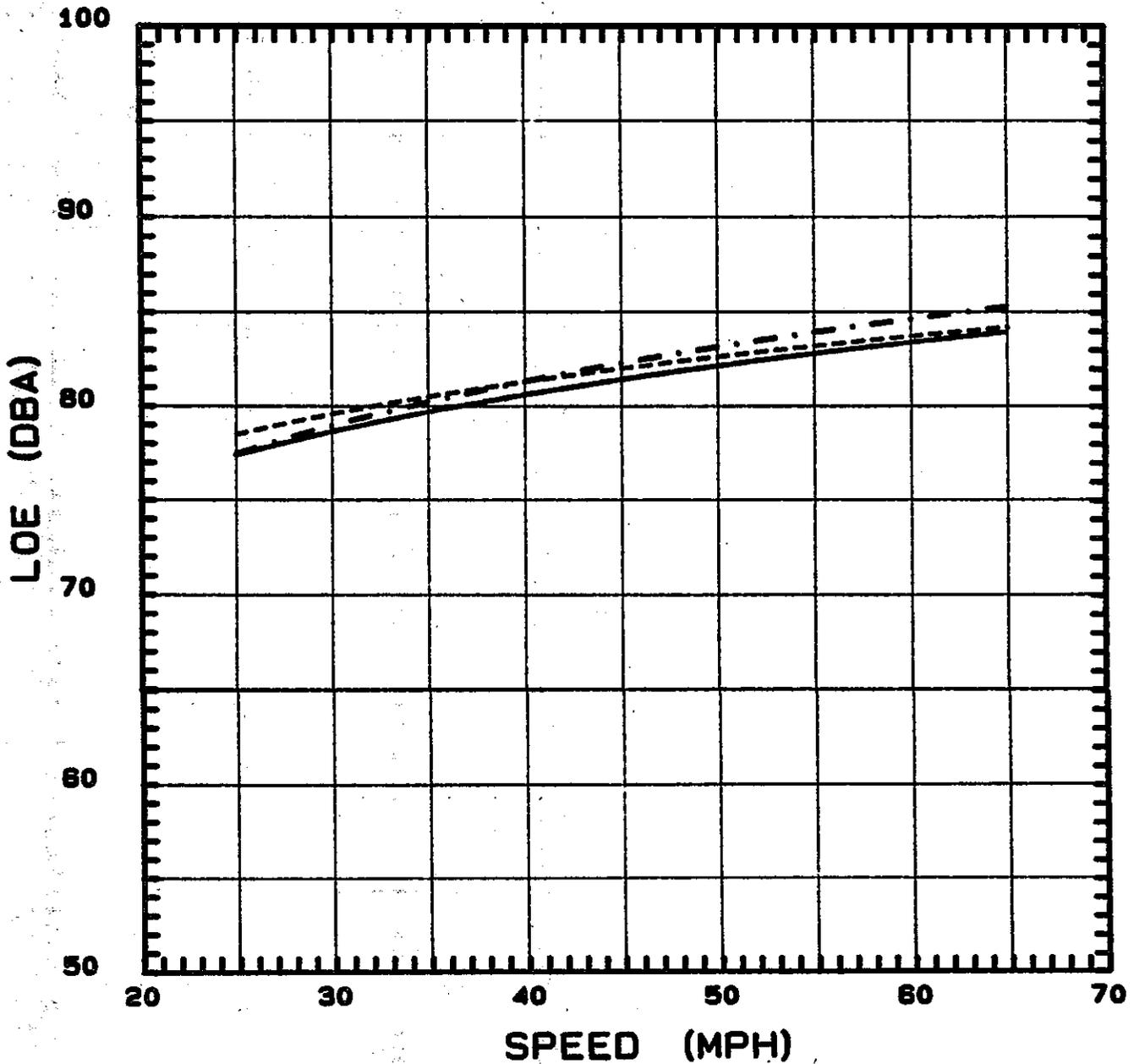
— VEH. TYPE: HT 5-AXLE LOE=51.06+18.88\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

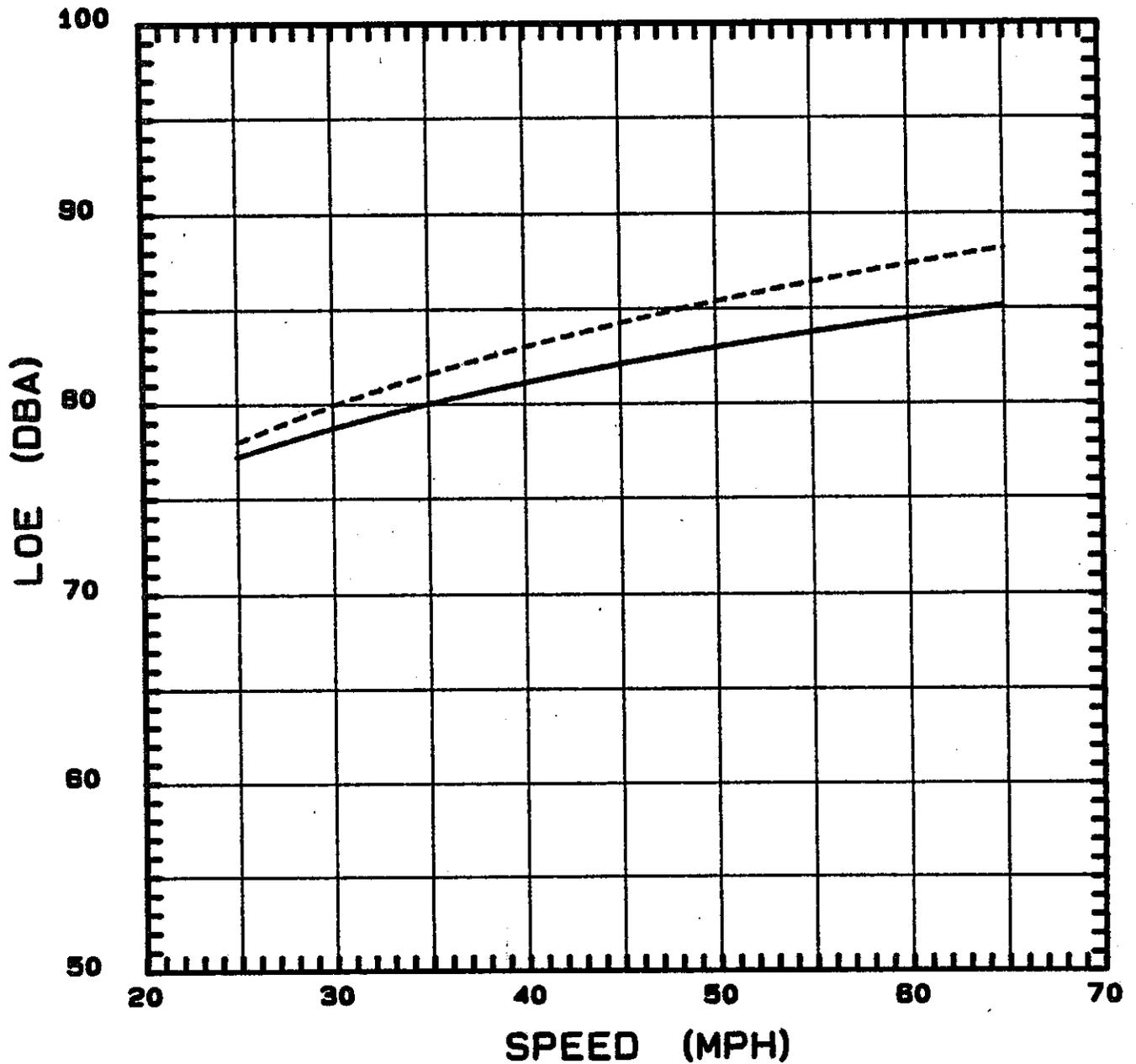
- VEH. TYPE: HT 3-AXLE LOE=55.28+15.8\*LOG (MPH)
- - - VEH. TYPE: HT 4-AXLE LOE=59.37+13.69\*LOG (MPH)
- · - · VEH. TYPE: HT 5-AXLE LOE=51.06+18.88\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#2 HT-5FT. DIST-50FT.

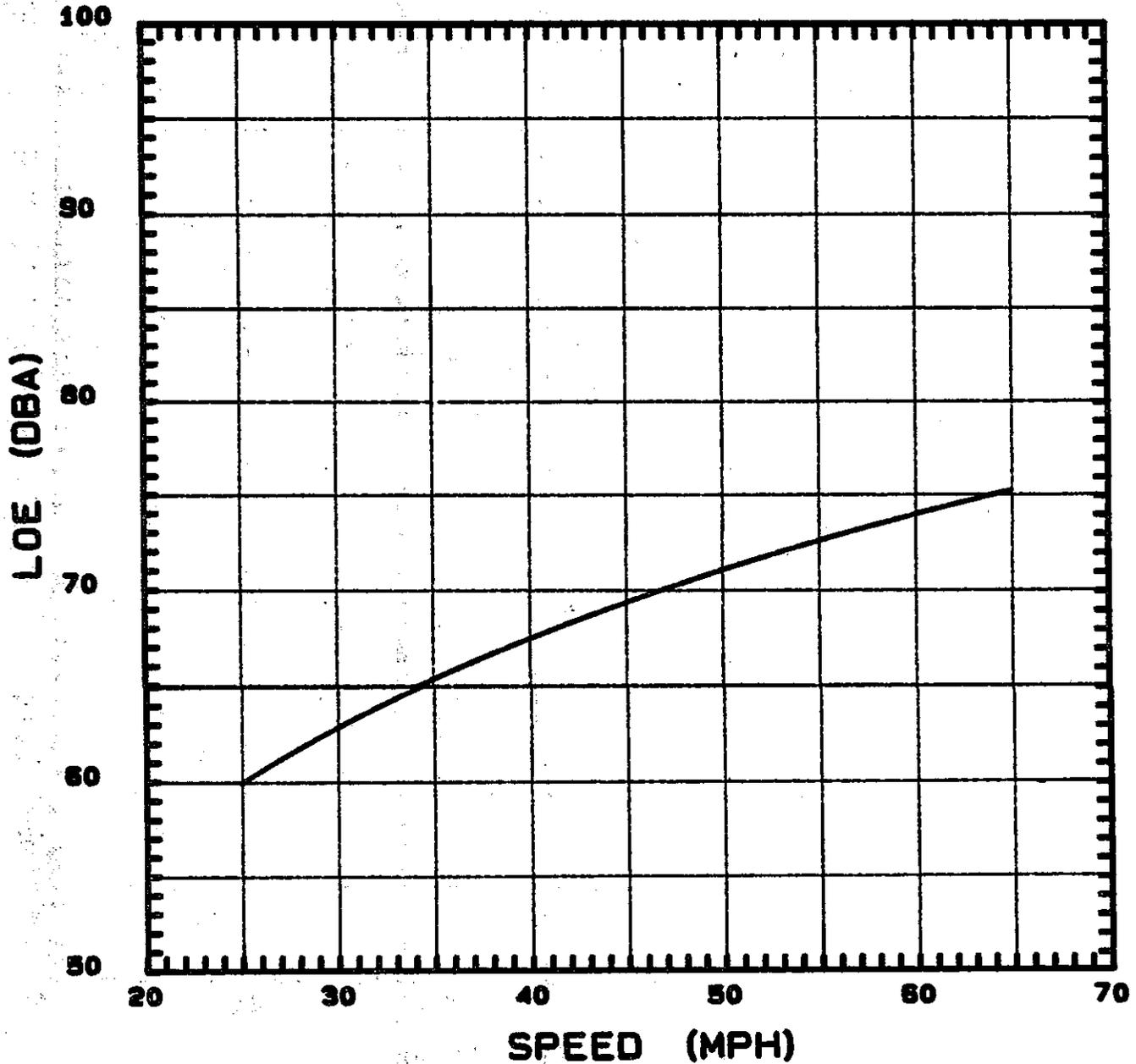
— VEH. TYPE: ALL HT     $LOE=50.37+19.18 \times \text{LOG}(\text{MPH})$   
- - - VEH. TYPE: FHWA HT     $LOE=43.6+24.6 \times \text{LOG}(\text{MPH})$



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

— VEH. TYPE: AUTO-COMP LOE=8.37+36.9\*LOG (MPH)

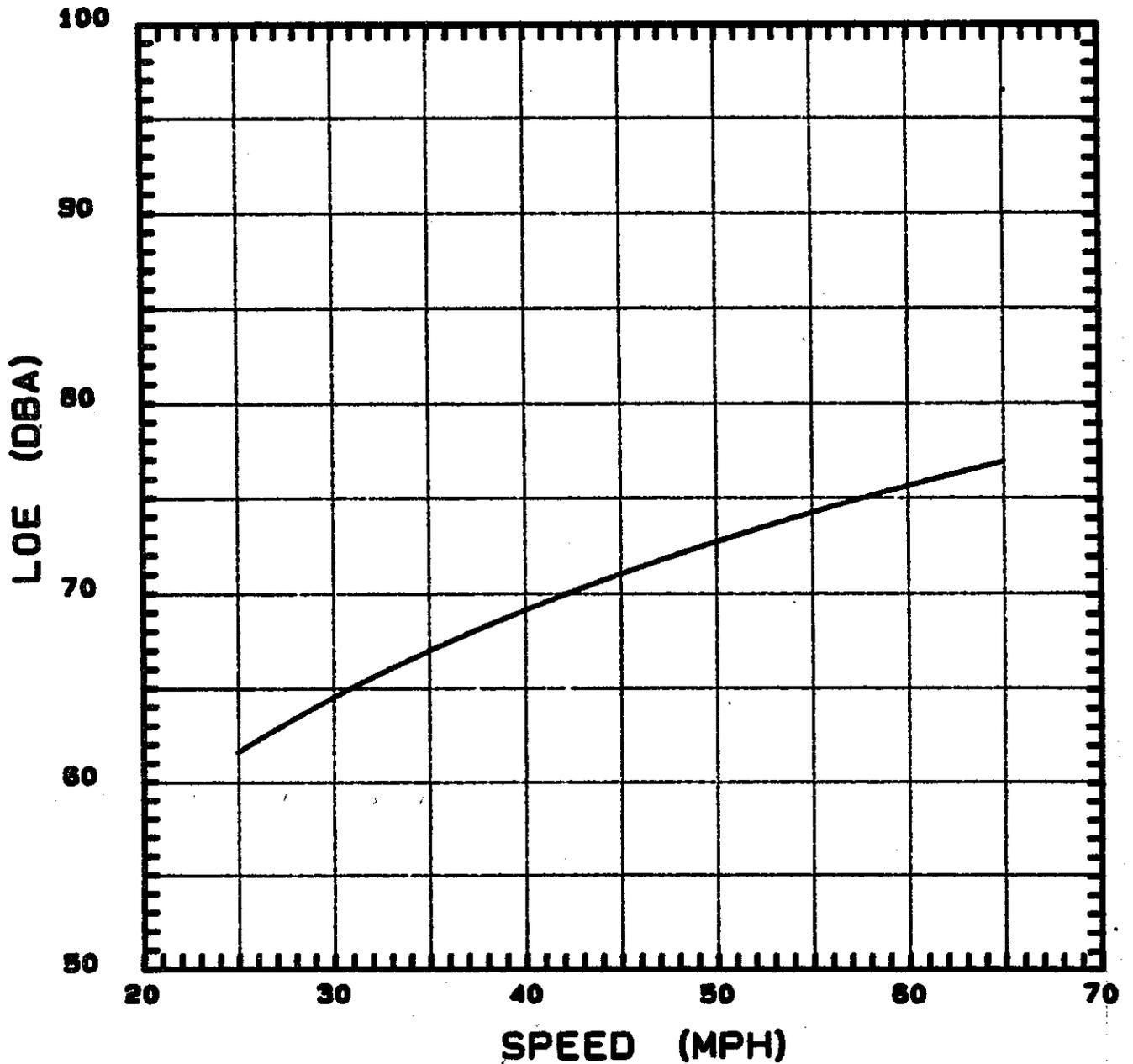


D-48

# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

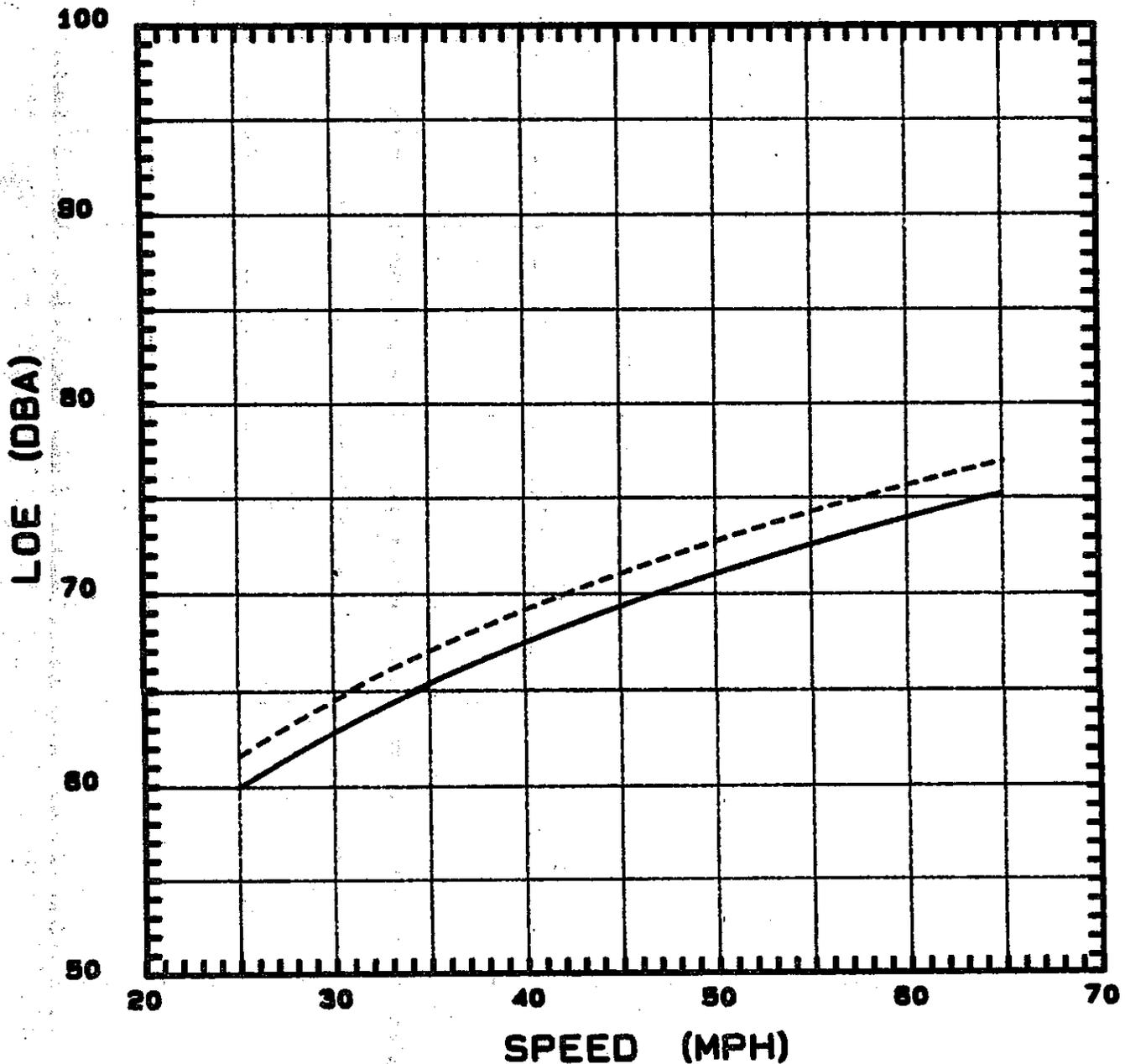
— VEH. TYPE: AUTO-STD LOE=10.06+36.89\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

— VEH. TYPE: AUTO-COMP LOE=8.37+36.9\*LOG (MPH)  
- - - VEH. TYPE: AUTO-STD LOE=10.06+36.89\*LOG (MPH)

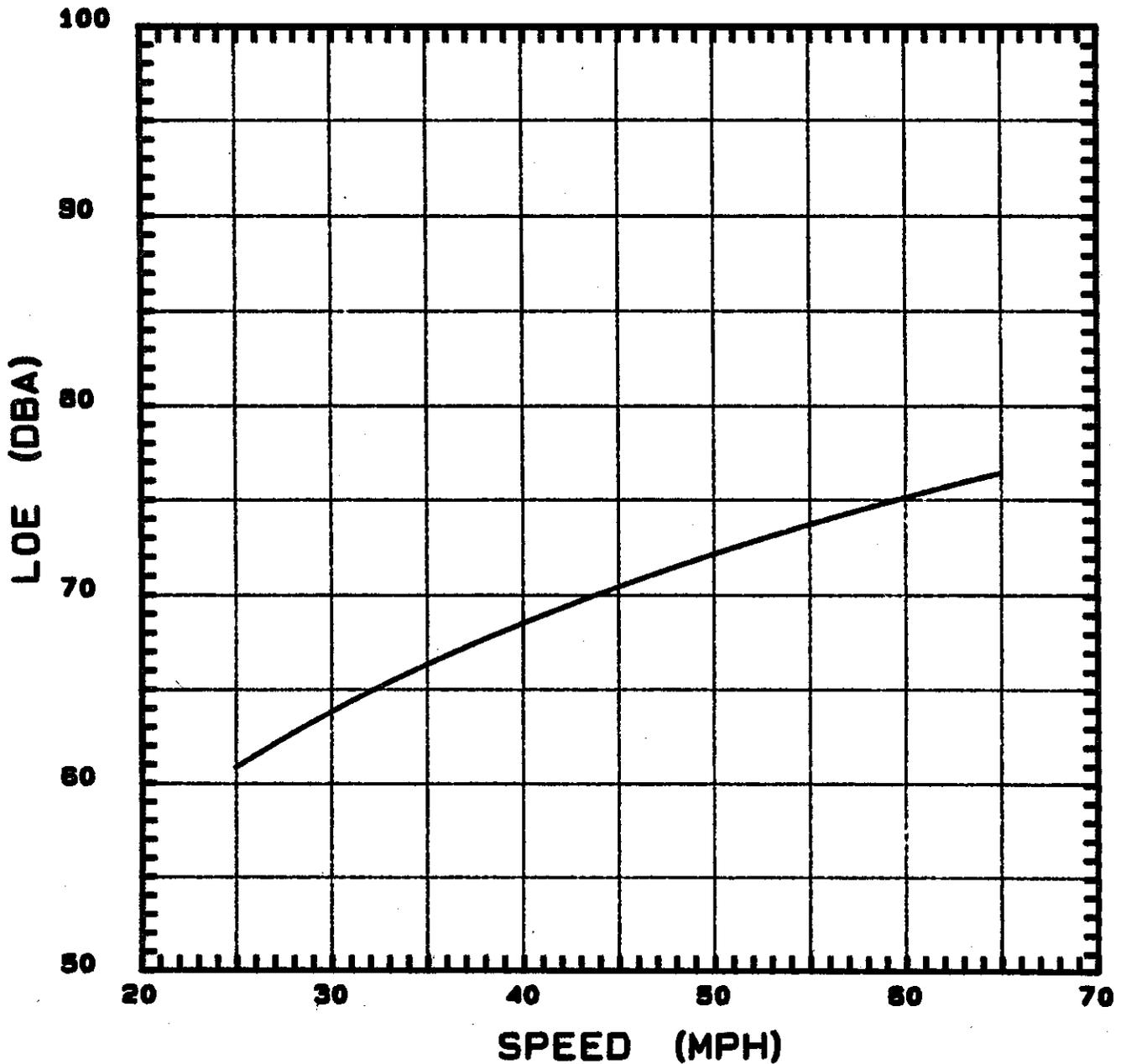


D-50

# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

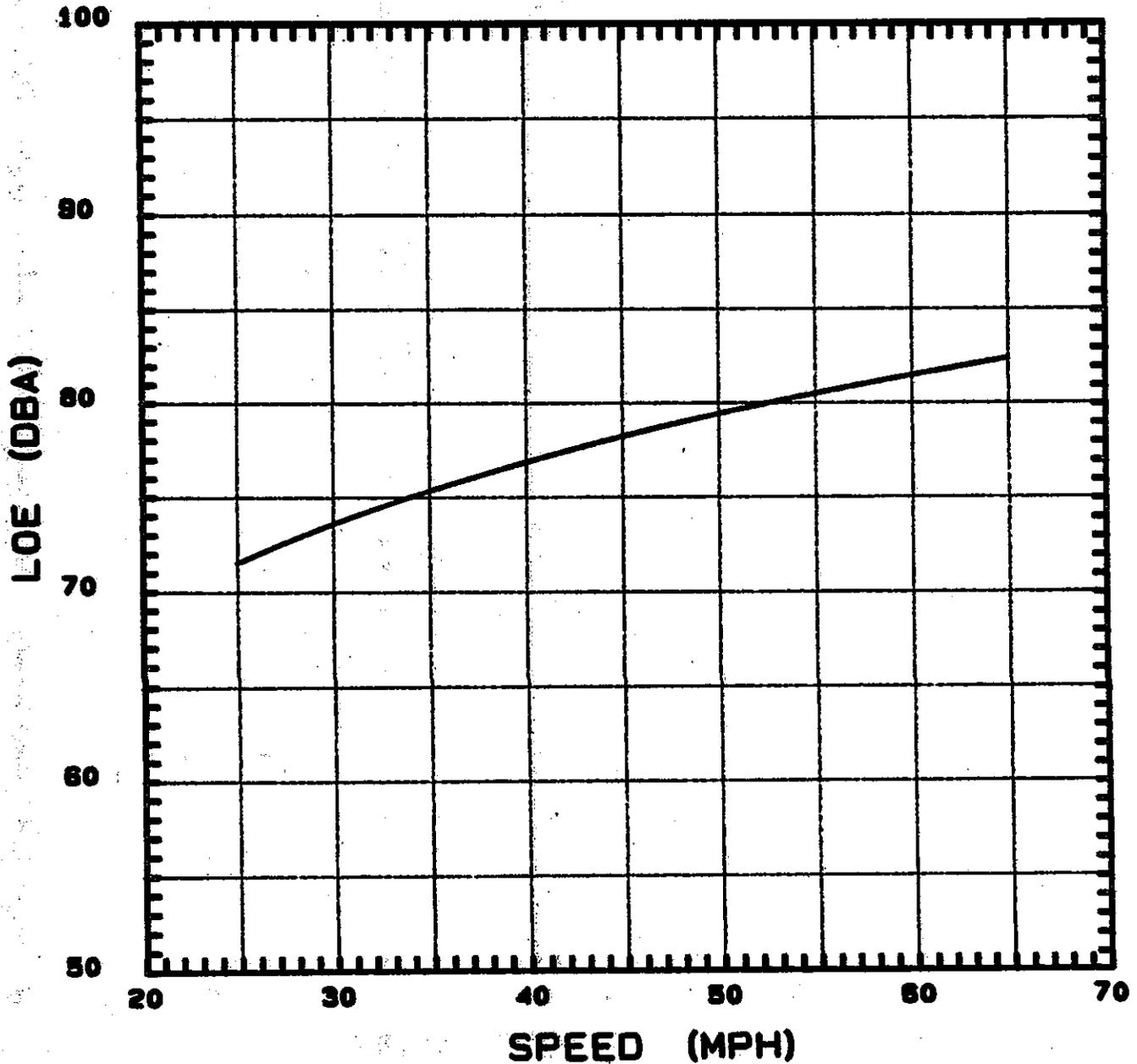
— VEH. TYPE: ALL AUTOS LOE=8.37+37.57\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

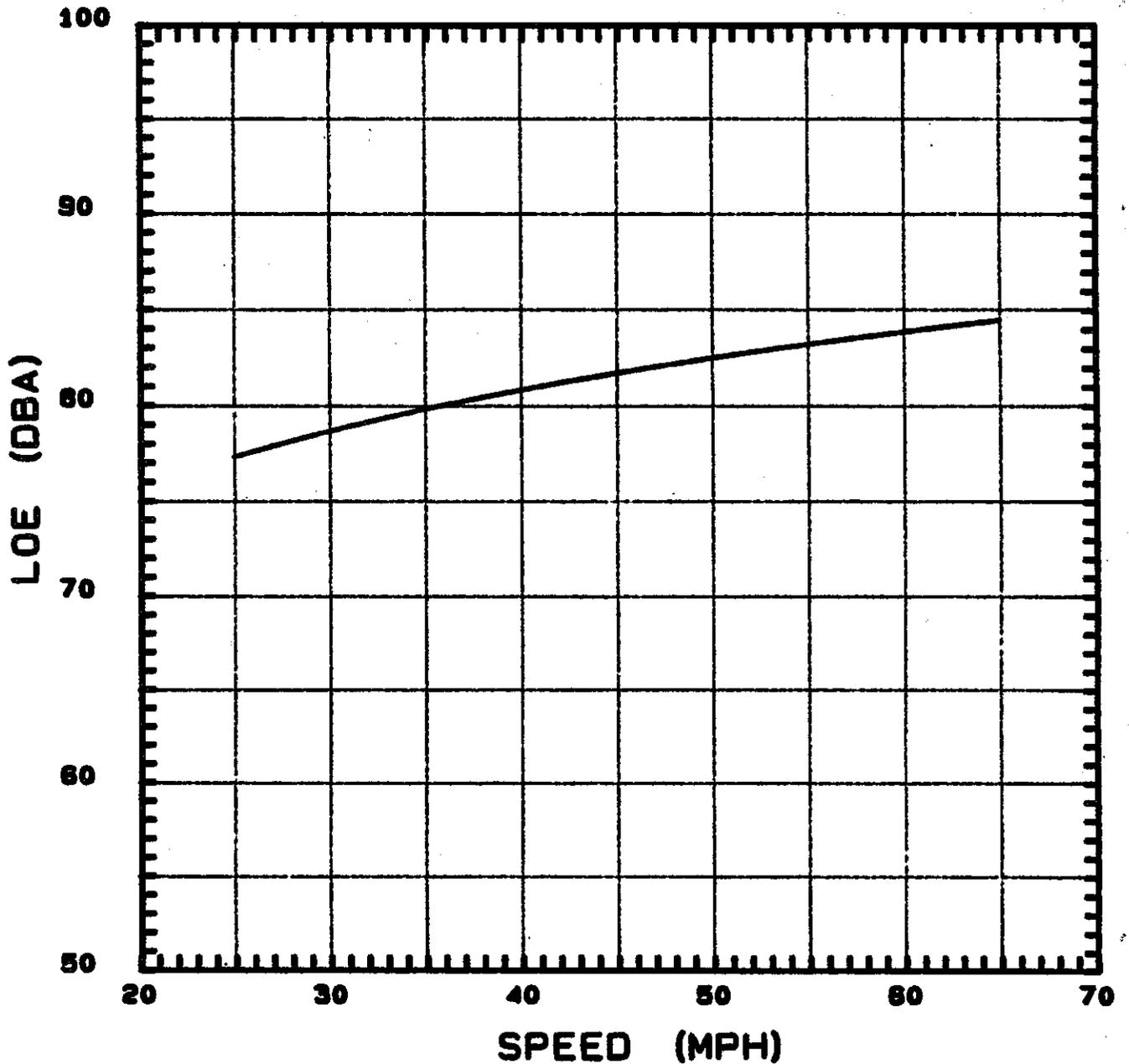
— VEH. TYPE: MEDIUM TRUCKS LOE=35+28.17\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

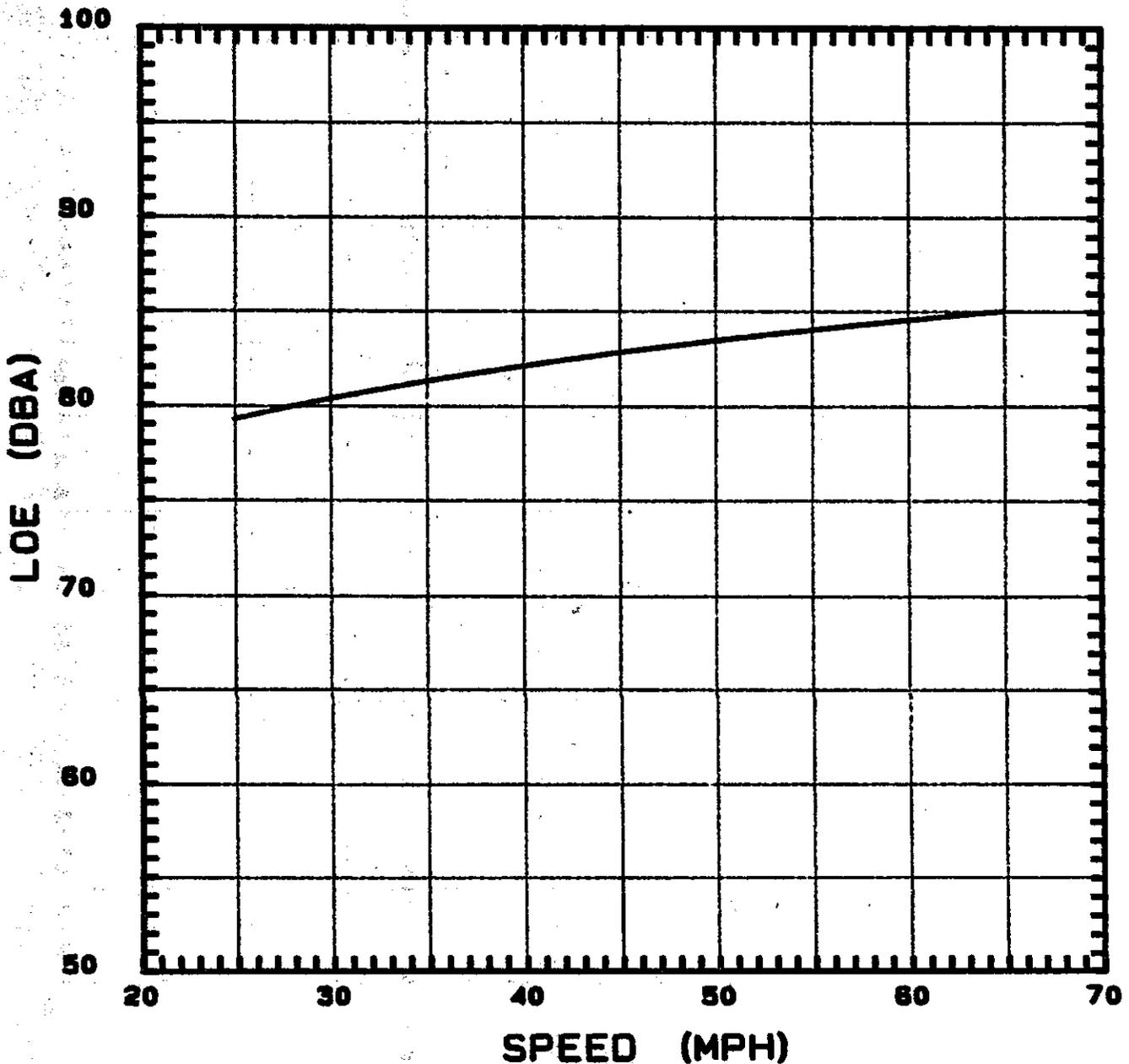
— VEH. TYPE: HT 3-AXLE LOE=53.34+17.19\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

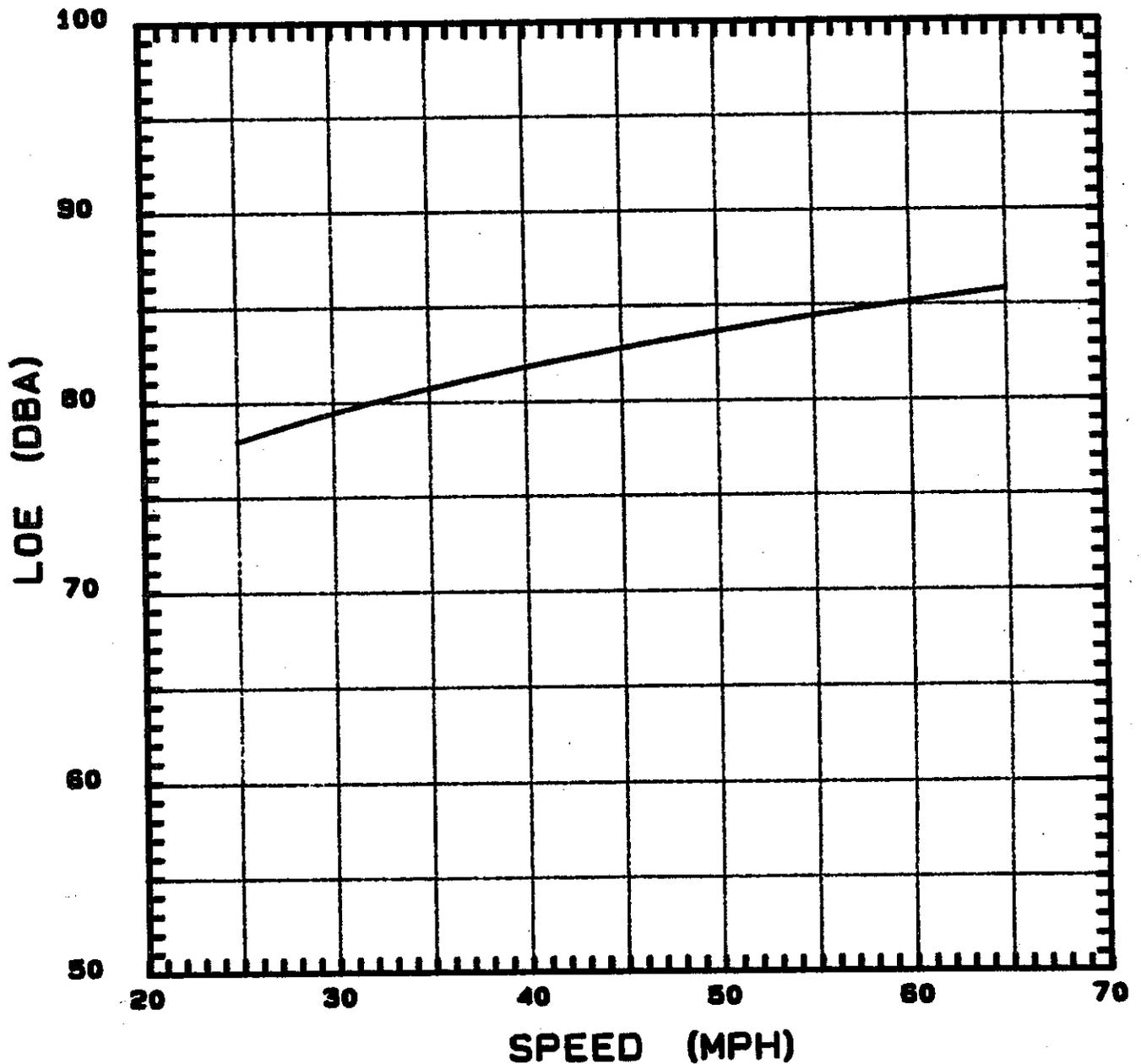
— VEH. TYPE: HT 4-AXLE LOE=59.97+13.86\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

— VEH. TYPE: HT 5-AXLE LOE=51.49+18.96\*LOG (MPH)

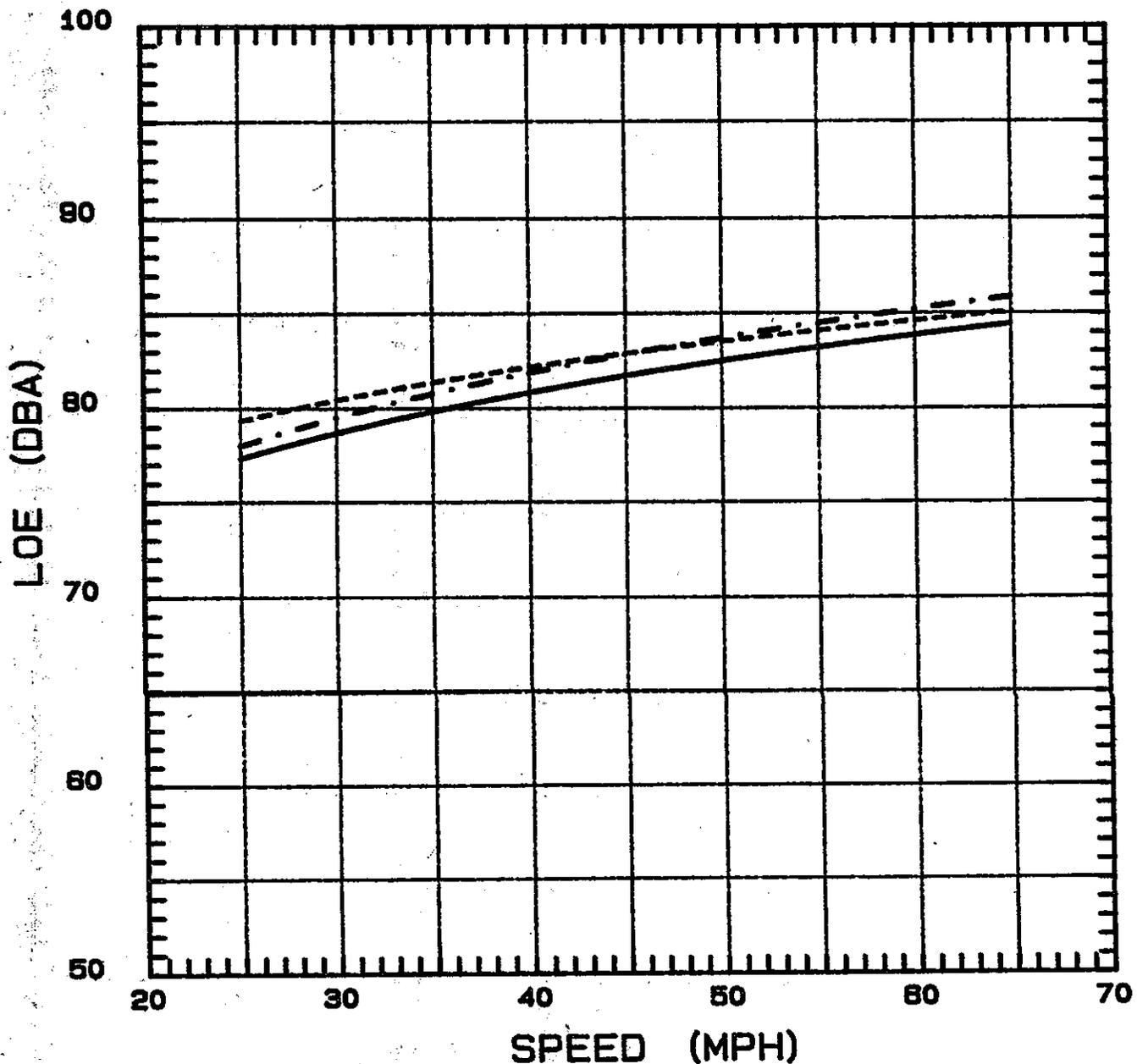


D-55

# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

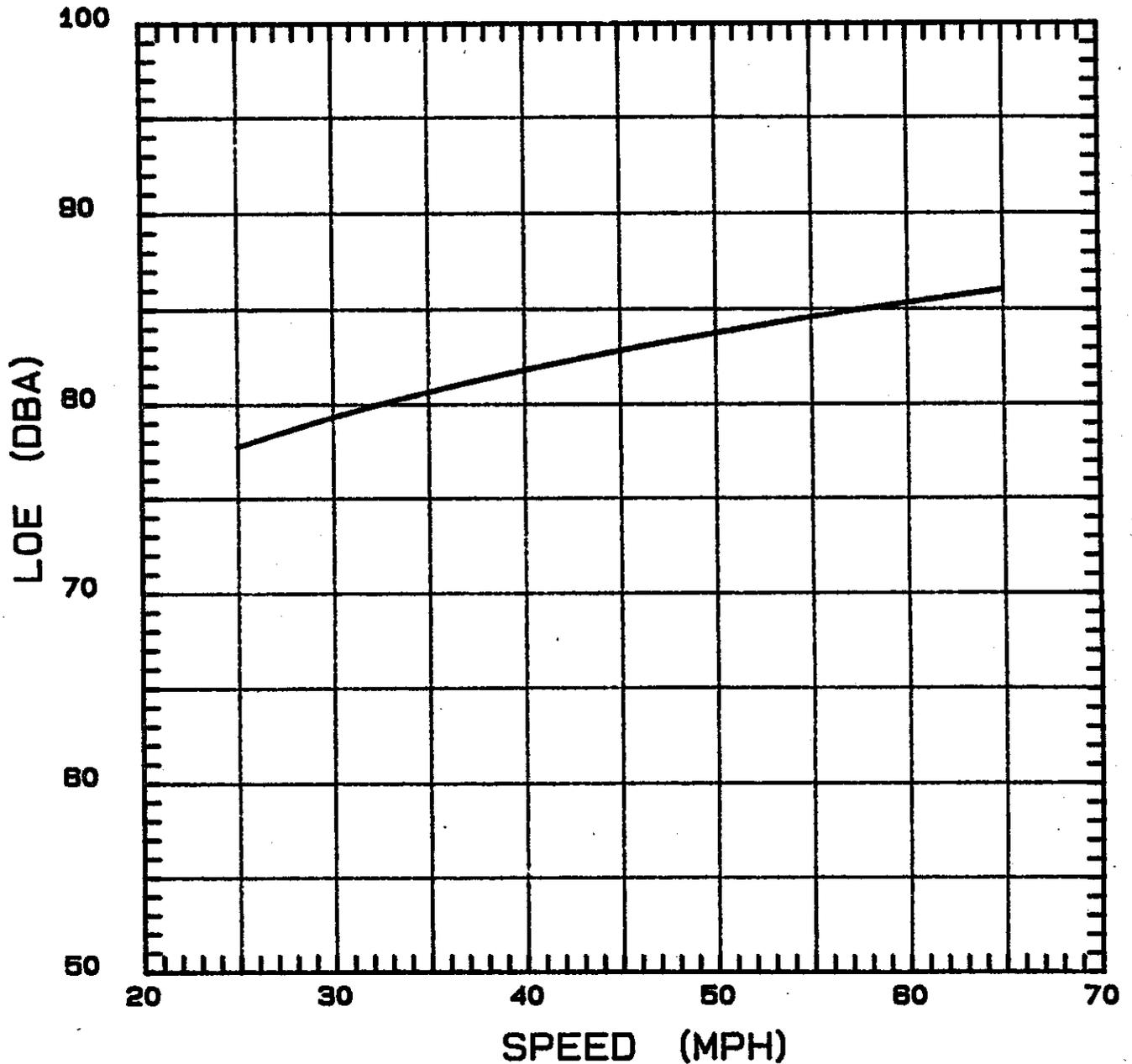
- VEH. TYPE: HT 3-AXLE LOE=53.34+17.19\*LOG (MPH)
- - - VEH. TYPE: HT 4-AXLE LOE=59.97+13.86\*LOG (MPH)
- · - VEH. TYPE: HT 5-AXLE LOE=51.49+18.98\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES EXCEPT 4, 8, 13  
MIC.#3 HT-10FT. DIST-50FT.

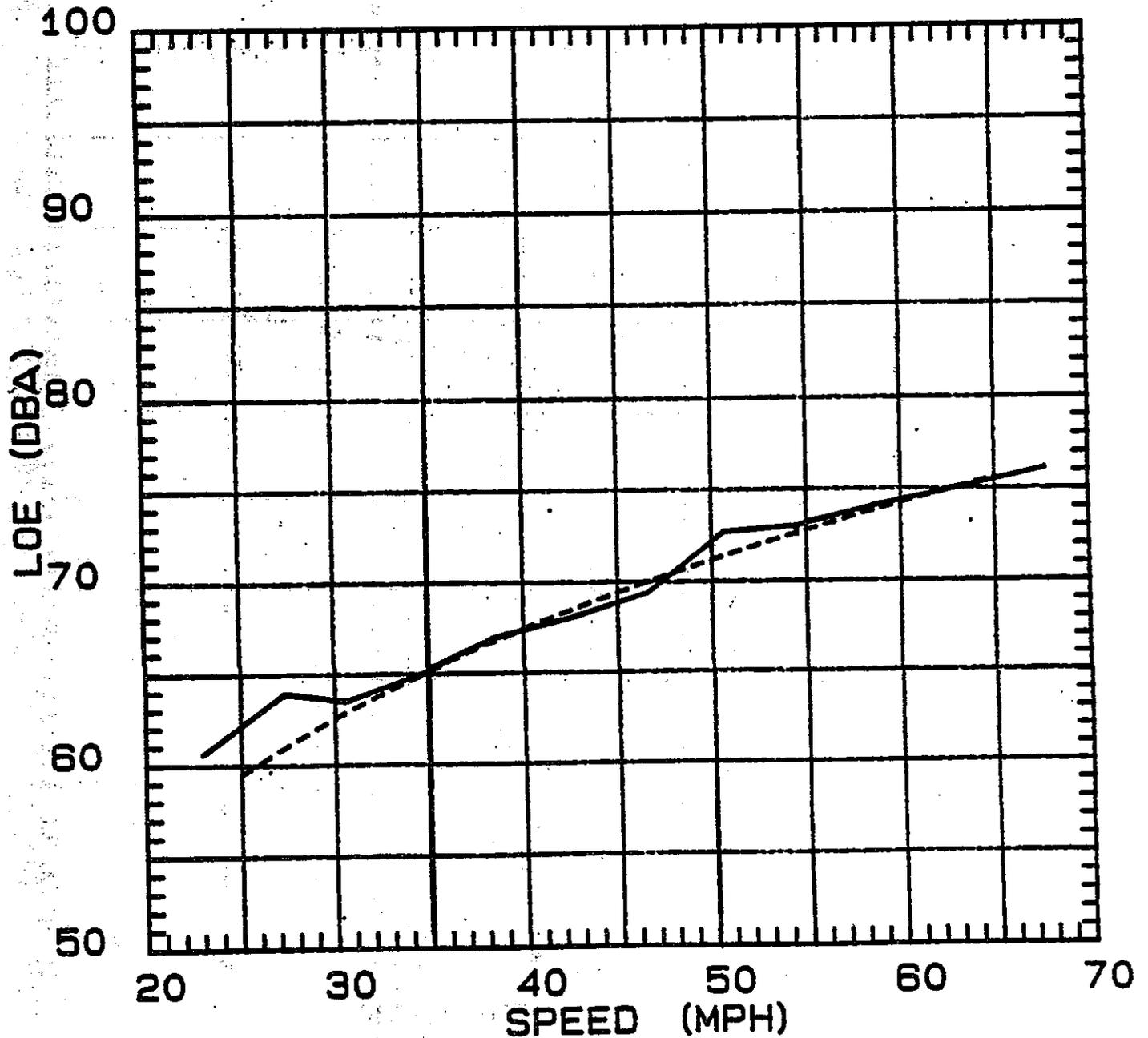
— VEH. TYPE: ALL HT LOE=49.88+19.97\*LOG (MPH)



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

VEHICLE TYPE: ALL AUTOS  
MIC.#2 HT-5FT. DIST-50FT.

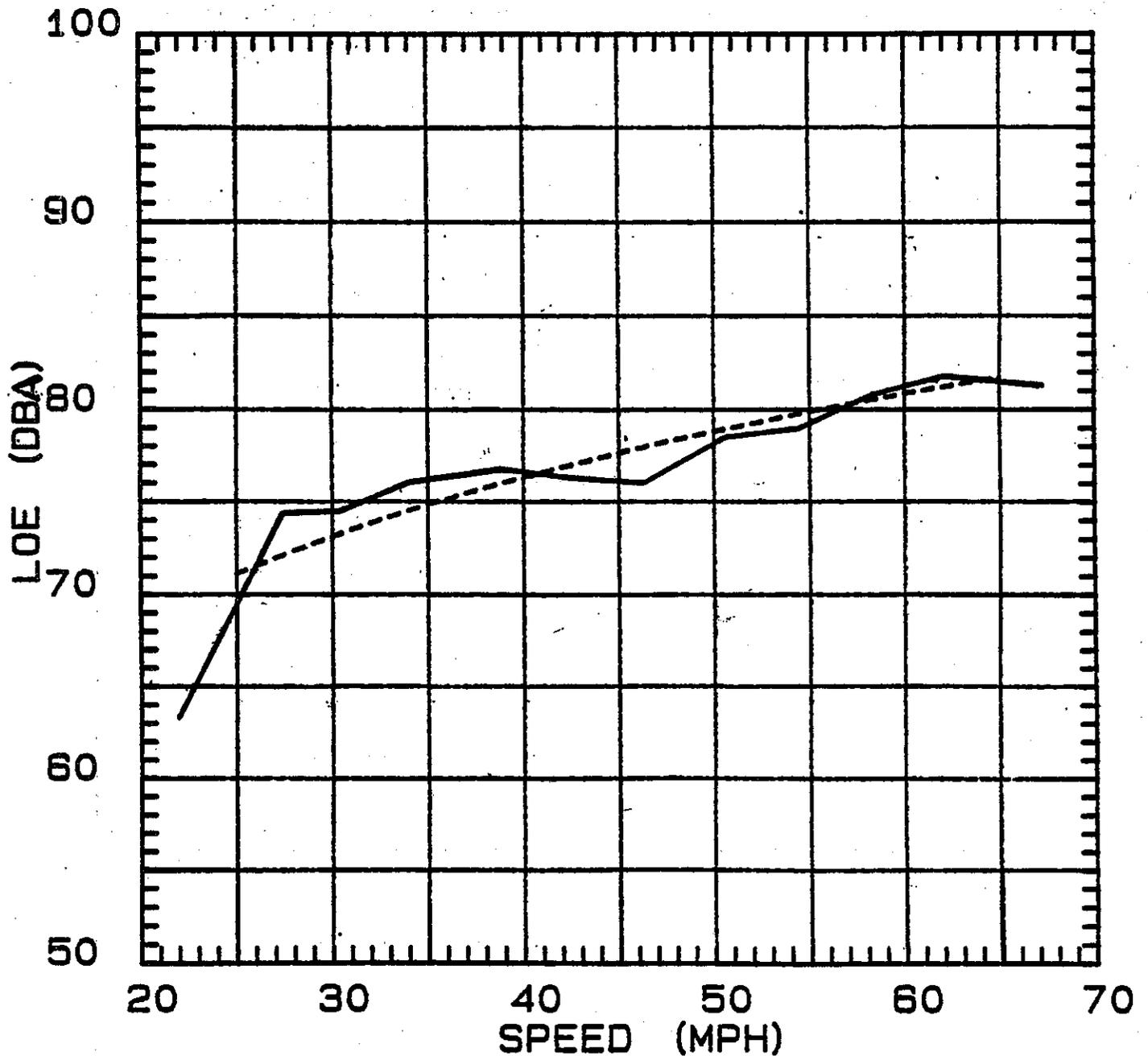
----- ALL SITES  $LOE = 5.21 + 38.83 \times \text{LOG}(\text{MPH})$   
——— ALL SITES SPEED CLASS MEAN DATA



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

VEHICLE TYPE: MEDIUM TRUCKS  
MIC.#2 HT-5FT. DIST-50FT.

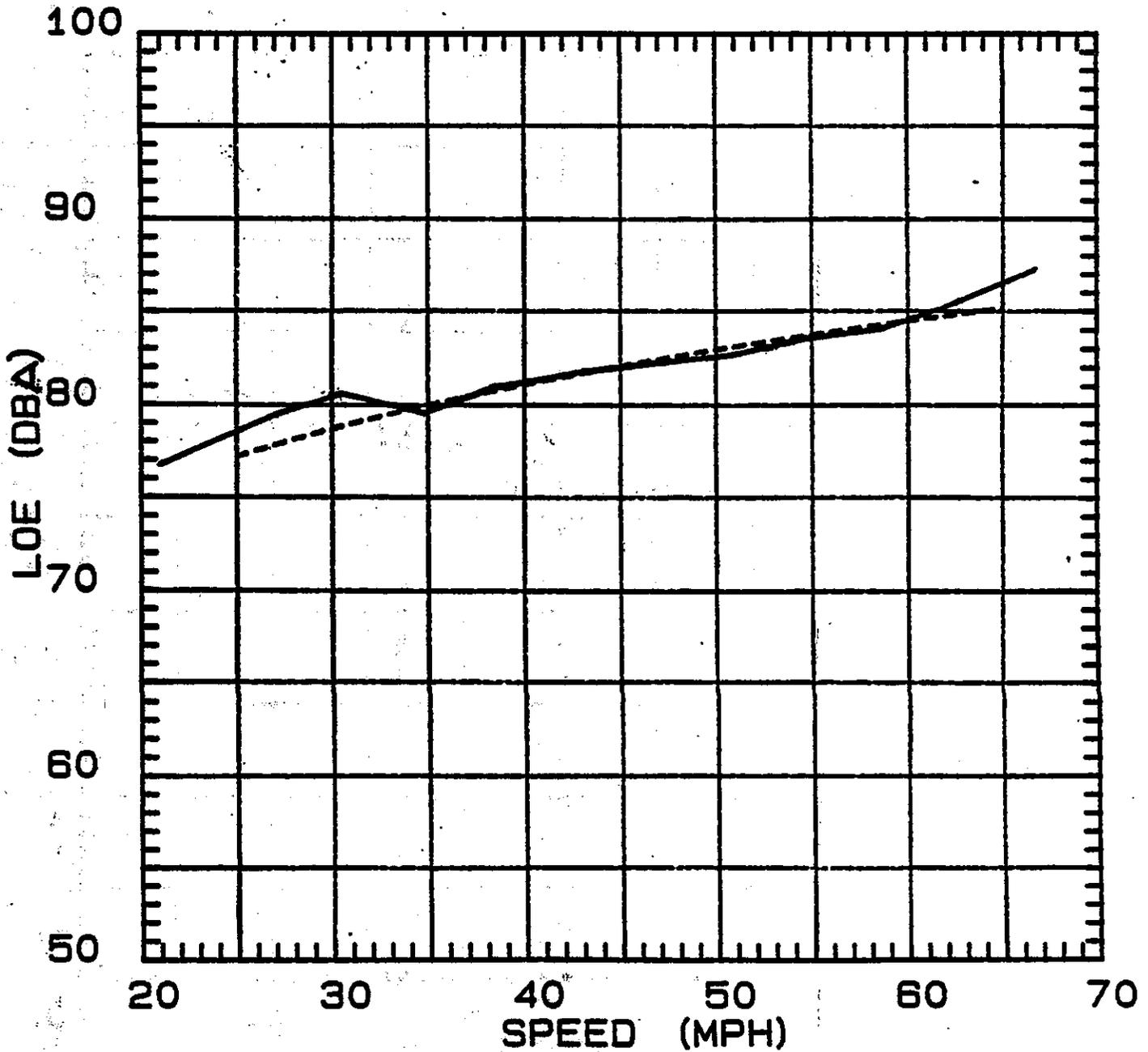
----- ALL SITES  $LOE = 35.34 + 25.59 * \text{LOG}(\text{MPH})$   
——— ALL SITES SPEED CLASS MEAN DATA



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

VEHICLE TYPE: HEAVY TRUCKS  
MIC.#2 HT-5FT. DIST-50FT.

----- ALL SITES LOE=50.37+19.18\*LOG (MPH)  
———— ALL SITES SPEED CLASS MEAN DATA



# CALIFORNIA VEHICLE NOISE EMISSIONS LOE VS. SPEED

ALL SITES  
MIC.#2 HT-5FT. DIST-50FT.

- |           |                         |                           |           |
|-----------|-------------------------|---------------------------|-----------|
| -----     | VEH.TYPE: ALL AUTOS     | LOE= 5.2 + 38.8*LOG (MPH) |           |
| - · - · - | VEH.TYPE: MEDIUM TRUCKS | LOE=35.3 + 25.6*LOG (MPH) |           |
| ————      | VEH.TYPE: HEAVY TRUCKS  | LOE=51.9 + 19.2*LOG (MPH) | 25<MPH<31 |
|           |                         | LOE=50.4 + 19.2*LOG (MPH) | 35<MPH<65 |
|           |                         | STRAIGHT LINE TRANSITION  | 31<MPH<35 |

